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EXPLORER 17 DATA REDUCTION PROGRAM DOCUMENTATION AND REPORT FOR THE PRESSURE DENSITY PROGRAM

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CHARLES HANLEY
WILLIAM GOUGH

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GODDARD SPACE FLIGHT CENTER
GREENBELT, MARYLAND

**EXPLORER 17 DATA REDUCTION
PROGRAM DOCUMENTATION AND REPORT FOR
THE PRESSURE DENSITY PROGRAM**

by

Charles Hanley

**Advanced Projects Branch
Systems Analysis & Program Design Section**

and

William Gough

**Advanced Projects Branch
Programming Methods Section**

March 15, 1965

**Goddard Space Flight Center
Greenbelt, Maryland**

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S-6 DATA REDUCTION
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INTRODUCTION

The Pressure Density Program (PDP) is a digital computer program for processing data consisting of voltage measurements of the neutral atmospheric density and temperature.

GENERAL DESCRIPTION

The problem involves analyses of the data recorded by the Bayard-Alpert (BA 1 & 2) and Redhead (RH 1 & 2) gauges. These four gauges combine to cover the expected 10^{-6} torr to 10^{-11} torr pressure range, and have been physically positioned on the satellite as follows:

1. Bayard-Alpert gauge #1 (BA 1) lower hemisphere
2. Bayard-Alpert gauge #2 (BA 2) equator
3. Redhead gauge #1 (RH 1) equator
4. Redhead gauge #2 (RH 2) upper hemisphere

These gauges are calibrated by laboratory and inflight measurements. The calibration values are represented by a single or set of functions.

1. Input to Pressure-Density Program

a. Input data provided by the experimenter

Laboratory calibration values for each sensor (gauge), hi and lo values for the Bayard-Alpert gauges, h_i (H_c), l_o (L_c), and medium (M_c) values for the Redhead gauges.

Conversion function (table) for each sensor (I_c vs. V_c)

Table of sensitivities (η) versus current (I_c) for each gauge

k factor for density calculations

b. Input from telemetry data

In-flight calibration values, h_i (H_f), l_o (L_f) and medium (M_f) for Redhead gauges only.

Selected DC voltage data for all four gauges (V)

Selected AC voltage data for Bayard-Alpert gauges (V_a)

Electronics card temperature (T_c)

Electrometer temperature (T_e)

c. Input from aspect reduction

Maximum ram velocity for each gauge (V_{rx})

Minimum ram velocity for each gauge (V_{rn})

Longitude, latitude, altitude, local solar time (position of the sun when data was received) and spin period.

2. Output from Pressure Density Program

The output from the program is a computed density and pressure history that is suitable for analysis by the experimenter.

MATHEMATICAL DESCRIPTION

Because of differences of design and gauge characteristics it is necessary to discuss the mathematics involved in computing pressure for the BA and RH gauges separately.

The density computations will be developed as functions of the gauge orientation on the satellite and will be divided into equatorial and non-equatorial gauge categories.

a. Definitions

The terms used in the following mathematical discussions are defined as follows:

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Source</u>
V	= raw telemetered input data	volts	telemetry
ΔV	= calibration adjustment	volts	computed
I_c	= current	amperes	computed
η_b	= sensitivity	—	computed
η_r	=	—	Lab
A_{r1}	=	—	Lab
A_{r2}	= table of values (see Fig. 3)	—	Lab
B_{r1}	=	—	Lab
B_{r2}	=	—	Lab
P	= pressure	torrs	computed
K	= unit conversion constant	grams kilo- meters/torr/ sec. squared	computed
H_L	= high lab calibration values	volts	Lab
H_f	= high flight calibration values	volts	telemetry
M_L	= medium lab calibration values	volts	Lab
M_f	= medium flight calibration values	volts	telemetry

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Source</u>
L_L =	low lab calibration values	volts	Lab
L_f =	low flight calibration values	volts	telemetry
I_e =	emission current	amperes	telemetry
V' =	adjusted telemetered voltage	volts	computed
V_{ba1} =	voltage vs current (I_n) conversion table	—	Monitor Control Program computation
V_{ba2} =	voltage vs current (I_n) conversion table	—	Monitor Control Program computation
V_{rh1} =	voltage vs current table	—	Lab
V_{rh2} =	voltage vs current table	—	Lab
P_x =	maximum pressure	torrs	computed
P_n =	minimum pressure	torrs	computed
V_{pi} =	most probable velocity of particles inside gauge	cm/sec	computed
V_{p0} =	most probable velocity of particles outside gauge	cm/sec	computed
V_{rx} =	maximum ram velocity	km/sec	aspect tape
V_{rn} =	minimum ram velocity	km/sec	aspect tape
V_{ave} =	average ram velocity	km/sec	aspect tape
R_0 =	gas constant	CGS	experimenter
T_0 =	outside temperature	deg. Kelvin	experimenter
T_i =	inside temperature	deg. Kelvin	experimenter
M_0 =	outside mass	grams/mole	experimenter
M_i =	inside mass	grams/mole	experimenter
S_x =	velocity ratio	—	computed
S_n =	velocity ratio	—	computed
D_1 =	density	—	computed
D_2 =	density	—	computed
V_x =	maximum voltage	volts	computed

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Source</u>
V_x	= adjusted maximum voltage	volts	computed
V_n	= minimum voltage	volts	computed
V_n'	= adjusted minimum voltage	volts	computed
I_x	= maximum current	amperes	computed
I_n	= minimum current	amperes	computed
T_x	= time of maximum pressure	sec	computed
T_n	= time of minimum pressure	sec	computed
k	= sensitivity factor	—	experimenter

GAUGE CHARACTERISTICS--PRESSURE COMPUTATIONS BAYARD-ALPERT GAUGES

BA 1	BA 2																												
$\Delta V = 0$ $V' = V + \Delta V$ $\text{Log } I_c = \text{Log } I_n + \left(\frac{V' - V_{ba_n}}{V_{ba1_{n+1}} - V_{ba_n}} \right) (\text{Log } I_{n+1} - \text{Log } I_n)$ <p>(see Figure B1)</p> <p>$I_c = \text{antilog} (\log \pm c)$</p> <p>now</p> <p>$\eta_b = 1/k \cdot I_e$ ($S = \text{sensitivity}$)</p> <p>where</p> <p>$k = 97.5$</p> <p>then</p> <p>$P = I_c / \eta_b$</p>	$\Delta V = .075 \text{ volts}$ <p>NOTE -- Where no corresponding formulas or values are given for BA 2, they are the same as those for BA 1. (see Figure B2)</p> <p>$k = 119.5$</p>																												
<table> <tr> <th>Vba1</th><th>I_n</th></tr> <tr> <td>x.xxx</td><td>x.xxE-xx</td></tr> <tr> <th>Vba1 2</th><th>Log I₂</th></tr> <tr> <td>.</td><td>.</td></tr> <tr> <td>.</td><td>.</td></tr> <tr> <td>.</td><td>.</td></tr> <tr> <th>Vba1 18</th><th>Log I₁₈</th></tr> </table> <p>Figure B1</p>	Vba1	I _n	x.xxx	x.xxE-xx	Vba1 2	Log I ₂	Vba1 18	Log I ₁₈	<table> <tr> <th>Vba2</th><th>I_n</th></tr> <tr> <td>Vba2₁</td><td>Log I₁</td></tr> <tr> <td>Vba2₂</td><td>Log I₂</td></tr> <tr> <td>.</td><td>.</td></tr> <tr> <td>.</td><td>.</td></tr> <tr> <td>.</td><td>.</td></tr> <tr> <th>Vba2 18</th><th>Log I₁₈</th></tr> </table> <p>Figure B2</p>	Vba2	I _n	Vba2 ₁	Log I ₁	Vba2 ₂	Log I ₂	Vba2 18	Log I ₁₈
Vba1	I _n																												
x.xxx	x.xxE-xx																												
Vba1 2	Log I ₂																												
.	.																												
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.	.																												
Vba1 18	Log I ₁₈																												
Vba2	I _n																												
Vba2 ₁	Log I ₁																												
Vba2 ₂	Log I ₂																												
.	.																												
.	.																												
.	.																												
Vba2 18	Log I ₁₈																												

GAUGE CHARACTERISTICS – PRESSURE COMPUTATIONS REDHEAD GAUGES

RH 1	RH 2																																
$\Delta V = \frac{(HL - Hf) + (ML - Mf) + (LL - Lf)}{3}$ $V' = V_i + \Delta V$ <p>then</p> $\text{Log } I_c = \text{Log } I_n + \left(\frac{V' - V_n}{V_{n+1} - V_n} \right) (\text{Log } I_{n+1} - \text{Log } I_n)$ <p>see Figure R1</p> $I_c = \text{Antilog} (\text{Log } I_c)$	<p>Figure R2 is the same as R1 in format, but the values are different.</p>																																
<table> <tr> <th>Vrh1</th><th>Ic</th></tr> <tr> <td>x.xxx</td><td>x.xxE-xx*</td></tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> </table> <p>Figure R1</p> <p>then the program enters gauge sensitivity table (Figure R3)</p> <table> <tr> <th>RH 1</th><th>RH 1</th></tr> <tr> <td>Ic</td><td>A B</td></tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> </table> <p>Figure R3</p>	Vrh1	Ic	x.xxx	x.xxE-xx*					RH 1	RH 1	Ic	A B					<table> <tr> <th>Vrh2</th><th>Ic</th></tr> <tr> <td>x.xxx</td><td>x.xxE-xx*</td></tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> </table> <p>Figure R2</p> <p>See Figure R4</p> <table> <tr> <th>RH 2</th><th>RH 2</th></tr> <tr> <td>Ic</td><td>A B</td></tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> </table> <p>Figure R4</p>	Vrh2	Ic	x.xxx	x.xxE-xx*					RH 2	RH 2	Ic	A B				
Vrh1	Ic																																
x.xxx	x.xxE-xx*																																
RH 1	RH 1																																
Ic	A B																																
Vrh2	Ic																																
x.xxx	x.xxE-xx*																																
RH 2	RH 2																																
Ic	A B																																

Having found A and B by table lookup (see Figure R3), the program computes Pressure using the following formula:

$$P = \frac{I_c}{B} + A$$

*Sample values

GAUGE ORIENTATION-DENSITY COMPUTATIONS

Following the pressure computations the program computes density. Computations of density are divided into equatorial and non-equatorial types depending on the gauge orientation on the satellite. The first of these types to be discussed will be equatorial.

Equatorial Gauges (BA 2 and RH 1)

Using the following parameters from the pressure program;

t = time

V = voltage

V' = adjusted voltage

P = Pressure

the density for the equatorial gauges is computed as follows.

$$P_x = \text{maximum } (P), \quad P_n = \text{minimum } (P)$$

$$\Delta P = P_x - P_n \text{ (over one spin cycle of .667 sec.)}$$

$$V_{pi} = \sqrt{\frac{2 R_0 T_i}{M_i}} \text{ (Most probable velocity of particles inside gauge)}$$

$$V_{p0} = \sqrt{\frac{2 R_0 T_0}{M_0}} \text{ (Most probable velocity of particles outside gauge)}$$

where

$$R_0 = 8.315 \times 10^7$$

$$T_0 = 1000^\circ \text{ Kelvin}$$

$$T_i = 313^\circ \text{ Kelvin}$$

$$M_0 = 16$$

$$M_i = 16$$

$$V_{rx} = \text{Max ram velocity (obtained from the aspect tape)}$$

$$\text{Density} = \frac{\Delta P \cdot K}{V_{rx}}$$

where

$$K = \frac{1333}{\sqrt{\pi} \cdot V_{pi} \cdot 10^5}$$

Non-Equatorial Gauges (BA 1 and RH 2)

The non-equatorial density computations use the same parameters and gas constant to obtain ΔP , V_{pi} , and V_{p0} . The program now computes:

$$S_x = \frac{V_{rx}}{V_{p0}} \quad \text{and} \quad S_n = \frac{V_{rn}}{V_{p0}}$$

where

V_{rn} = Minimum ram velocity for each gauge.

From S_x and S_n the program determines which of the cases described below is needed to solve for the atmospheric density in torr units.

Case 1

$$S_x > 1 \quad \text{and} \quad S_n \geq 1$$

$$D_1 = \frac{P_x \cdot K}{V_{rx}}$$

$$D_2 = \frac{\Delta P \cdot K}{2 [V_{rx} - V_{ave}]}$$

where V_{ave} = Average ram velocity

Case 2

$$S_x > 1 \quad S_n < 1$$

$$D_1 = \frac{P_x \cdot K}{V_{rx}}$$

$$D_2 = \frac{1333 \cdot \Delta P \cdot M_0}{R_0 \cdot \sqrt{T_0 T_i} [F(S_x) - F(S_n)]}$$

where

$$F(s) = e^{-s^2} + s \cdot \sqrt{\pi} [1 + \operatorname{erf}(s)]$$

where

$$\operatorname{erf}(s) = \frac{a}{\pi} \cdot \int_0^s e^{-x^2} dx$$

Case 3

$$0 < S_x \leq 1$$

$$D_1 = 0$$

$$D_2 = \frac{1333 \Delta P M_0}{R_0 \sqrt{T_0 T_i} [F(S_x) - F(S_n)]}$$

Case 4

$$S_x \leq 0$$

$$D_1 = 0$$

$$D_2 = 0$$

After case computations the program is ready to write out on tape the parameters required by the experimenter for each spin cycle. The output format is as follows:

$T_x, V_x, V_{x'}, I_x, P_x$

BA 1 Alt., Lat., Long., LST (Local Solar Time), ΔP , T_{rx} , V_{rx} $D_1 = x.xxxE-xx$
 $T_n, V_n, V_{n'}, I_n, P_n$ $D_2 = x.xxxE-xx$

BA 2 same format as BA 1

RH 1 same format as BA 1

RH 2 same format as BA 1.

OTHER COMPUTATIONS

In addition to the computations for pressure and density values, the experimenter requested that certain parameters be computed and written out on the pressure plot tapes for plotting purposes.

$F(s)$ is determined from the $F(s)$ function using s computed as follows:

$$s = \frac{A + B \cos \theta}{V_{p0}}$$

where θ is determined by the formula:

$$\theta = \frac{(t - t_x) \cdot 9^\circ}{.0167}$$

The A and B above are described as:

$$A = V_{ave}$$

$$B = V_{rx} - V_{ave}$$

Both A and B are obtained from the aspect tape.

It is requested that P_i be normalized, which is accomplished by multiplying the raw pressure by the parameter M , where

$$M = \frac{V_{p0} \cdot F(S_x)}{P_x}$$

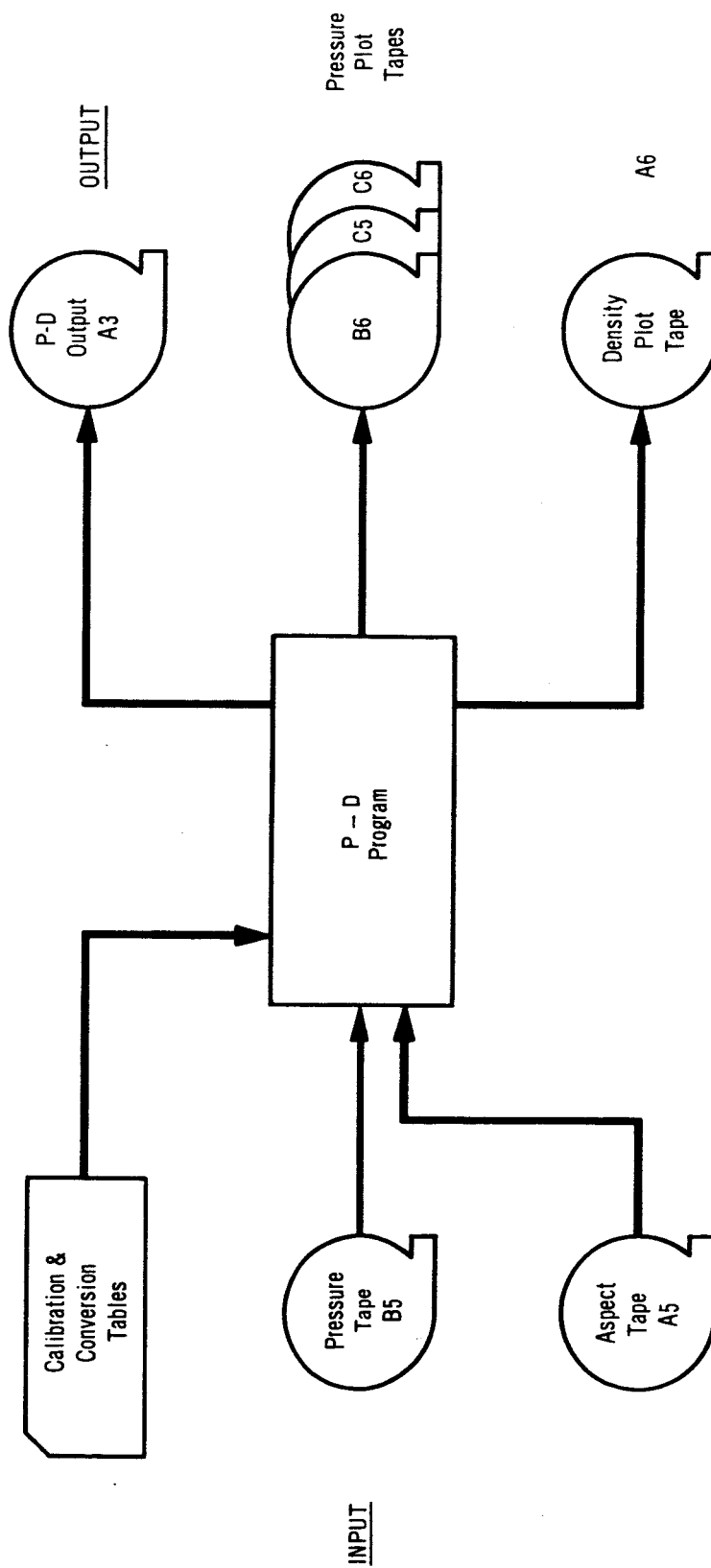
now

$$P_{\text{norm}} = P_i \cdot M$$

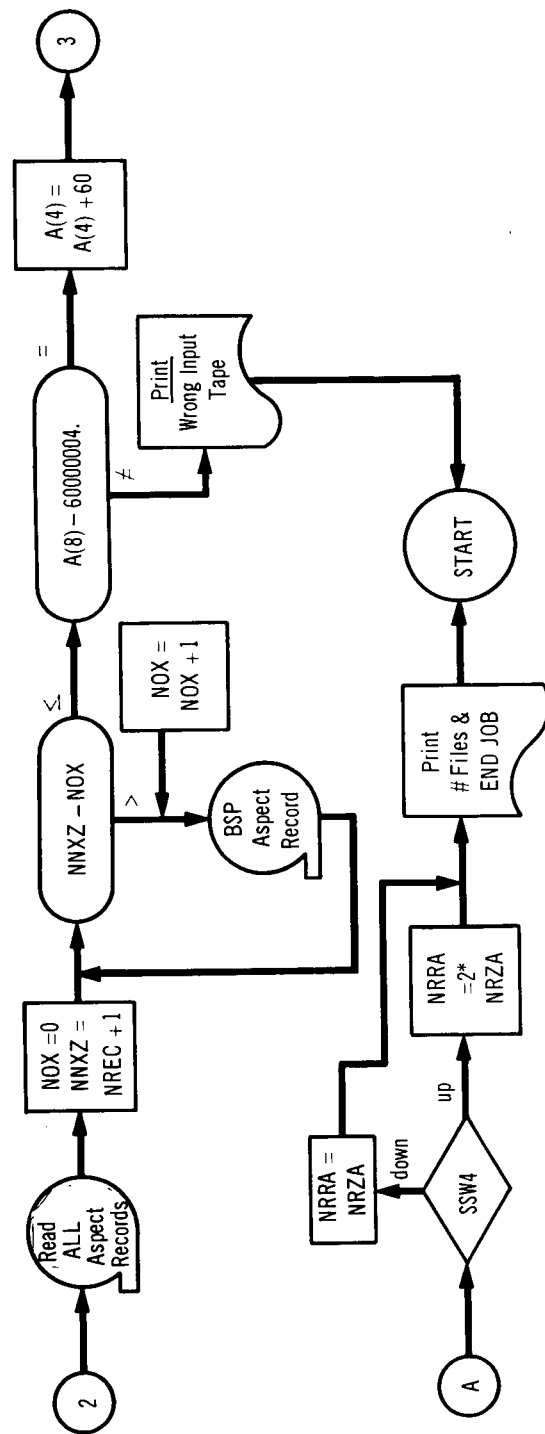
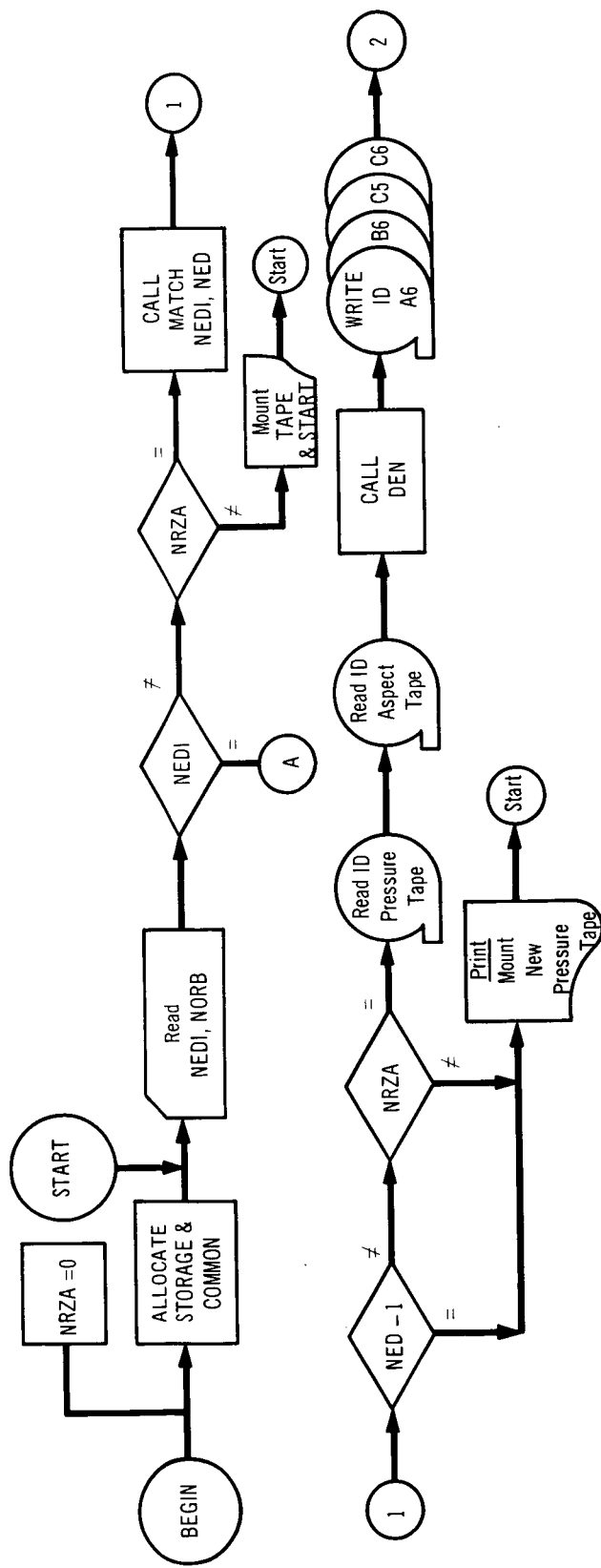
P_{norm} is later plotted against t (time) on the same graph as $V_{p0} \cdot F(s)$ vs θ .

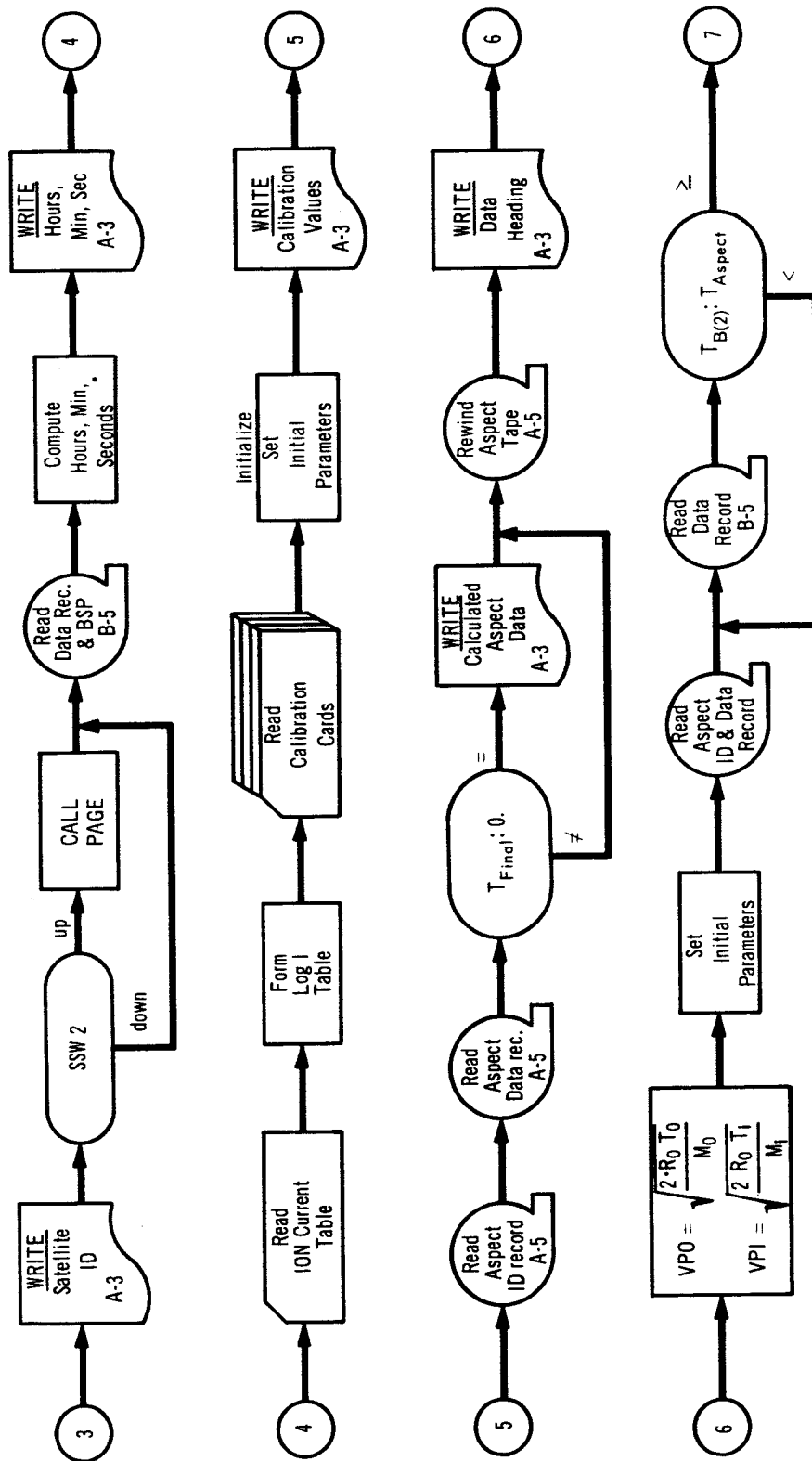
STRUCTURE OF THE PROGRAM

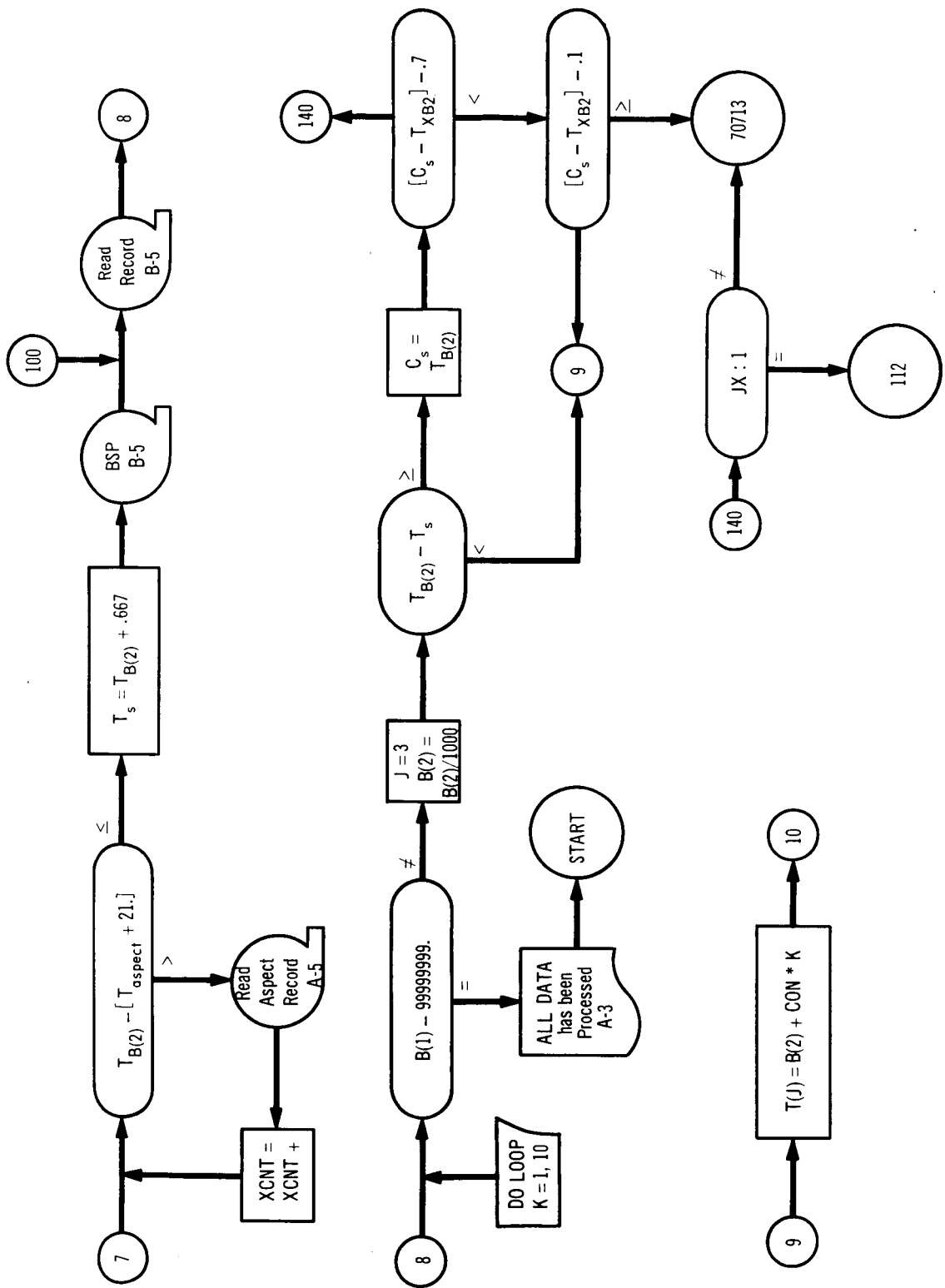
Input-Output Flow Diagram

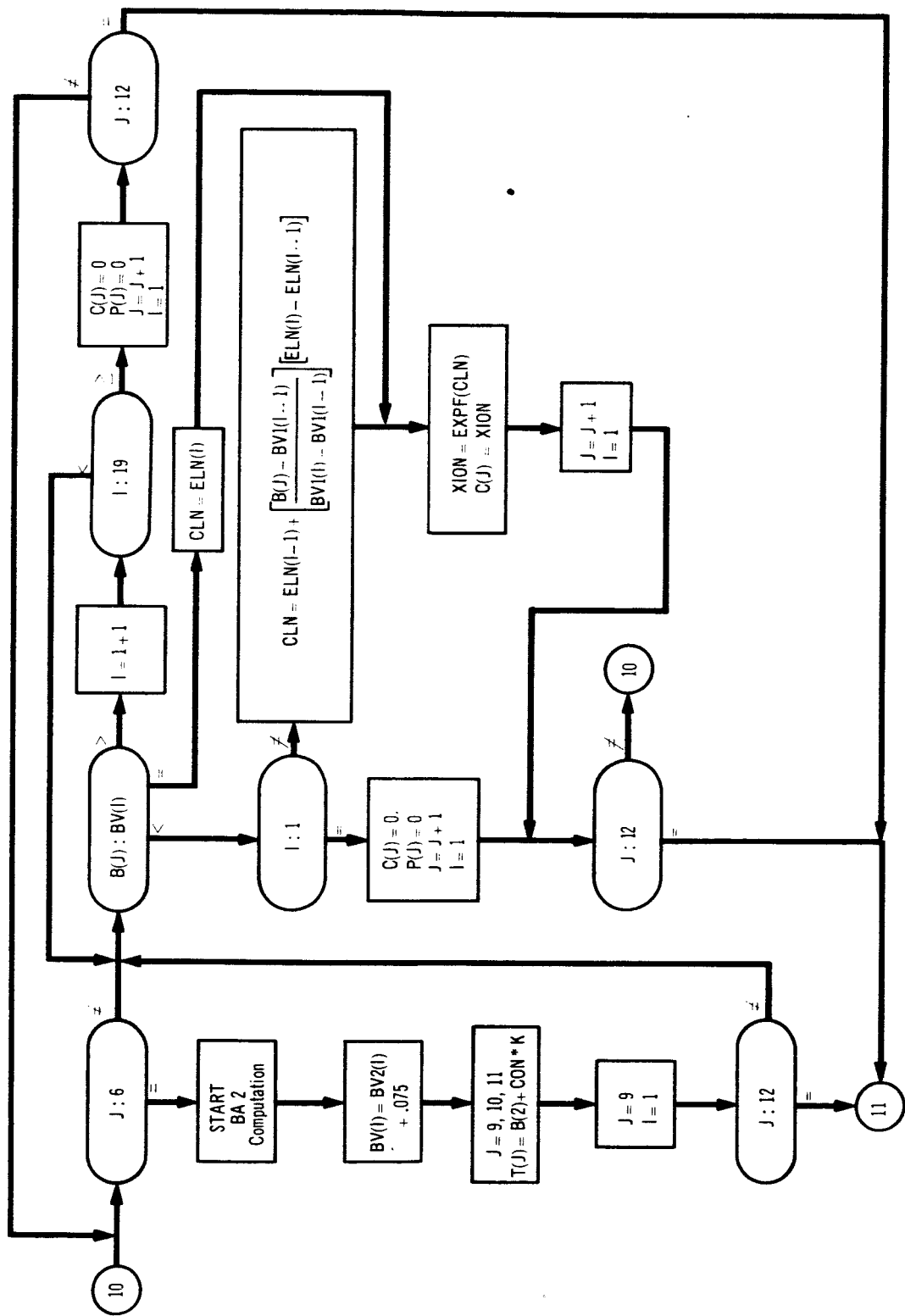


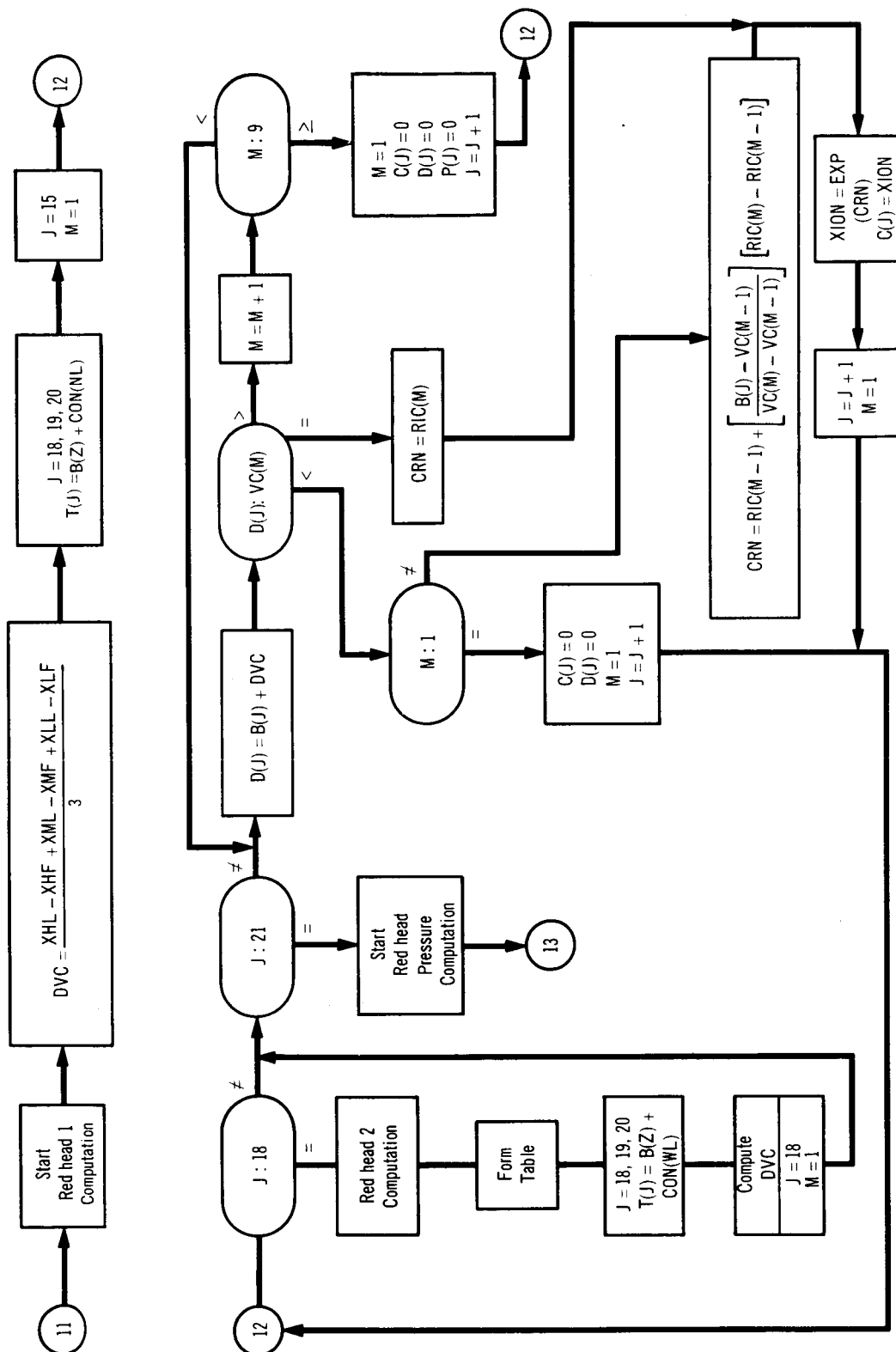
Pressure Density Program

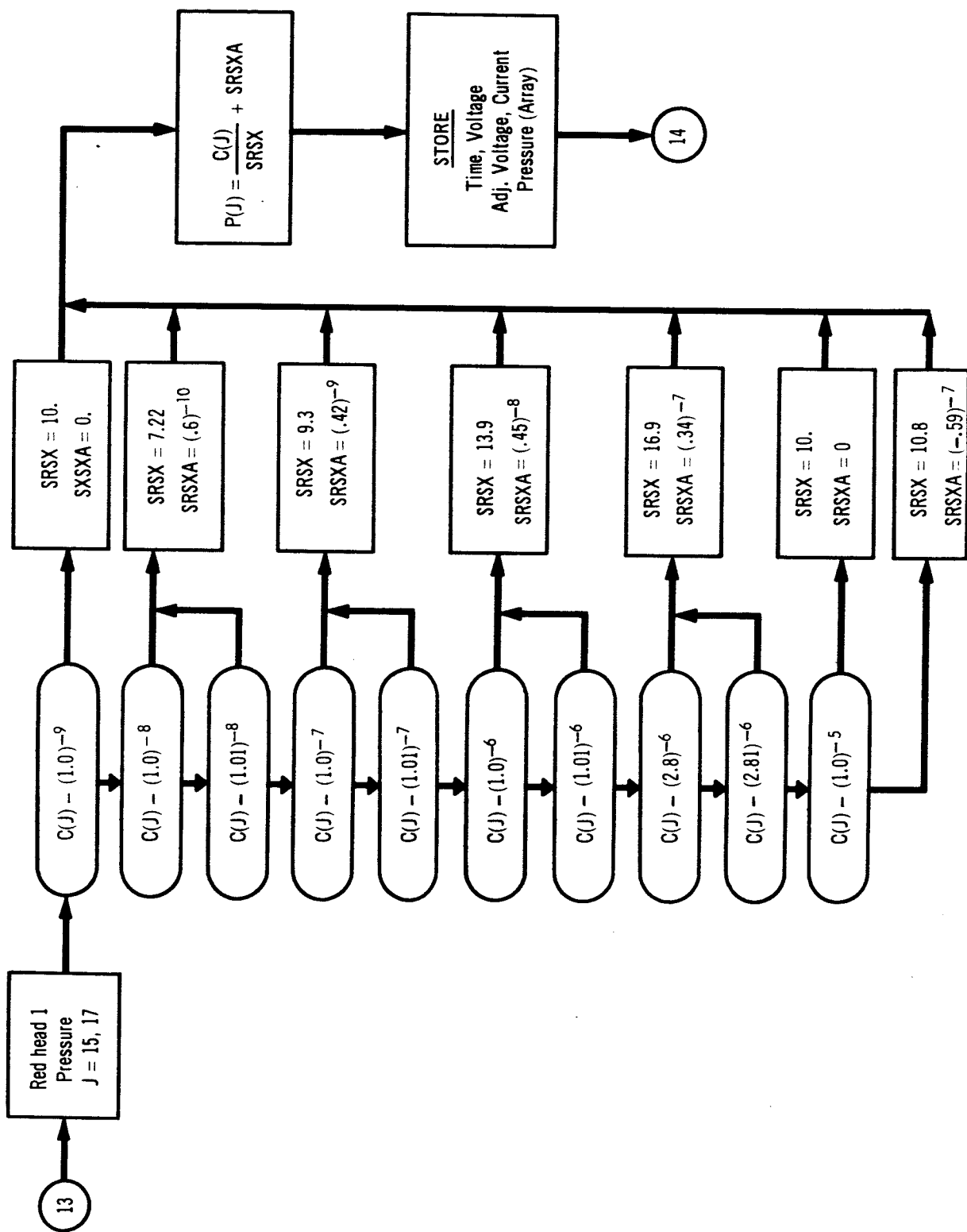


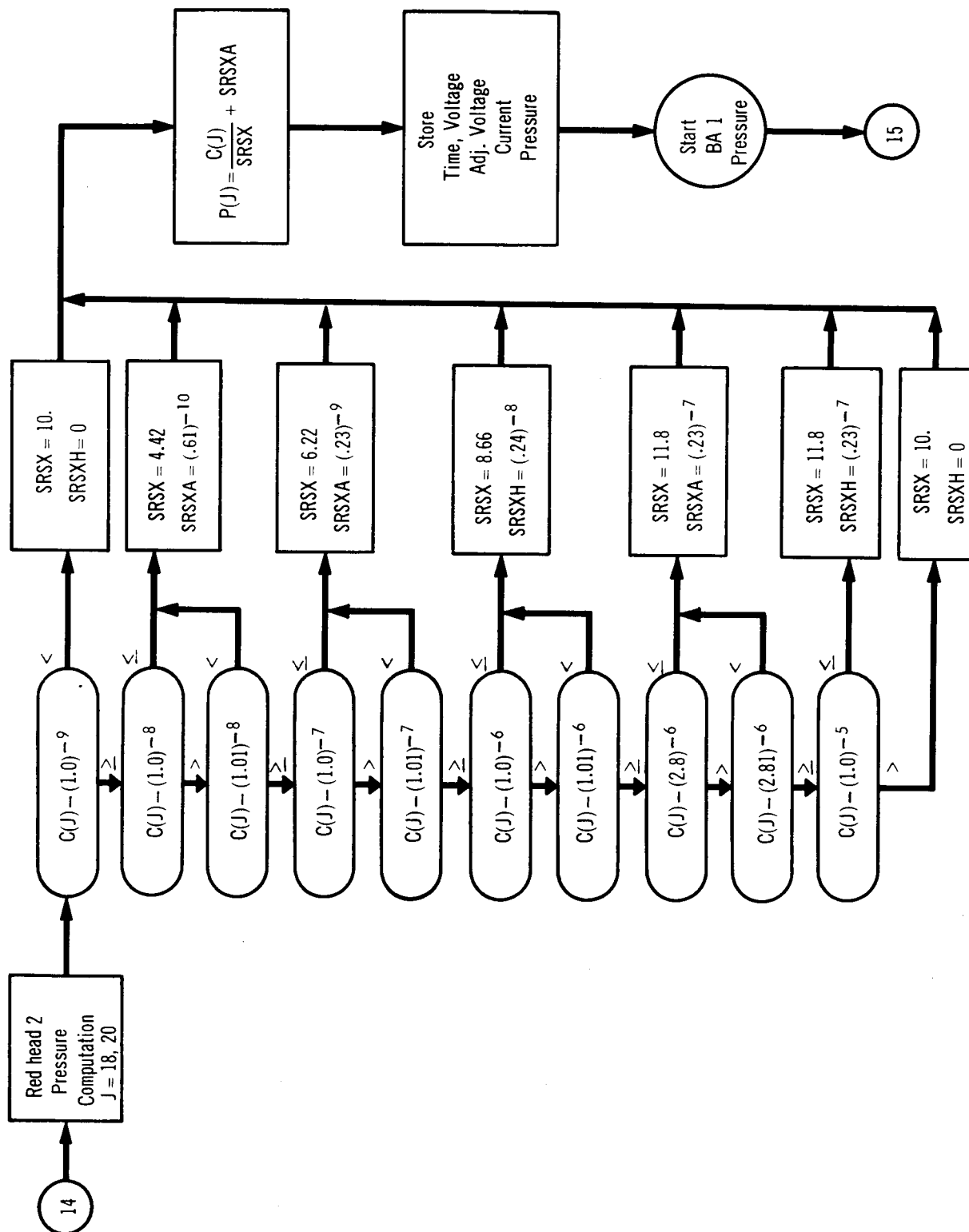


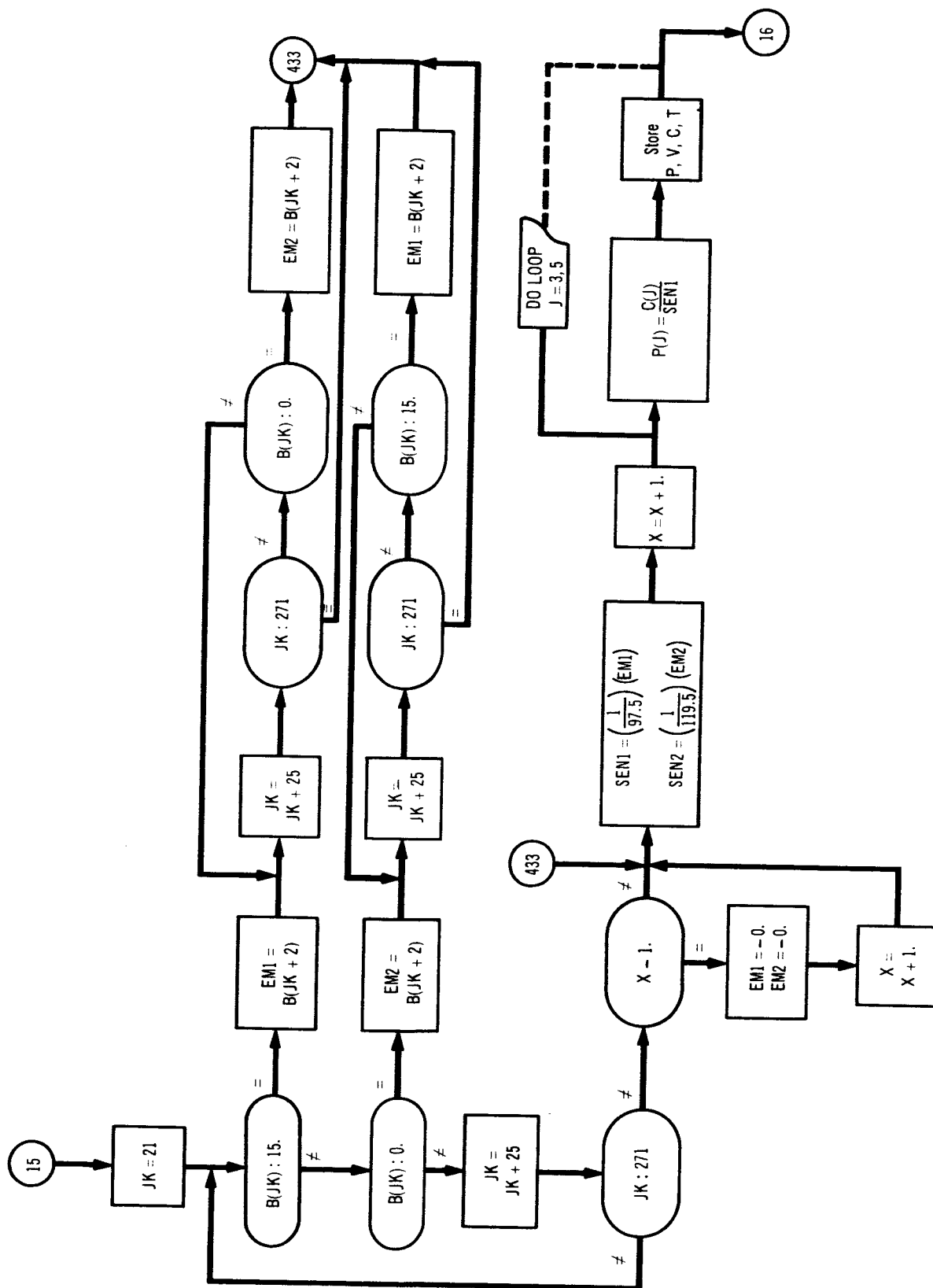




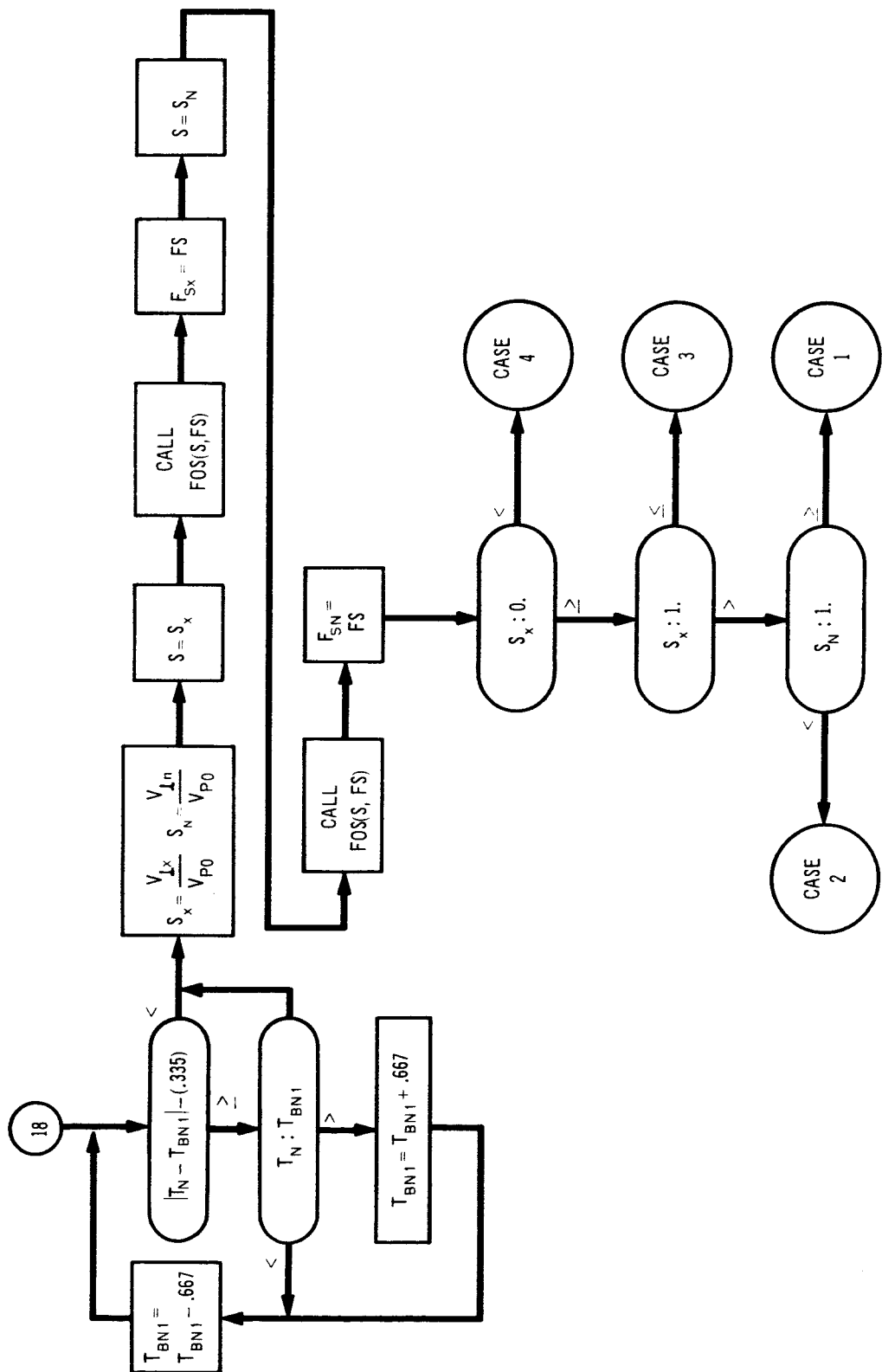


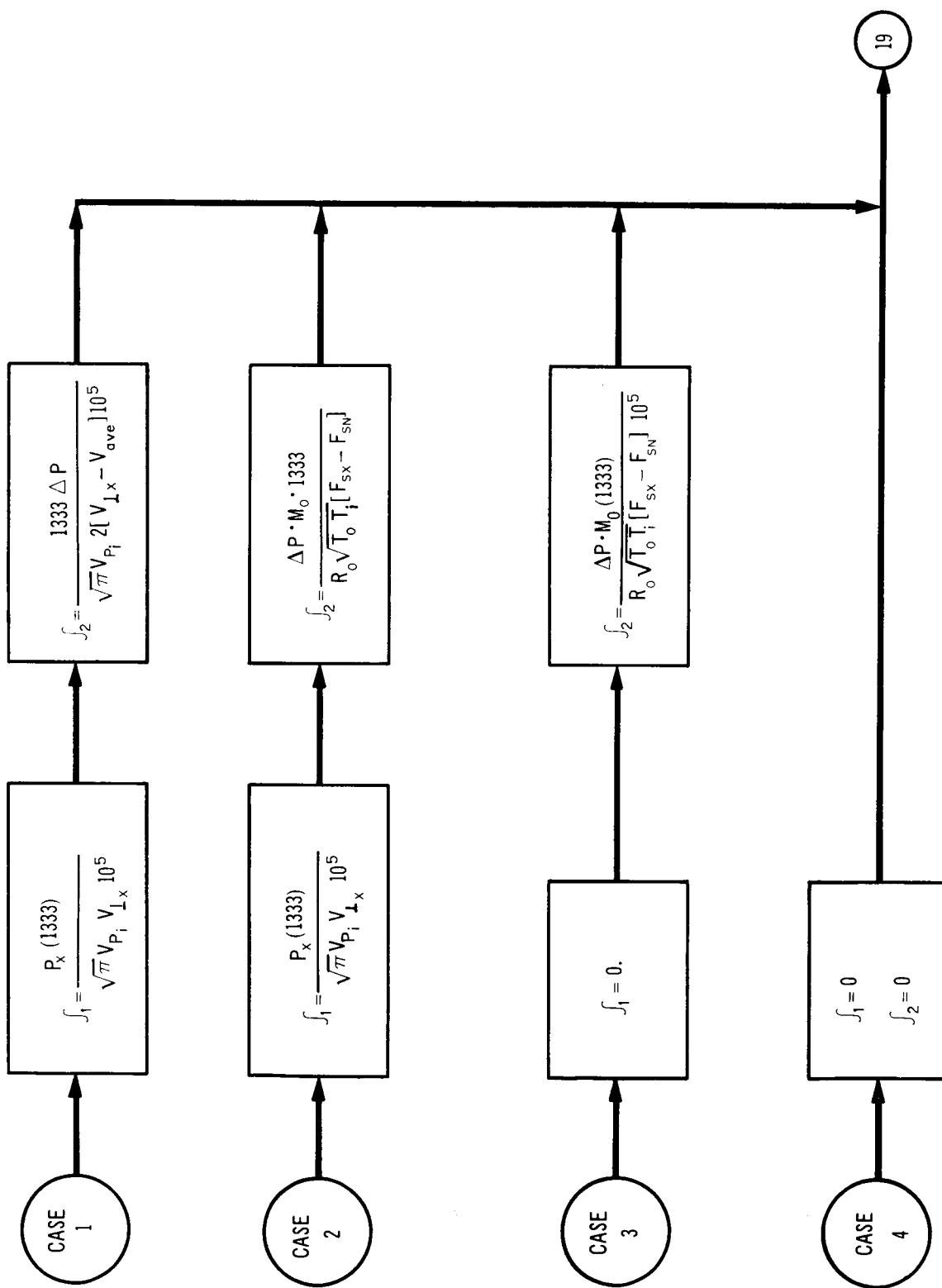


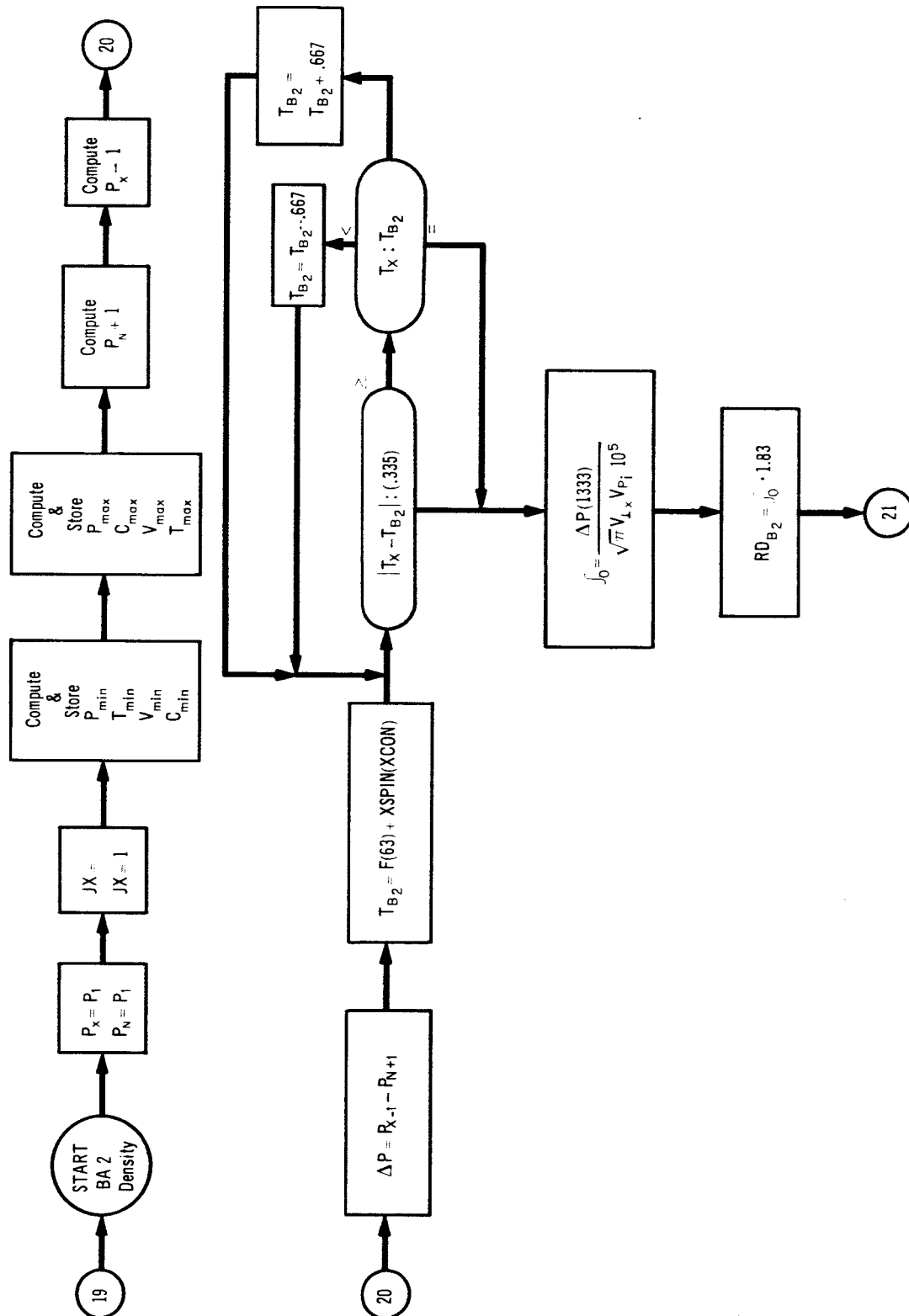


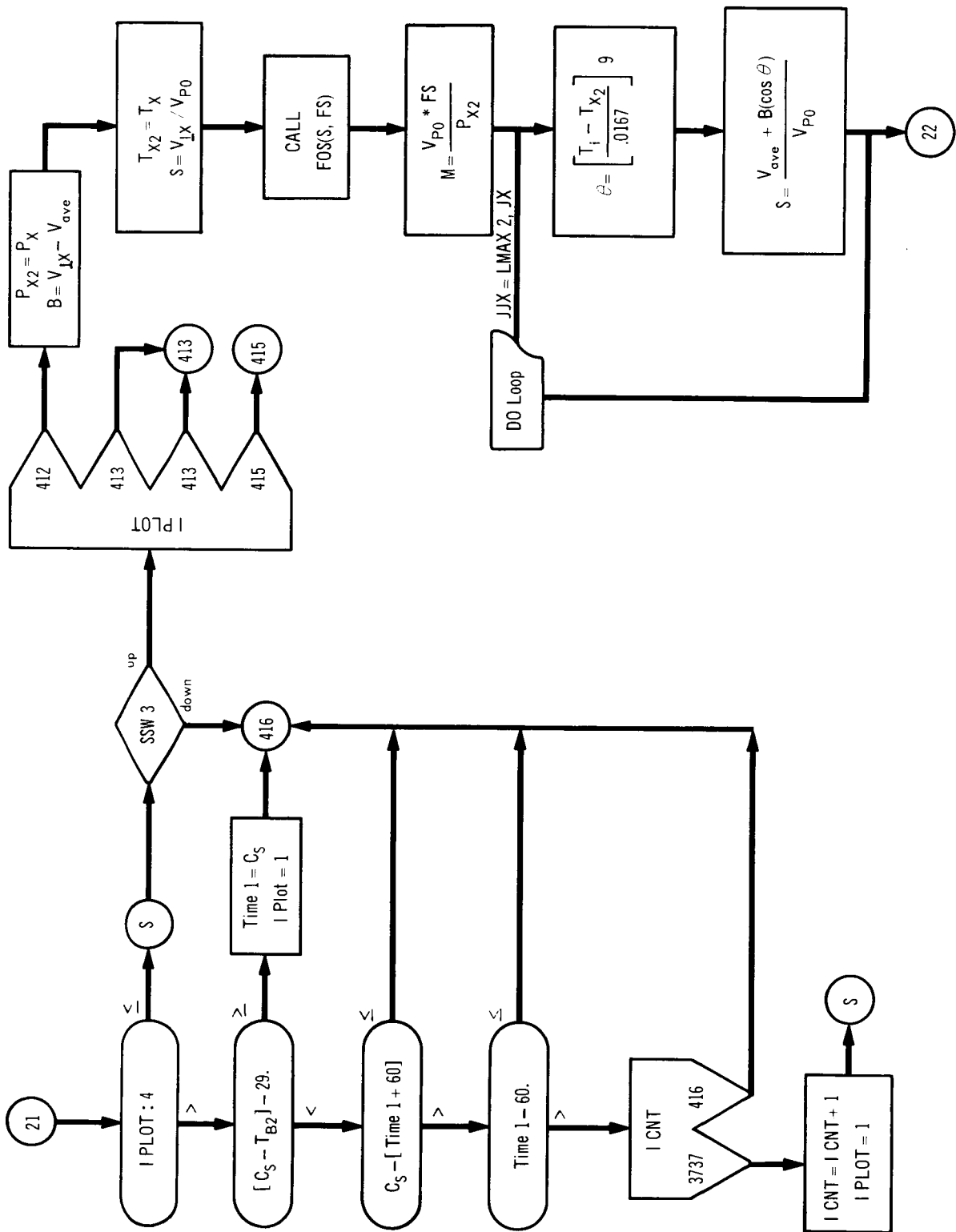


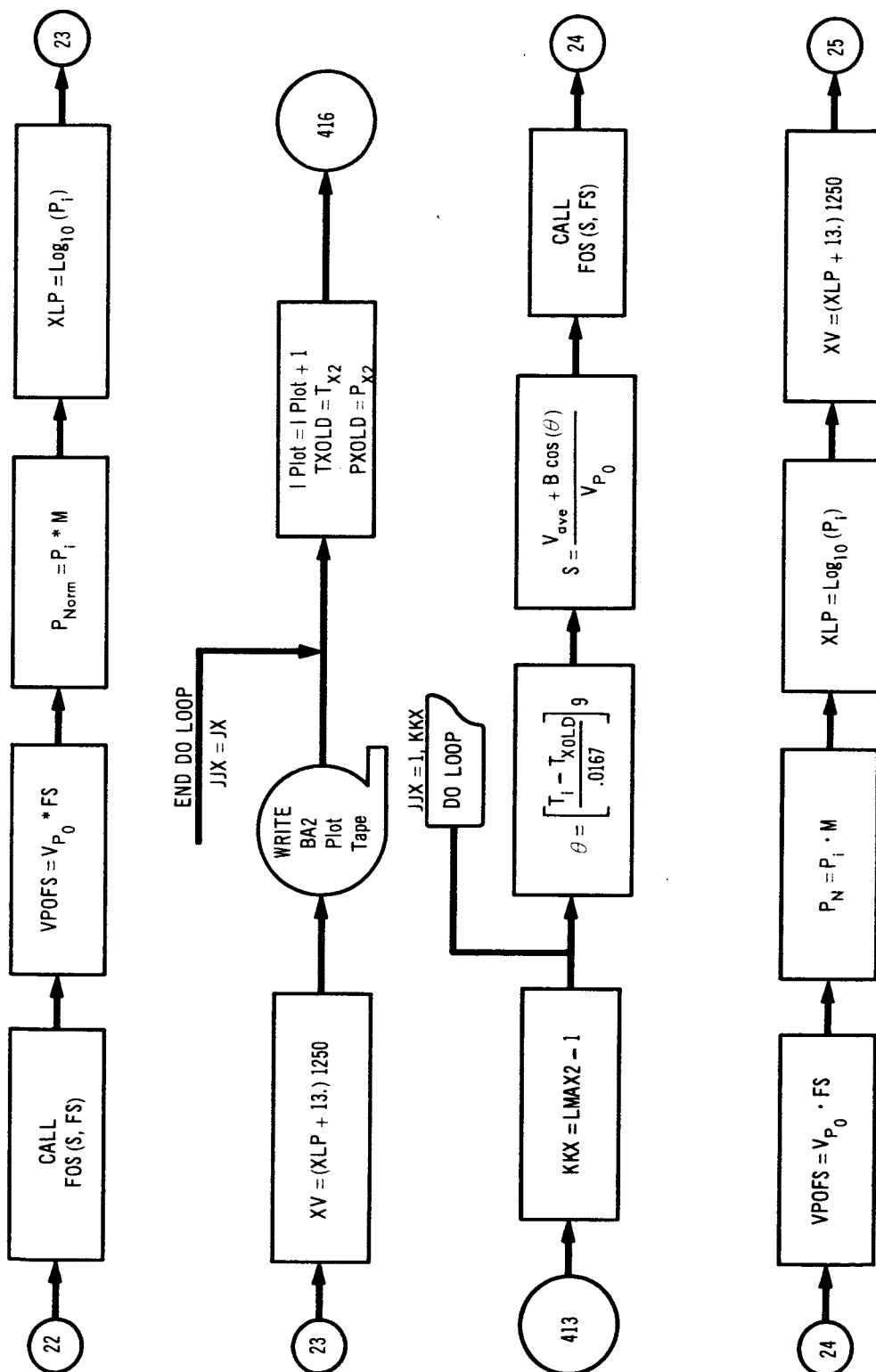


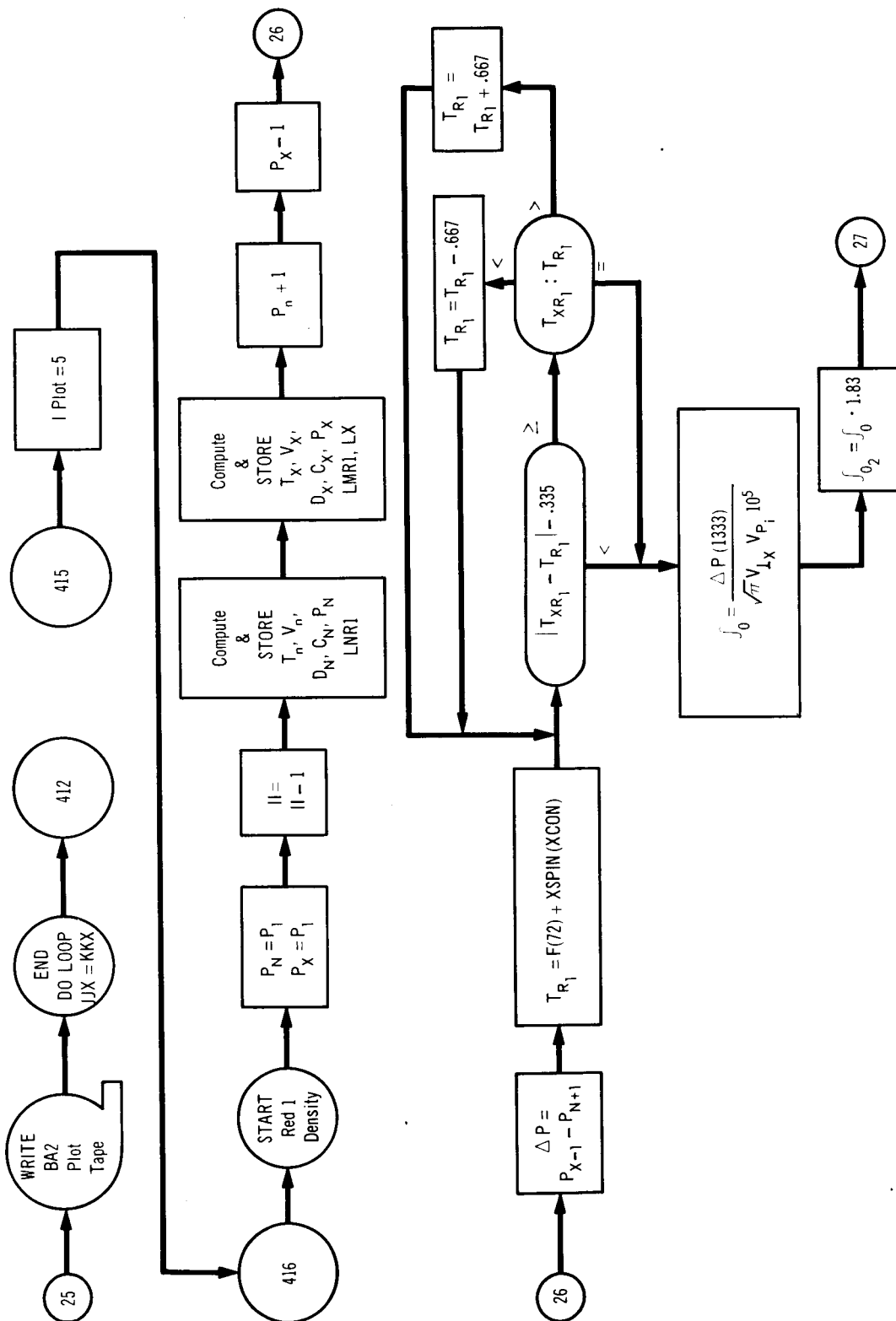


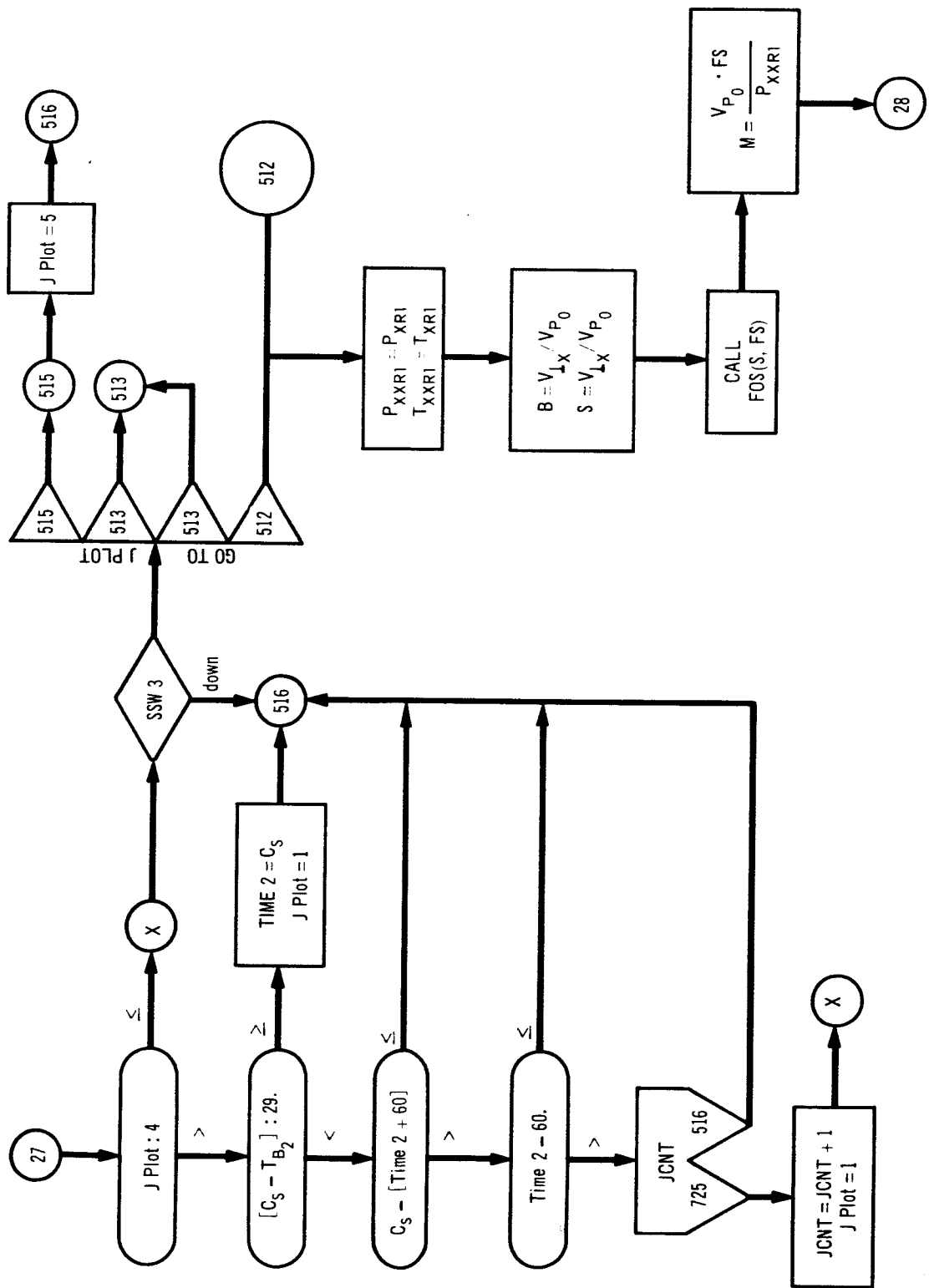


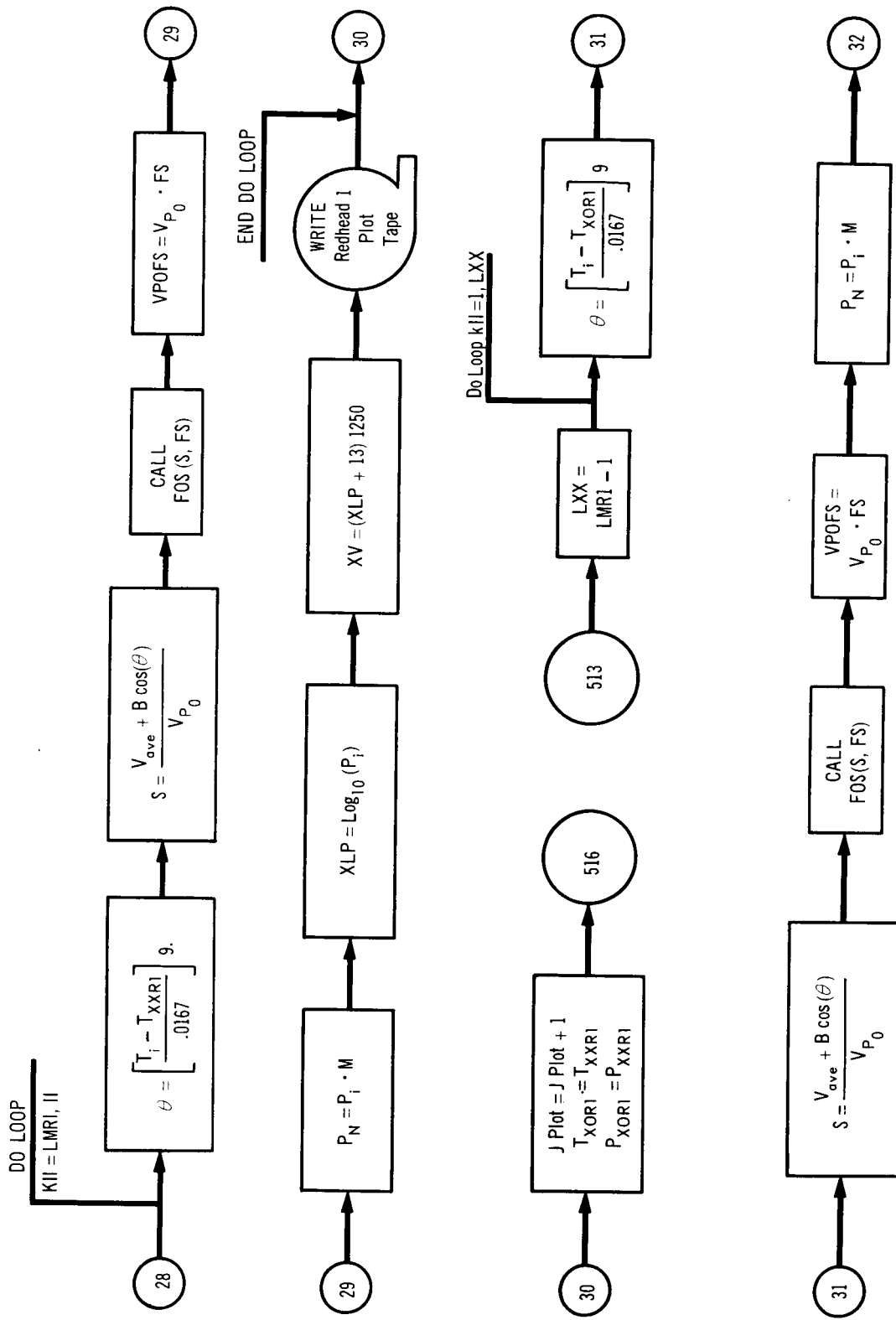


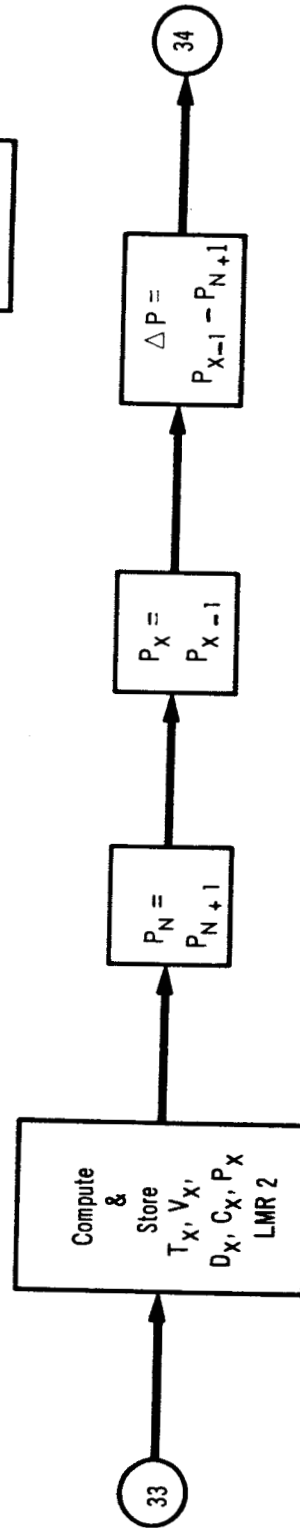
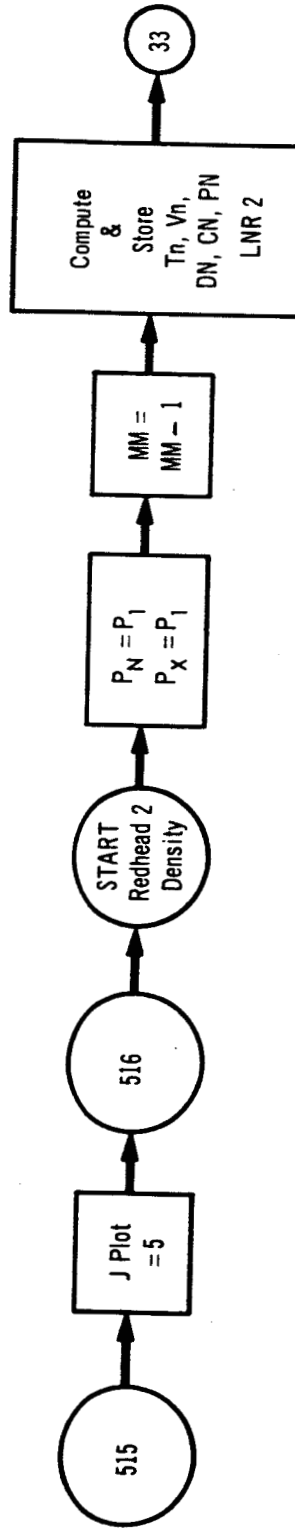
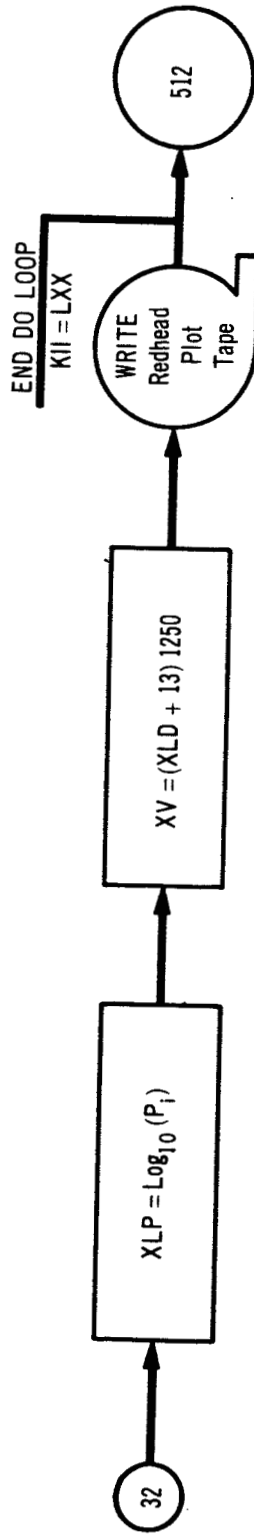


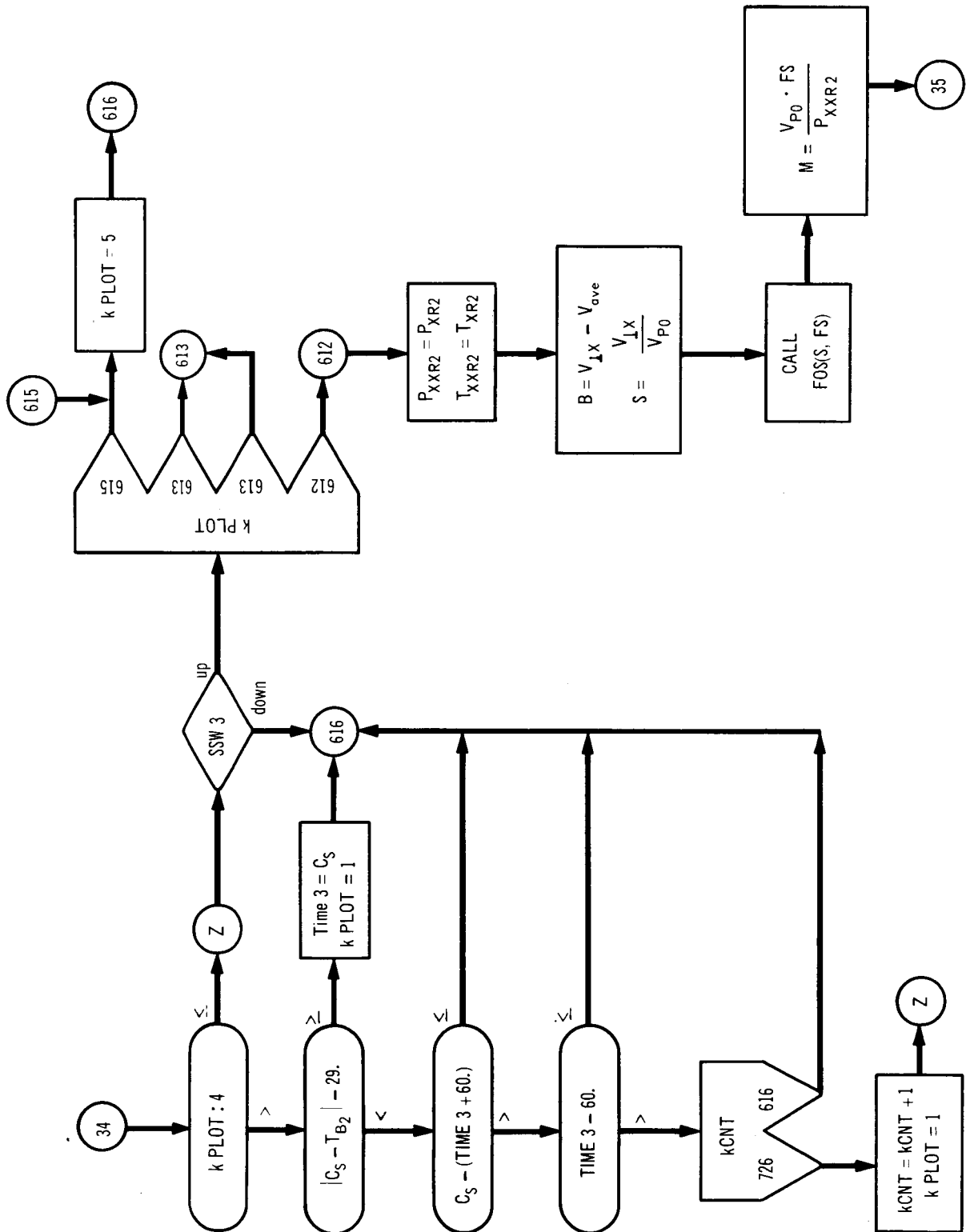


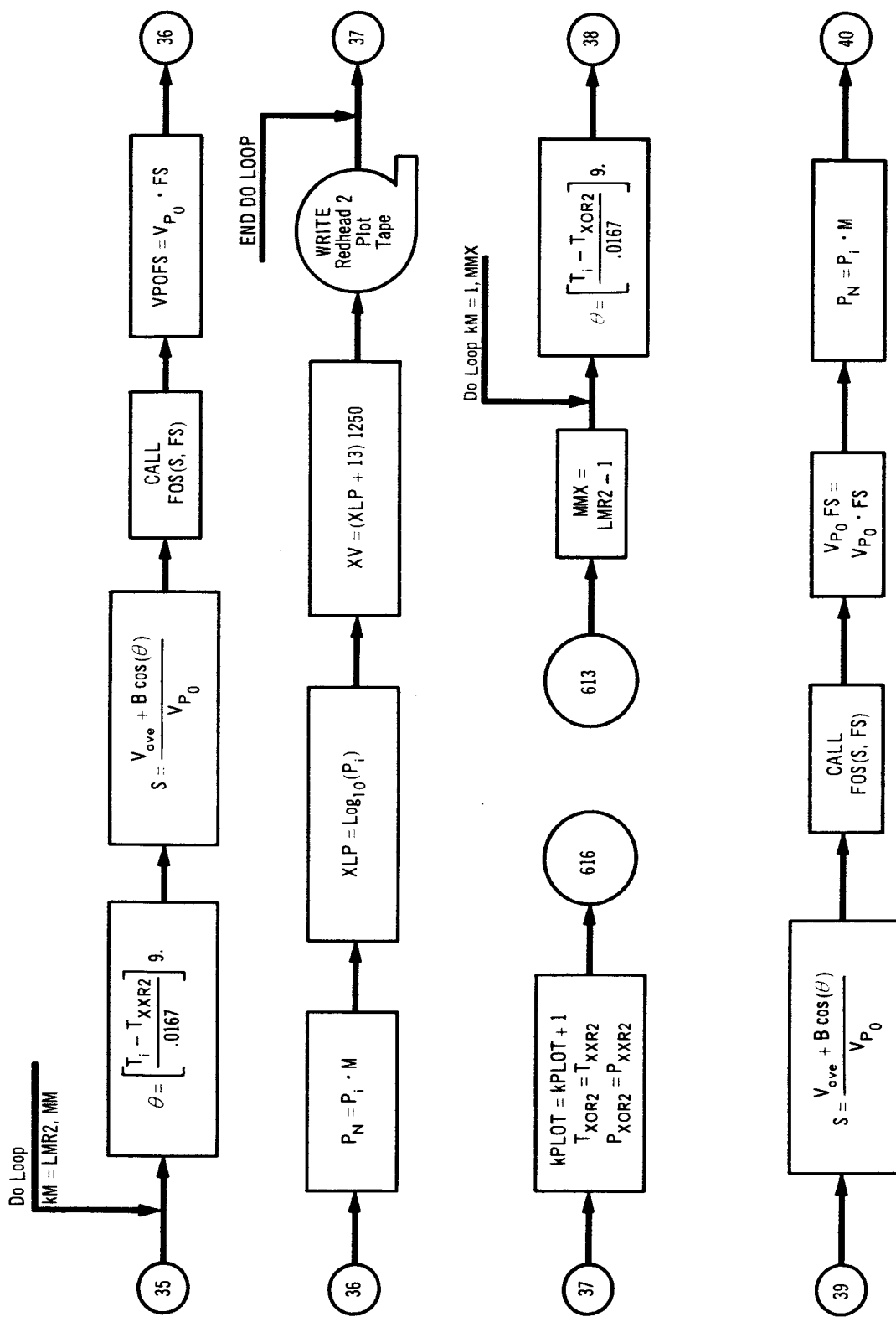


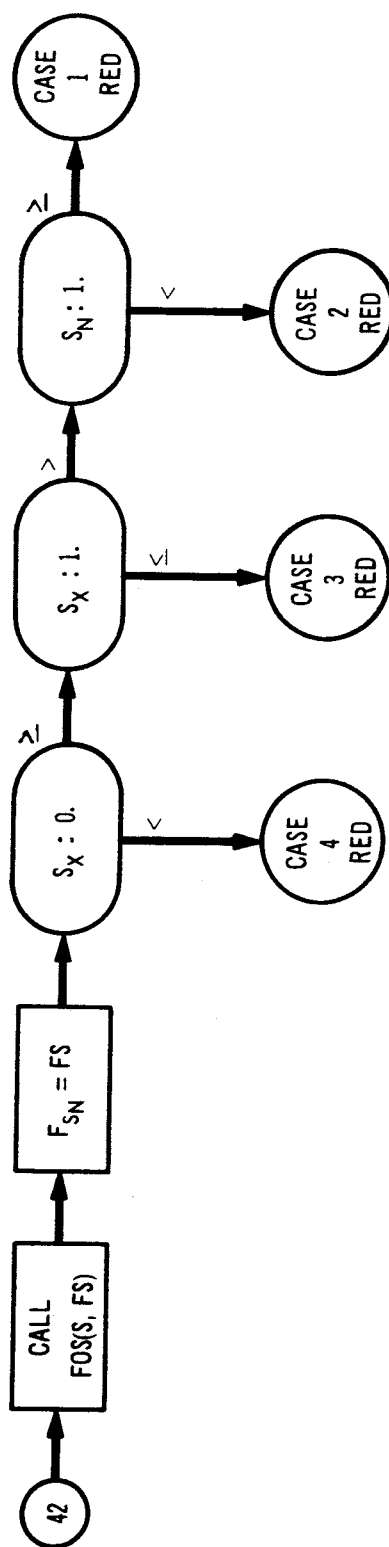
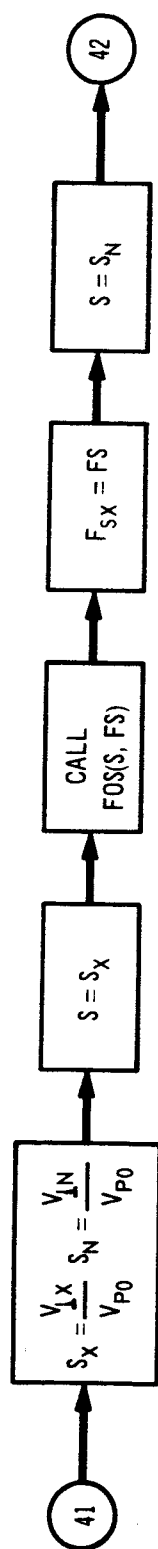


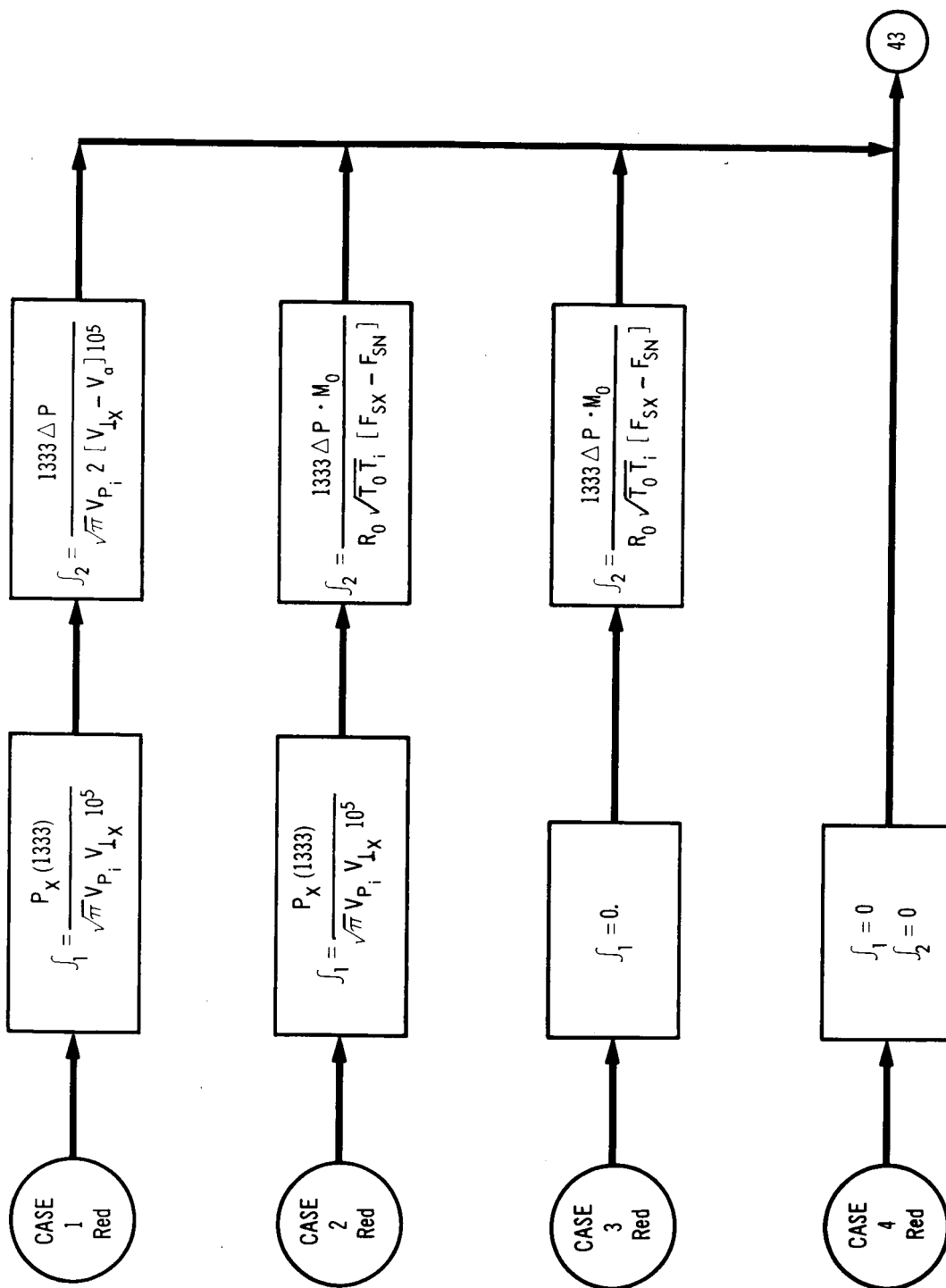


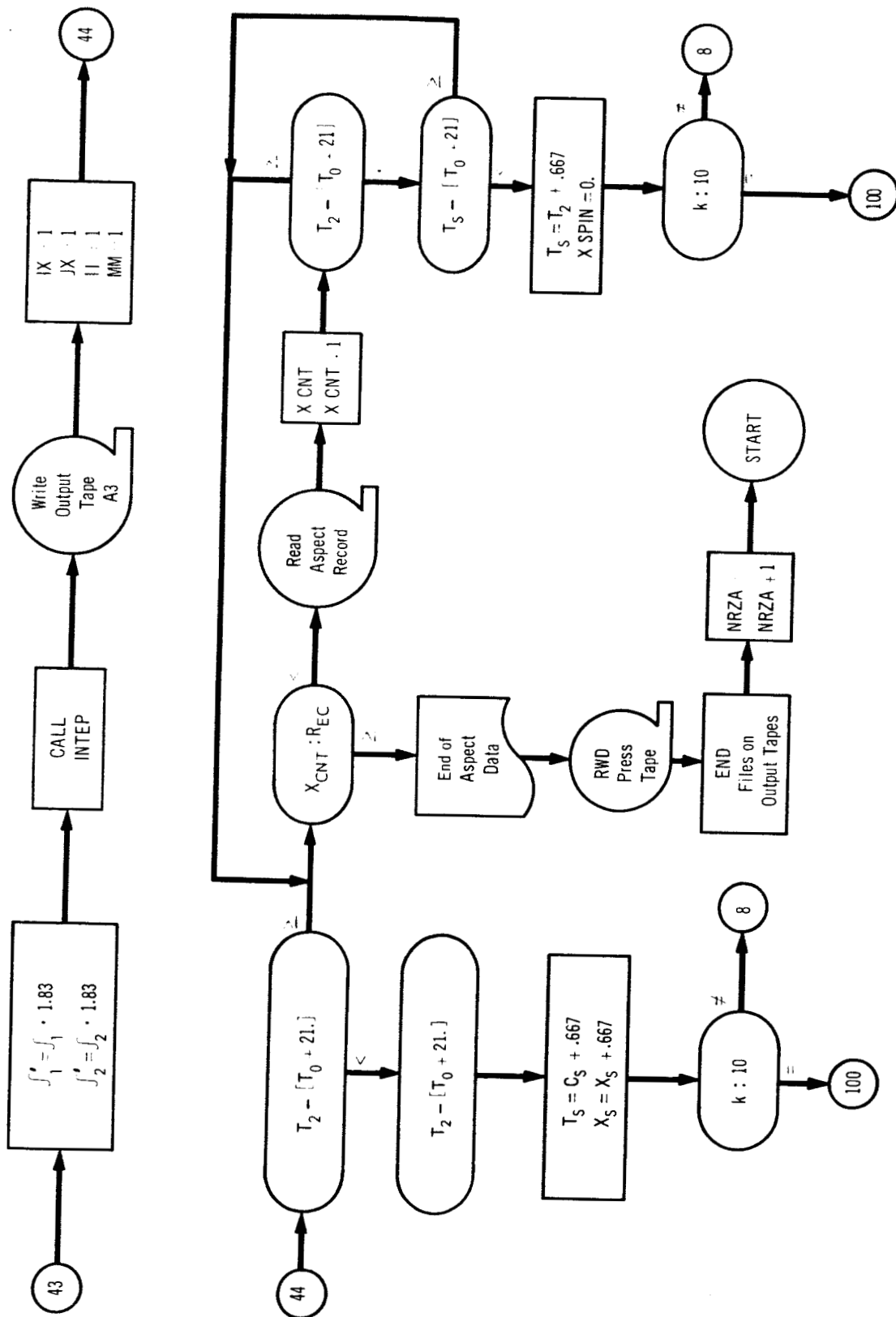












SUBROUTINES

November 1963

Program Write Up

0. Programmer—A. O. Forehand
1. Program Name—SUBROUTINE FOS
2. Programming System—FORTRAN II
3. General Description—

This subroutine computes the value of the Thermal Transpiration Function, defined by:

$$F(s) = e^{-s^2} + s \sqrt{\pi} (1 + \operatorname{erf}(s))$$

where s is the given independent variable and erf is the error function.

4. Calling Sequence—

CALL FOS (S, FS) where S is the independent variable taken as input to the routine and FS is the value of the function, $F(S)$.

5. Mathematical Description of the Computation

- (1) Definitions and relations

$$*F(s) = e^{-s^2} + s \sqrt{\pi} (1 + \operatorname{erf}(s))$$

where

$$\operatorname{erf}(s) = \frac{2}{\sqrt{\pi}} \int_0^s e^{-x^2} dx.$$

Substituting this value for $\operatorname{erf}(s)$ in * yields

$$F(s) = e^{-s^2} + s \sqrt{\pi} + 2s \int_0^s e^{-x^2} dx$$

Since the integral in the above expression is an odd function we see that

$$F(-s) = e^{-s^2} - s\sqrt{\pi} + 2s \int_0^s e^{-x^2} dx$$

or

$$**F(-s) = F(s) - 2s\sqrt{\pi}$$

Since for large positive values of s , e^{-s^2} is small and $\operatorname{erf}(s)$ is nearly equal to 1, then $2s\sqrt{\pi}$ is a good approximation to $F(s)$ in this case.

Since by $**F(s) = 2s\sqrt{\pi} + F(-s)$ we see that the error in this approximation is exactly equal to $F(-s)$.

(2) Evaluation of $\int_0^s e^{-x^2} dx$

Expanding e^{-x^2} in a Taylor's series and integrating termwise yields

$$s - \frac{s^3}{3.1!} + \frac{s^5}{5.2!} - \frac{s^7}{7.3!} + \dots$$

This series converges for all values of s but the number of terms required for accuracy becomes excessive as $|s|$ increases.

This difficulty is overcome by using this series only for $|s| \leq 2.5$ and using an asymptotic series for $|s| > 2.5$.

(a) The asymptotic series T

(1) Define $n = (\text{largest integer} \leq s^2)$

(2) Define $t = 2s^2$

Then the asymptotic series T is defined by

$$T = \frac{1}{t} - \frac{1.3}{t^2} + \frac{1.3.5}{t^3} - \dots + (-1)^{n+1} \frac{1.3.5 \dots (2n-1)}{t^n}$$

(b) Expression of the integral in terms of T

Case I. $s > 2.5$

$$\int_0^s e^{-x^2} dx = \frac{\sqrt{\pi}}{2} - \frac{e^{-s^2}}{2s} (1 - T)$$

Substituting this expression back into the equation for F(s) gives

$$\begin{aligned} F(s) &= e^{-s^2} + s \sqrt{\pi} + 2s \left[\frac{\sqrt{\pi}}{2} - \frac{e^{-s^2}}{2s} (1 - T) \right] \\ &= 2s \sqrt{\pi} + e^{-s^2} T \end{aligned}$$

Case II. $s < -2.5$

$$\int_0^s e^{-x^2} dx = -\frac{\sqrt{\pi}}{2} - \frac{e^{-s^2}}{2s} (1 - T)$$

This expression substituted into the F(s) equation yields:

$$\begin{aligned} F(s) &= e^{-s^2} + s \sqrt{\pi} + 2s \left[-\frac{\sqrt{\pi}}{2} - \frac{e^{-s^2}}{2s} (1 - T) \right] \\ &= e^{-s^2} T \end{aligned}$$

6. References

For a complete discussion of the integral involved here and the derivation of the asymptotic series see Numerical Math. Analysis by J. B. Scarborough. (Pages 406-409 of the 4th edition.)

March 1965

Program Writeup

0. Programmer—C. Hanley
1. Program Name—SUBROUTINE MATCH
2. Programming System—FORTRAN II
3. General Description—

Subroutine Match reads the identification record of the experiment data tape and the aspect tape and proceeds to compare the appropriate aspect data with the experimental data tape for each satellite pass of data. The station number, month, day, hours, and minutes are the ID parameters to be matched. All parameters are to be matched otherwise processing of the data is deleted and an appropriate message is printed out.

The subroutine (Match) is called into operation by the following program statement:

CALL MATCH (NEDI, N)

where NEDI is the satellite pass number;

N = output parameter which tells if match has occurred

N = 0 Match has occurred

N = 1 Match has not occurred

Program Writeup

0. Programmer—C. Hanley
1. Program Name—SUBROUTINE INTEP
2. Programming System—FORTRAN II
3. General Description—

Subroutine INTEP is a routine used for interpolating the altitude, latitude, longitude and local sun time parameters on the aspect tape. The above parameters are given once every 22 sec. and it is required to have the above parameter values every spin period (.667 sec.).

The subroutine (INTEP) is called into operation by the following FORTRAN II program statement:

CALL INTEP (TS, NREC, YALT, YLAT, YLONG, YLST)

INPUT	{	TS*	=	time
PARAMETERS		NREC	=	number of records

OUTPUT PARAMETERS	{	YALT	=	altitude
		YLAT	=	latitude
		YLONG	=	longitude
		YLST	=	local sun time

Program Writeup

0. Programmer—A. O. Forehand
1. Program Name—SUBROUTINE GTMC
2. Programming System—FORTRAN II
3. General Description—

This FORTRAN II subroutine converts geographic coordinates (latitude, longitude) to geomagnetic coordinates (latitude, longitude). The coordinates in each case are in degrees.

Equations

Definition of Symbols (all refer to degrees)

- λ latitude (input)
- ϕ longitude (input)
- θ co-latitude ($90^\circ - \lambda$)
- Φ geomagnetic latitude (output)
- Λ geomagnetic longitude (output)
- Θ geomagnetic co-latitude ($90^\circ - \Phi$)
- θ_1 co-latitude of north magnetic pole (program constant)
- ϕ_1 longitude of north magnetic pole (program constant)

The geomagnetic position is determined by the equations:

$$\sin \Phi = \cos \theta_1 \sin \lambda + \sin \theta_1 \cos \lambda \cos (\phi - \phi_1)$$

$$\cos \Lambda = \frac{\cos \theta_1 \cos \Theta - \cos \theta}{\sin \theta_1 \sin \Theta}$$

NOTE: (θ_1, ϕ_1) are defined in the program to be $(11.494^\circ, -69.68^\circ)$. These values may be re-determined by the user before compilation if desired.

Calling Sequence

CALL GTMC (A, B, C, D)

where

A and B are input; C and D are output.

A, B are latitude, longitude

C, D are geomagnetic latitude, longitude

Restrictions

The input coordinates should satisfy the following inequalities:

$$-90^\circ \leq A \leq 90^\circ$$

$$-180^\circ \leq B \leq 180^\circ$$

C and D need not be separate locations from A and B i.e.,

CALL GTMC (A, B, A, B) is acceptable.

System subroutines MINIF, ABSF, SIGNF, SQRTF, SIN, COS, ASINE, ACOSD are used.

NOTE: This routine is a modification of Subroutine GCON obtained from the Fields and Plasmas Branch, GSFC. The original routine converts coordinates in either direction.

Definitions of Program Symbols

<u>Program Symbol</u>	<u>Definition</u>
A	λ
B	ϕ

<u>Program Symbol</u>	<u>Definition</u>
C	Φ
D	Λ
THK	θ_1
PHK	ϕ_1
SK	$\text{Sin } \theta_1$
CK	$\text{Cos } \theta_1$
E	latitude in radians
CT	$\text{sin } \lambda (= \text{Cos } \theta)$
DEL	$(\phi - \phi_1)$ (if $\phi \leq 180^\circ$)
COS T	$\text{Cos } \Theta (= \text{Sin } \Phi)$
SIN T	$\text{Sin } \Theta (= \text{Cos } \Phi)$
ARG	$\text{Cos } (180^\circ - \Lambda)$ for $0 \leq \text{DEL} \leq 180^\circ$ $\text{Cos } (\Lambda + 180^\circ)$ for $\text{DEL} < 0$ $\text{DEL} > 180^\circ$.

March 1965

Program Writeup

0. Programmer—C. Hanley
1. Program Name—SUBROUTINE DEN
2. Programming System—FAP
3. General Description—

This binary subroutine (DEN) sets tape units B6, A6, C5, and C6 to low density when called into the program. Subroutine DEN is called into operation by the following statement:

CALL DEN

OPERATING INSTRUCTIONS

Sense Switches

1. Sense Switch 1 and 2

SSW 1 and 2 are always in a normal position, which is the up position. These Sense Switches were originally put into the program for a purpose that never materialized. They were never deleted because the idea might have been incorporated at anytime.

2. Sense Switch 3

When Sense Switch 3 is in the normal position the program will write three pressure plot tapes on channels B6, C5, C6 respectively. In the down position no plot output tapes will be written.

3. Sense Switch 4

In the normal position the optional output (T, V, C, P for every point) will be written out on tape. For no optional output SSW 4 must be down.

DATA CARDS

There are 14 data cards for each pass or orbit of the satellite to be processed. A blank card following the data cards indicates end of data and end of job. The format for these cards is as follows:

<u>Card No.</u>	<u>Col.</u>	<u>Fortran Symbol</u>	<u>Job Format</u>
1	1-14	blank	—
	15-18	NEDI	I4
	19-28	blank	—
	29-32	NORB	I4
2	1-72	BI	9E8.2
3	1-72	BI	9E8.2
4	1-72	VC1	9F8.6
5	1-56	VC2	7F8.6
	59-72	blank	—
6	1-72	RI	9E8.2

<u>Card No.</u>	<u>Col.</u>	<u>Fortran Symbol</u>	<u>Job Format</u>
7	1-56	RI2	7E8.2
	57-72	blank	—
8	1-6	XHL	F6.3
	7-12	XML	F6.3
	13-18	XLL	F6.3
	19-24	X2HL	F6.3
	25-30	X2ML	F6.3
	31-36	X2LL	F6.3
	37-72	blank	—
9	1-8	TO	F8.2
	9-16	TI	F8.2
	17-24	WO	F8.2
	25-32	WI	F8.2
	33-35	HID	A3
	36-72	blank	—
*10	1-6	XHF	F6.3
	7-12	XMF	F6.3
	13-18	XLf	F6.3
	19-24	X2HF	F6.3
	25-30	X2MF	F6.3
	31-36	X2LF	F6.3
	37-72	blank	—
*11	1-54	BV1	9F6.3
	55-72	blank	—
*12	1-54	BV1	9F6.3
	55-72	blank	—
*13	1-54	BV2	9F6.3
	55-72	blank	—
*14	1-54	BV2	9F6.3
	55-72	blank	—
15	1-72	blank	—

*These cards are supplied for each pass by the MCP program.

TAPE FORMATS

Input Data Tapes

Pressure Data Tape

The pressure data tape is a binary tape with standard FORTRAN record lengths of 255 words, the first record being an identification record of each orbit containing satellite number, month, day, year, station number, and analog tape number for each recorded orbit. Following the orbit identification record there are data records of 255 words containing the selected DC voltage for all four gauges. Following the data words is a sentinel, which is a record of all nines (9999's) indicating the end of data.

Aspect Data Tape

The aspect data tape is a binary tape with standard FORTRAN records of 255 words. Each aspect tape has numerous passes of aspect data. Each pass consists of an identification record of 209 words containing satellite number, month, day, year, station number and analog tape number. Words 1-200 contain orbital tape input data which are not relevant to the pressure density program. Following the identification record (ID) are data records each containing 141 words in length. Every pass of data is separated by a record of nines (9999's) to indicate end of data.

Output Data Tapes

P-D Output Tape

The pressure-density output tape contains all computed parameters for each experiment gauge, as requested by the experimenter.

The output tape is in the BCD mode. This tape, containing records of varying lengths, is placed on unit A3.

Density Plot Tape

The density plot tape, contains aspect and density values for all gauges and is formatted for plotting purposes. (S-C-4020 is used to plot these values.)

The density plot tape contains records of variable lengths and is in the BCD mode. It is placed on unit A6.

Pressure Plot Tapes

The pressure plot output tapes contain the raw pressure values, normalized pressure, time, and other parameters formatted for plotting purposes.

The pressure plot tapes are in the BCD mode and contain records of varying lengths. These tapes are placed on units B6, C5, and C6.

PRESSURE TAPE FORMAT

630403
AOPB-WPH

S-6 PRESSURE GAUGE BINARY TAPE FORMAT

THE PRESSURE GAUGE BINARY TAPE CONSISTS OF 1 TITLE RECORD, 1 OR MORE DATA RECORDS, 2 EOF'S.

TITLE RECORD

WORD NO.	DESCRIPTION
0	STANDARD FORTRAN RECORD SIZE INDICATOR. (FIXED POINT) *
1	SATELLITE NO. = 6
2	MONTH DATE OF FIRST DATA FRAME
3	DAY ON S-6 BINARY TELEMETRY
4	YEAR TAPE
5	STATION NO.
6	ANALOG TAPE NO.
7	IRRELEVANT
8	S-6 PRESSURE GAUGES I.D. = 60000004
9-255	IRRELEVANT

* THE RECORD SIZE INDICATOR = 00377000001 OCTAL IS THE ONLY FIXED POINT NUMBER IN EACH RECORD.

PRESSURE TAPE FORMAT

DATA RECORD

WORD NO.	DESCRIPTION **	
0	STANDARD FORTRAN RECORD SIZE INDICATOR. (FIXED POINT) *	
1	DAY COUNT OF YEAR	TIME OF
2	MILLISECONDS OF DAY	FRAME
3- 5	CHS.3,19,35	DC (VOLTS) BAYARD ALPERT 1
6- 8	CHS.4,20,36	AC (VOLTS)
9-11	CHS.5,21,37	DC (VOLTS) BAYARD ALPERT 2
12-14	CHS.6,22,38	AC (VOLTS)
15-17	CHS.10,26,42	(VOLTS) REDHEAD 1
18-20	CHS.11,27,43	(VOLTS) REDHEAD 2
21	SUBCOM POSITION	
22	CH.31	(VOLTS) CONTENTS OF CHS.31 AND 33
23	CH.31	(DEGREES) ARE INTERPRETED BY THE
24	CH.33	(VOLTS) VALUE OF THE SUBCOM POS-
25	CH.33	(DEGREES) ITION. (SEE ATTACHMENT)
26-50	NEXT FRAME OF DATA IN SAME FORM AS 1-25	
*	*	
*	*	
*	*	
226-250	TENTH FRAME OF RECORD	
251-255	SPARES	

** SEE ATTACHMENT FOR VALUES SIGNIFIING END OF DATA OR IRRELEVANT DATA.

ASPECT TAPE FORMAT

630508
AOPB-MLR

S-6 ASPECT AND SATELLITE POSITION DATA BINARY TAPE

THE S-6 ASPECT AND SATELLITE POSITION DATA BINARY TAPE CONSISTS OF 1 TITLE RECORD, 1 OR MORE DATA RECORDS, 2 EOF'S. THERE IS TO BE ONE DATA RECORD FOR EACH TIME BLOCK IN THE TELEMETRY DATA IDENTIFIED IN WORDS 201-206 OF THE TITLE RECORD.*

TITLE RECORD

WORD NO.	FORM	DESCRIPTION
0	FIXED PT.	STANDARD FORTRAN RECORD SIZE INDICATOR. =000321000001 OCTAL IN THE TITLE RECORD ON THIS TAPE. THIS INDICATES A TOTAL WORD COUNT PER RECORD OF 209 WORDS.
1-200	FLOATING PT.	INFORMATION FROM WORDS 1-200 OF ORBITAL TAPE INPUT.
201	FLOATING PT.	SATELLITE NO. = 6
202	FLOATING PT.	MONTH
203	FLOATING PT.	DATE OF FIRST DATA FRAME
204	FLOATING PT.	DAY ON S-6 BINARY TELEMETRY
		YEAR TAPE
205	FLOATING PT.	STATION NO.
206	FLOATING PT.	ANALOG TAPE NO.
207	FLOATING PT.	IRRELEVANT
208	FLOATING PT.	S-6 ASPECT I.D. = 600000000
209	FLOATING PT.	IRRELEVANT

* NOMINALLY, A TIME BLOCK IS 21 SEC., I.E., 7 SEC. MULTIVIBRATOR CYCLE AND A 14 SEC. MULTIVIBRATOR CYCLE.

ASPECT TAPE FORMAT

DATA RECORD WORD NO.	FORM	DESCRIPTION
0	FIXED PT.	STANDARD FORTRAN RECORD SIZE INDICATOR. = 000215000001 OCTAL IN EACH DATA RECORD ON THIS TAPE. THIS INDICATES A TOTAL WORD COUNT PER RECORD OF 141 WORDS.
1	FLOATING PT.	DATE
2	FLOATING PT.	TIME OF DATA
3	FLOATING PT.	DAY COUNT OF YEAR
		SECONDS OF DAY
4	FLOATING PT.	X SATELLITE POSITION
5	FLOATING PT.	Y VECTOR IN KM.
6	FLOATING PT.	Z
7	FLOATING PT.	XDOT SATELLITE VELOCITY
8	FLOATING PT.	YDOT VECTOR IN KM./SEC.
9	FLOATING PT.	ZDOT
10	FLOATING PT.	LONGITUDE SUBSATELLITE
11	FLOATING PT.	LATITUDE POSITION IN DEGREES
12	FLOATING PT.	ALTITUDE IN KM.
13	FLOATING PT.	LOCAL APPARENT TIME IN HOURS
14	FLOATING PT.	MAGNITUDE OF POSITION VECTOR IN KM.
15	FLOATING PT.	MAGNITUDE OF VELOCITY VECTOR IN KM./SEC.
16	FLOATING PT.	POSITION VECTOR R.A. IN DEGREES
17	FLOATING PT.	POSITION VECTOR DECLINATION IN DEGREES
18	FLOATING PT.	VELOCITY VECTOR R.A. IN DEGREES
19	FLOATING PT.	VELOCITY VECTOR DECLINATION IN DEGREES
20	FLOATING PT.	SUN VECTOR R.A. IN DEGREES
21	FLOATING PT.	SUN VECTOR DECLINATION IN DEGREES
22	FLOATING PT.	MOMENTUM VECTOR R.A. IN DEGREES
23	FLOATING PT.	MOMENTUM VECTOR DECLINATION IN DEGREES
24	FLOATING PT.	ASPECT SENSOR R.A. IN DEGREES
25	FLOATING PT.	ASPECT SENSOR DECLINATION IN DEGREES
26	FLOATING PT.	ETP1 SENSOR R.A. IN DEGREES
27	FLOATING PT.	ETP1 SENSOR DECLINATION IN DEGREES
28	FLOATING PT.	ETP2 SENSOR R.A. IN DEGREES
29	FLOATING PT.	ETP2 SENSOR DECLINATION IN DEGREES

ASPECT TAPE FORMAT

30	FLOATING PT.	B.A.1 SENSOR R.A. IN DEGREES
31	FLOATING PT.	B.A.1 SENSOR DECLINATION IN DEGREES
32	FLOATING PT.	B.A.2 SENSOR R.A. IN DEGREES
33	FLOATING PT.	B.A.2 SENSOR DECLINATION IN DEGREES
34	FLOATING PT.	M.S.1 SENSOR R.A. IN DEGREES
35	FLOATING PT.	M.S.1 SENSOR DECLINATION IN DEGREES
36	FLOATING PT.	M.S.2 SENSOR R.A. IN DEGREES
37	FLOATING PT.	M.S.2 SENSOR DECLINATION IN DEGREES
38	FLOATING PT.	R.H.1 SENSOR R.A. IN DEGREES
39	FLOATING PT.	R.H.1 SENSOR DECLINATION IN DEGREES
40	FLOATING PT.	R.H.2 SENSOR R.A. IN DEGREES
41	FLOATING PT.	R.H.2 SENSOR DECLINATION IN DEGREES
42	FLOATING PT.	ASPECT SENSOR A* IN DEGREES
43	FLOATING PT.	ETP1 SENSOR A* IN DEGREES
44	FLOATING PT.	ETP2 SENSOR A* IN DEGREES
45	FLOATING PT.	B.A.1 SENSOR A* IN DEGREES
46	FLOATING PT.	B.A.2 SENSOR A* IN DEGREES
47	FLOATING PT.	M.S.1 SENSOR A* IN DEGREES
48	FLOATING PT.	M.S.2 SENSOR A* IN DEGREES
49	FLOATING PT.	R.H.1 SENSOR A* IN DEGREES
50	FLOATING PT.	R.H.2 SENSOR A* IN DEGREES
51	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ASPECT S. MAX. RAM V
52	FLOATING PT.	ASPECT SENSOR MAX. RAM VELOCITY IN KM./SEC.
53	FLOATING PT.	ASPECT SENSOR MAX. RAM A* IN DEGREES
54	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ETP1 S. MAX. RAM V.
55	FLOATING PT.	ETP1 SENSOR MAX. RAM VELOCITY IN KM./SEC.
56	FLOATING PT.	ETP1 SENSOR MAX. RAM A* IN DEGREES
57	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ETP2 S. MAX. RAM V.
58	FLOATING PT.	ETP2 SENSOR MAX. RAM VELOCITY IN KM./SEC.
59	FLOATING PT.	ETP2 SENSOR MAX. RAM A* IN DEGREES
60	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF B.A.1 S. MAX. RAM V.
61	FLOATING PT.	B.A.1 SENSOR MAX. RAM VELOCITY IN KM./SEC.
62	FLOATING PT.	B.A.1 SENSOR MAX. RAM A* IN DEGREES
63	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF B.A.2 S. MAX. RAM V.
64	FLOATING PT.	B.A.2 SENSOR MAX. RAM VELOCITY IN KM./SEC.
65	FLOATING PT.	B.A.2 SENSOR MAX. RAM A* IN DEGREES
66	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF M.S.1 S. MAX. RAM V.
67	FLOATING PT.	M.S.1 SENSOR MAX. RAM VELOCITY IN KM./SEC.

ASPECT TAPE FORMAT

68	FLOATING PT.	M.S. SENSOR MAX. RAM A* IN DEGREES
69	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF M.S.2 S. MAX. RAM V.
70	FLOATING PT.	M.S.2 SENSOR MAX. RAM VELOCITY IN KM./SEC.
71	FLOATING PT.	M.S.2 SENSOR MAX. RAM A* IN DEGREES
72	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF R.H.1 S. MAX. RAM V.
73	FLOATING PT.	R.H.1 SENSOR MAX. RAM VELOCITY IN KM./SEC.
74	FLOATING PT.	R.H.1 SENSOR MAX. RAM A* IN DEGREES
75	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF R.H.2 S. MAX. RAM V.
76	FLOATING PT.	R.H.2 SENSOR MAX. RAM VELOCITY IN KM./SEC.
77	FLOATING PT.	R.H.2 SENSOR MAX. RAM A* IN DEGREES
78	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ASP.S. MIN. RAM V.
79	FLOATING PT.	ASPECT SENSOR MIN. RAM VELOCITY IN KM./SEC.
80	FLOATING PT.	ASPECT SENSOR MIN. RAM A* IN DEGREES
81	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ETP1 S. MIN. RAM V.
82	FLOATING PT.	ETP1 SENSOR MIN. RAM VELOCITY IN KM./SEC.
83	FLOATING PT.	ETP1 SENSOR MIN. RAM A* IN DEGREES
84	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ETP2 S. MIN. RAM V.
85	FLOATING PT.	ETP2 SENSOR MIN. RAM VELOCITY IN KM./SEC.
86	FLOATING PT.	ETP2 SENSOR MIN. RAM A* IN DEGREES
87	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF BA 1 S. MIN. RAM V.
88	FLOATING PT.	B.A.1 SENSOR MIN. RAM VELOCITY IN KM./SEC.
89	FLOATING PT.	B.A.1 SENSOR MIN. RAM A* IN DEGREES
90	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF BA 2 S. MIN. RAM V.
91	FLOATING PT.	B.A.2 SENSOR MIN. RAM VELOCITY IN KM./SEC.
92	FLOATING PT.	B.A.2 SENSOR MIN. RAM A* IN DEGREES
93	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF MS 1 S. MIN. RAM V.
94	FLOATING PT.	M.S.1 SENSOR MIN. RAM VELOCITY IN KM./SEC.
95	FLOATING PT.	M.S.1 SENSOR MIN. RAM A* IN DEGREES
96	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF MS 2 S. MIN. RAM V.
97	FLOATING PT.	M.S.2 SENSOR MIN. RAM VELOCITY IN KM./SEC.
98	FLOATING PT.	M.S.2 SENSOR MIN. RAM A* IN DEGREES
99	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF RH 1 S. MIN. RAM V.
100	FLOATING PT.	R.H.1 SENSOR MIN. RAM VELOCITY IN KM./SEC.
101	FLOATING PT.	R.H.1 SENSOR MIN. RAM A* IN DEGREES
102	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF RH 2 S. MIN. RAM V.
103	FLOATING PT.	R.H.2 SENSOR MIN. RAM VELOCITY IN KM./SEC.
104	FLOATING PT.	R.H.2 SENSOR MIN. RAM A* IN DEGREES
105	FLOATING PT.	ASPECT SENSOR AV. RAM VELOCITY IN KM./SEC.
106	FLOATING PT.	ETP1 SENSOR AV. RAM VELOCITY IN KM./SEC.
107	FLOATING PT.	ETP2 SENSOR AV. RAM VELOCITY IN KM./SEC.
108	FLOATING PT.	B.A.1 SENSOR AV. RAM VELOCITY IN KM./SEC.
109	FLOATING PT.	B.A.2 SENSOR AV. RAM VELOCITY IN KM./SEC.
110	FLOATING PT.	M.S.1 SENSOR AV. RAM VELOCITY IN KM./SEC.
111	FLOATING PT.	M.S.2 SENSOR AV. RAM VELOCITY IN KM./SEC.
112	FLOATING PT.	R.H.1 SENSOR AV. RAM VELOCITY IN KM./SEC.

ASPECT TAPE FORMAT

113	FLOATING PT.	R.H. SENSOR AV. RAM VELOCITY IN KM./SEC.
114	FLOATING PT.	ELAPSED T. IN SEC. OF DAY ASP. S. MIN. SUN ANG.
115	FLOATING PT.	ASPECT SENSOR MIN. SUN ANG. IN DEGREES
116	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ETP1 S. MIN SUN A.
117	FLOATING PT.	ETP1 SENSOR MIN. SUN ANGLE IN DEGREES
118	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF ETP2 S. MIN SUN A.
119	FLOATING PT.	ETP2 SENSOR MIN. SUN ANGLE IN DEGREES
120	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF BA 1 S. MIN SUN A.
121	FLOATING PT.	BA 1 SENSOR MIN. SUN ANGLE IN DEGREES
122	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF BA 2 S. MIN SUN A.
123	FLOATING PT.	BA 2 SENSOR MIN. SUN ANGLE IN DEGREES
124	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF MS 1 S. MIN SUN A.
125	FLOATING PT.	MS 1 SENSOR MIN. SUN ANGLE IN DEGREES
126	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF MS 2 S. MIN SUN A.
127	FLOATING PT.	MS 2 SENSOR MIN. SUN ANGLE IN DEGREES
128	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF RH 1 S. MIN SUN A.
129	FLOATING PT.	RH 1 SENSOR MIN. SUN ANGLE IN DEGREES
130	FLOATING PT.	ELAPSED T. IN SEC. OF DAY OF RH 2 S. MIN SUN A.
131	FLOATING PT.	RH 2 SENSOR MIN. SUN ANGLE IN DEGREES
132	FLOATING PT.	T SUB 0 IN SECONDS OF DAY
133	FLOATING PT.	T SUB F IN SECONDS OF DAY
134	FLOATING PT.	BETA, MOM. VECTOR-SUN OR MOON ANGLE IN DEG.
135	FLOATING PT.	THETA, PREC. CONE HALF ANGLE IN DEG.
136	FLOATING PT.	PHI DOT, EULERIAN PREC. VEL. IN DEG./SEC.
137	FLOATING PT.	PSI DOT, EULERIAN SPIN VEL. IN DEG./SEC.
138	FLOATING PT.	ROTATION RATE IN DEGREES/SEC.
139	FLOATING PT.	A SUB 0
140	FLOATING PT.	B SUB 0
141	FLOATING PT.	MEASURE OF ASPECT RELIABILITY IN DEGREES
142	FLOATING PT.	1 OR 0
		0 = RA & DEC. SUN.
		1 = RA & DEC. MOON

NOTE-

1. A* MEANS ANGLE BETWEEN THE GIVEN SENSOR AND THE VELOCITY VECTOR

END OF FILE

2 EOF'S FOLLOW LAST DATA RECORD.

SAMPLE PROGRAM OUTPUT

CDIT = 327 JARIT = 711

SATELLITE NU. = 6.
 PCATH = 5.
 CAY = 20.
 YEAR = 67.
 STATION NU. = 10.
 ANALOG TAPE NU. = 30.
 PRESSURE GAUGES ID = 60000004.

SATELLITE S6.

DATA ANALYSIS

STATION - WCMHRA DATE 5-20-63.
 ALTITUDE RANGE (KM) 910.57 TO 709.86
 LATITUDE RANGE (DEG.) -40.62 TO -30.92
 GEOMAGNETIC LAT (DEG.) -57.35 TO -46.14
 LONGITUDE RANGE (DEG.) 131.22 TO 144.09
 GEOMAGNETIC LONG(DEG.) -153.10 TO -140.10
 LOCAL TIME (HRS) 1.09 TO 2.00

TIME (GMT)

FROM 140.DAYS 16 HRS 16 MIN 5.033 SEC
 TO 140.DAYS 16 HRS 20 MIN 16.924 SEC

TIME - HRS =16 MIN =16 SEC =59.141
 10A1 0.189 0.285 0.495 0.611 0.721 0.859 1.065 1.172 1.365
 20A1 1.503 1.808 2.195 2.365 2.955 3.330 3.756 4.211 4.686
 16A2 -0.212-0.123 0.049 0.212 0.305 0.418 0.639 0.790 0.985
 20A2 1.164 1.488 1.868 2.170 2.538 2.889 3.307 3.720 4.235

BAYARD ALPERT 2 DC SHIFT = .075
 RM1 - 2.75 RM2 - 3.22

FLIGHT CAL 4.663 3.353 1.089 4.983 3.635 2.161

TO =1000.000 TI = 313.000 MO = 16.000 MI = 16.000

TORR/AMP 1 = 19.500 TORR/AMP 2 = 23.900

PRESSURE GAUGES DC OUTPUT VOLTAGES CONVERTED TO PRESSURE AND DENSITY

TMAX(SEC)=58619.862 V(VOLT)= 1.574 C(AMP)= 0.31E-C8 P(TORRS)= 0.75E-07									
BA2	ALT= 918.4	LAT= -44.8	LONG= 134.4	LST= 1.30	DP = 0.	TXRAM=58619.645	RX = 2.129	DENSITY =0.	0.
TMIN(SEC)=58619.646 V(VOLT)= 1.574 C(AMP)= 0.31E-C8 P(TORRS)= 0.75E-07									
TMAX(SEC)=58619.301 V(VOLT)= 3.632 ADJ V= 3.801 C(AMP)= 0.17E-08 P(TORRS)= 0.29E-09									
RH1	ALT= 918.4	LAT= -44.8	LONG= 134.4	LST= 1.30	DP =-0.34E-10	TXRAM=58619.431	RX = 2.129	DENSITY =0.212E-17	0.388E-17
TMIN(SEC)=58619.501 V(VOLT)= 3.794 ADJ V= 3.763 C(AMP)= 0.19E-08 P(TORRS)= 0.33E-09									
TMAX(SEC)=58619.869 P(TORRS)= 0.11E-08 TXRAM(SEC)=58619.854 MAX-RAM VEL.=4.428 SX= -0.434E 01 DENSITY =0.									
RH2	ALT= 918.4	LAT= -44.8	LONG= 134.4	LST= 1.30	DELTA P =-0.93E-10	AVE-RAM VEL.= -5.649	DENSITY =0.	0.	0.
TMIN(SEC)=58619.752 P(TORRS)= 0.12E-08 TXRAM(SEC)=58619.538 MIN-RAM VEL.= -6.871 SN = -0.674E 01									
TMAX(SEC)=58620.329 V(VOLT)= 1.582 C(AMP)= 0.32E-C8 P(TORRS)= 0.77E-07									
BA2	ALT= 918.4	LAT= -44.8	LONG= 134.4	LST= 1.30	DP = 0.51E-08	TXRAM=58620.312	RX = 2.129	DENSITY =0.315E-15	0.576E-15
TMIN(SEC)=58620.062 V(VOLT)= 1.561 C(AMP)= 0.30E-C8 P(TORRS)= 0.72E-07									
TMAX(SEC)=58620.067 V(VOLT)= 3.909 ADJ V= 3.877 C(AMP)= 0.13E-03 P(TORRS)= 0.24E-09									
RH1	ALT= 918.4	LAT= -44.8	LONG= 134.4	LST= 1.30	DP =-0.90E-10	TXRAM=58620.098	RX = 2.129	DENSITY =0.559E-17	0.102E-16
TMIN(SEC)=58619.924 V(VOLT)= 3.794 ADJ V= 3.763 C(AMP)= 0.19E-03 P(TORRS)= 0.33E-09									
TMAX(SEC)=58620.364 P(TORRS)= 0.98E-09 TXRAM(SEC)=58620.521 MAX-RAM VEL.=4.428 SX= -0.434E 01 DENSITY =0.									
RH2	ALT= 918.4	LAT= -44.8	LONG= 134.4	LST= 1.30	DELTA P =-0.22E-09	AVE-RAM VEL.= -5.649	DENSITY =0.	0.	0.
TMIN(SEC)=58620.252 P(TORRS)= 0.12E-08 TXRAM(SEC)=58620.205 MIN-RAM VEL.= -6.871 SN = -0.674E 01									
TMAX(SEC)=58621.112 V(VOLT)= 1.574 C(AMP)= 0.31E-C8 P(TORRS)= 0.75E-07									
BA2	ALT= 918.4	LAT= -44.8	LONG= 134.5	LST= 1.31	DP = 0.34E-C8	TXRAM=58620.979	RX = 2.129	DENSITY =0.211E-15	

0.386E-15

TMIN(SEC)=58620.612 V(VOLT)= 1.561 C(AMP)= 0.30E-C3 P(TURRS)= 0.72E-07

TMAX(SEC)=58620.651 V(VOLT)= 3.845 ADJ V= 3.814 C(AMP)= 0.16E-08 P(TURRS)= 0.28E-09

RH1 ALT= 018.4 LAT= -44.8 LONG= 134.5 LST= 1.31 DP =-0.33E-10 TXRAM=58620.765 RX = 2.129 DENSITY =0.203E-17
0.371E-17

TMIN(SEC)=58621.234 V(VOLT)= 3.807 ADJ V= 3.775 C(AMP)= 0.18E-08 P(TURRS)= 0.32E-09

TMAX(SEC)=58621.135 P(TURRS)= 0.12E-08 TXRAM(SEC)=58621.188 MAX.RAM VEL.=4.428 SA= -0.434E 01 DENSITY =0.

RH2 ALT= 018.4 LAT= -44.8 LONG= 134.5 LST= 1.31 DELTA P = 0. AVE.RAM VEL.= -5.649 DENSITY =0.
0.

TMIN(SEC)=58621.135 P(TURRS)= 0.12E-08 TXRAM(SEC)=58620.872 MIN.RAM VEL.= -6.871 SN = -0.674E 01

TMAX(SEC)=58621.779 V(VOLT)= 1.561 C(AMP)= 0.30E-C8 P(TURRS)= 0.72E-07

RH2 ALT= 018.4 LAT= -44.7 LONG= 134.5 LST= 1.31 DP =-0.95E-09 TXRAM=58621.646 RX = 2.129 DENSITY =0.586E-14
0.107E-15

TMIN(SEC)=58621.929 V(VOLT)= 1.565 C(AMP)= 0.30E-C8 P(TURRS)= 0.73E-07

TMAX(SEC)=58621.901 V(VOLT)= 3.893 ADJ V= 3.861 C(AMP)= 0.14E-03 P(TURRS)= 0.25E-09

RH1 ALT= 018.4 LAT= -44.7 LONG= 134.5 LST= 1.31 DP =-0.83E-10 TXRAM=58622.099 RX = 2.129 DENSITY =0.514E-17
0.940E-17

TMIN(SEC)=58621.817 V(VOLT)= 3.791 ADJ V= 3.760 C(AMP)= 0.20E-08 P(TURRS)= 0.33E-09

TMAX(SEC)=58621.902 P(TURRS)= 0.13E-08 TXRAM(SEC)=58621.855 MAX.RAM VEL.=4.428 SA= -0.434E 01 DENSITY =0.

RH2 ALT= 018.4 LAT= -44.7 LONG= 134.5 LST= 1.31 DELTA P = 0.13E-10 AVE.RAM VEL.= -5.649 DENSITY =0.
0.

TMIN(SEC)=58621.519 P(TURRS)= 0.12E-08 TXRAM(SEC)=58621.539 MIN.RAM VEL.= -6.871 SN = -0.674E 01

TMAX(SEC)=58622.079 V(VOLT)= 1.574 C(AMP)= 0.31E-C8 P(TURRS)= 0.75E-07

BA2 ALT= 018.4 LAT= -44.7 LONG= 134.5 LST= 1.31 DP = 0.22E-03 TXRAM=58622.312 RX = 2.129 DENSITY =0.137E-15
0.251E-15

TMIN(SEC)=58622.496 V(VOLT)= 1.555 C(AMP)= 0.30E-C3 P(TURRS)= 0.73E-07

TMAX(SEC)=58622.494 V(VOLT)= 3.542 ADJ V= 3.511 C(AMP)= 0.16E-04 P(TURRS)= 0.29E-09

PRESSURE GAUGES DC OUTPUT VOLTAGES CONVERTED TO ION CURRENT AND PRESSURE

TIME	GAGE VOLTS	ADJ VOLTS	CURRENT	PRESSURE	TIME	GAGE VOLTS	ADJ VOLTS	CURRENT	PRESSURE
58619.144	C.444	3.861	0.27E-10	-0.	58619.146	BA2 EMISSION CURRENT =	1.574	0.31E-08	-0.
58619.151	3.332	3.861	0.17E-08	C.29E-C9	58619.152	3.782	3.4C5	0.54E-08	0.12E-08
58619.160	C.444	3.852	0.27E-10	-0.	58619.162	1.574		0.31E-08	-0.
58619.167	3.883	3.852	0.14E-08	C.25E-C9	58619.168	3.794	3.418	0.51E-08	0.12E-08
58619.177	C.431	3.890	0.27E-10	-0.	58619.179	1.574		0.31E-08	-0.
58619.184	3.921	3.890	0.12E-08	C.23E-C9	58619.185	3.820	3.443	0.47E-08	0.11E-08
58619.194	C.431	3.826	0.27E-10	-0.	58619.196	BA2 EMISSION CURRENT =	0.	-0.	-0.
58619.201	3.858	3.826	0.15E-08	C.27E-C9	58619.202	1.574	3.456	0.45E-08	0.10E-08
58619.210	C.431	3.763	0.27E-10	-0.	58619.212	3.832		0.31E-08	-0.
58619.218	3.794	3.763	0.19E-08	C.33E-C9	58619.219	3.820	3.443	0.47E-08	0.11E-08
58619.227	C.431	3.775	0.27E-10	-0.	58619.229	1.561		0.30E-08	-0.
58619.234	3.807	3.775	0.18E-08	C.32E-C9	58619.235	3.807	3.431	C.49E-08	0.11E-08
58619.244	C.444	3.814	0.27E-10	-0.	58619.246	BA2 EMISSION CURRENT =	0.	-0.	-0.
58619.251	3.845	3.814	0.16E-08	C.28E-C9	58619.252	1.574	3.363	0.31E-08	0.12E-08
58619.260	C.444	3.852	0.27E-10	-0.	58619.262	3.769		0.31E-08	-0.
58619.268	3.883	3.852	0.14E-08	C.25E-C9	58619.269	3.794	3.393	0.56E-08	0.12E-08
58619.277	C.431	3.890	0.27E-10	-0.	58619.279	1.574		0.31E-08	-0.
58619.284	3.921	3.890	0.12E-08	C.23E-C9	58619.285	3.782	3.4C5	0.54E-08	0.12E-08
58619.293	C.431	3.801	0.27E-10	-0.	58619.295	BA2 EMISSION CURRENT =	0.	-0.	-0.
58619.301	3.832	3.801	0.17E-08	C.29E-C9	58619.302	1.574	3.421	0.31E-08	0.11E-08
58619.310	C.431	3.750	0.27E-10	-0.	58619.312	3.807		0.49E-08	-0.
58619.317	3.782	3.750	0.20E-08	C.34E-09	58619.318	3.794	3.418	0.31E-08	0.12E-08
58619.327	C.431	3.775	0.27E-10	-0.	58619.329	1.574		0.31E-08	-0.
58619.334	3.807	3.775	0.18E-08	C.32E-C9	58619.335	3.820	3.443	0.47E-08	0.11E-08
58619.344	C.444	3.826	0.27E-10	-0.	58619.346	BA2 EMISSION CURRENT =	0.	-0.	-0.
58619.351	3.858	3.826	0.15E-08	C.27E-C9	58619.352	1.561		0.30E-08	-0.
58619.360	C.433	3.861	0.27E-10	-0.	58619.362	3.858	3.482	0.42E-08	0.13E-08
58619.368	3.893	3.861	0.14E-08	C.25E-09	58619.369	3.779		0.30E-08	-0.
58619.377	C.420	3.912	0.26E-10	-0.	58619.379	1.565	3.4C2	0.54E-08	0.12E-08
58619.384	3.944	3.912	0.11E-08	C.22E-C9	58619.385	3.766	3.390	0.30E-08	0.13E-08
58619.394	C.420	3.826	0.26E-10	-0.	58619.396	BA2 EMISSION CURRENT =	0.	-0.	-0.
58619.401	3.804	3.826	0.19E-08	C.32E-C9	58619.402	1.565		0.30E-08	-0.
58619.410	C.431	3.772	0.27E-10	-0.	58619.422	3.753	3.377	0.59E-08	0.13E-08
58619.417	3.794	3.763	0.19E-08	C.33E-C9	58619.418	1.574		0.31E-08	-0.
58619.427	C.431	3.788	0.27E-10	-0.	58619.429	3.769	3.393	0.56E-08	0.12E-08
58619.434	3.820	3.788	0.18E-08	C.30E-C9	58619.435	1.574		0.31E-08	-0.
58619.444	C.444	3.826	0.27E-10	-0.	58619.435	3.807	3.431	0.49E-08	0.11E-08
58619.451	3.858	3.826	0.15E-08	C.27E-C9	58619.446	BA2 EMISSION CURRENT =	0.	-0.	-0.
58619.460	C.444	3.877	0.27E-10	-0.	58619.462	1.574	3.456	0.45E-08	0.10E-08
58619.468	3.909	3.877	0.13E-08	C.24E-09	58619.469	3.845		0.31E-08	-0.
58619.477	C.444	3.928	0.27E-10	-0.	58619.479	3.858	3.469	0.43E-08	0.09E-09
58619.484	3.959	3.928	0.11E-08	C.21E-C9	58619.485	1.561		0.30E-08	-0.
58619.494	C.431	3.826	0.27E-10	-0.	58619.496	BA2 EMISSION CURRENT =	0.	-0.	-0.
58619.501	3.794	3.763	0.19E-08	C.33E-C9	58619.502	1.561	3.367	0.30E-08	0.14E-08
58619.510	C.431	3.763	0.27E-10	-0.	58619.512	3.744		0.31E-08	-0.

58619.518	3.807	3.775	0.19E-08	0.33E-05	58619.519	3.744	3.367	0.61E-08	0.14E-08
58619.527	C.431	3.861	0.27E-10	0.29E-05	58619.529	1.574	3.405	0.31E-08	-0.
58619.534	3.832	BAL EMISSION CURRENT = -0.	0.17E-08	0.29E-05	58619.535	3.782	3.405	0.54E-05	0.12E-08
58619.543	C.444	3.859	0.27E-10	-0.	58619.545	1.574		-0.	-0.
58619.551	3.871	0.27E-10	0.19E-08	C.26E-05	58619.552	3.807	3.431	0.49E-08	0.11E-08
58619.560	C.433	3.887	0.27E-10	-0.	58619.562	1.565		0.30E-08	-0.
58619.567	3.919	3.887	0.12E-08	C.23E-05	58619.568	3.817	3.440	0.48E-08	0.11E-08
58619.574	C.420	3.900	0.26E-10	-0.	58619.579	1.552		0.29E-08	-0.
58619.581	3.931	BAL EMISSION CURRENT = -0.	0.12E-05	0.21E-05	58619.585	3.830	3.453	0.46E-08	0.10E-08
58619.594	C.420	3.760	0.26E-10	-0.	58619.596	1.552		-0.	-0.
58619.601	3.791	3.760	0.20E-08	0.33E-05	58619.602	3.830	3.453	0.46E-08	0.10E-08
58619.610	C.431	3.775	0.27E-10	-0.	58619.612	1.574		0.31E-08	-0.
58619.618	3.807	3.775	0.18E-08	C.34E-05	58619.619	3.769	3.393	0.56E-08	0.12E-08
58619.627	C.431	3.801	0.17E-08	-0.	58619.629	1.574		0.31E-08	-0.
58619.634	3.832	BAL EMISSION CURRENT = 4.871	0.17E-08	0.29E-05	58619.635	3.756	3.380	0.58E-08	0.13E-08
58619.644	C.444	3.852	0.27E-10	C.54E-05	58619.646	1.574		0.31E-08	0.75E-07
58619.651	3.883	3.852	0.14E-08	C.25E-05	58619.652	3.769	3.353	0.56E-08	0.12E-08
58619.660	0.444	3.890	0.27E-10	0.54E-05	58619.658	1.574		0.31E-08	0.75E-07
58619.667	3.921	3.890	0.12E-08	C.23E-05	58619.668	3.794	3.418	0.51E-08	0.12E-08
58619.677	C.431	3.839	0.27E-10	C.53E-05	58619.679	1.561		0.30E-08	0.72E-07
58619.684	3.871	BAL EMISSION CURRENT = 4.871	0.15E-08	0.26E-05	58619.685	3.807	3.431	0.49E-08	0.11E-08
58619.694	C.431	3.763	0.27E-10	0.53E-05	58619.696	1.574		0.31E-08	0.75E-07
58619.701	3.754	3.763	0.19E-08	C.33E-05	58619.702	3.807	3.431	0.49E-08	0.11E-08
58619.710	C.431	3.788	0.27E-10	C.53E-05	58619.712	1.574		0.31E-08	0.75E-07
58619.718	3.820	3.788	0.18E-08	0.30E-05	58619.719	3.845	3.469	0.43E-08	0.98E-09
58619.727	C.431	3.814	0.27E-10	C.53E-05	58619.729	1.574		0.31E-08	0.75E-07
58619.734	3.845	BAL EMISSION CURRENT = 4.871	0.16E-08	C.28E-05	58619.735	3.858	3.442	0.42E-08	0.94E-09
58619.744	0.444	3.852	0.27E-10	0.54E-05	58619.746	1.574		0.31E-08	0.75E-07
58619.751	3.883	3.852	0.14E-08	0.25E-05	58619.752	3.782	3.405	0.54E-08	0.12E-08
58619.760	C.444	3.902	0.27E-10	0.54E-05	58619.762	1.574		0.31E-08	0.75E-07
58619.768	3.934	3.902	0.12E-08	0.22E-05	58619.769	3.769	3.393	0.56E-08	0.12E-08
58619.777	C.431	3.788	0.27E-10	0.53E-05	58619.779	1.574		0.31E-08	0.75E-07
58619.784	3.820	BAL EMISSION CURRENT = 4.871	0.18E-08	C.30E-05	58619.785	3.782	3.405	0.54E-08	0.12E-08
58619.793	C.431	3.763	0.27E-10	0.53E-05	58619.795	1.574		0.31E-08	0.75E-07
58619.801	3.794	3.763	0.19E-08	0.33E-05	58619.802	3.782	3.405	0.54E-08	0.12E-08
58619.810	C.431	3.788	0.27E-10	0.53E-05	58619.812	1.574		0.31E-08	0.75E-07
58619.817	3.820	3.788	0.18E-08	C.30E-05	58619.818	3.820	3.443	0.47E-08	0.11E-08
58619.827	C.431	3.801	0.27E-10	C.53E-05	58619.829	1.574		0.31E-08	0.75E-07
58619.834	3.832	BAL EMISSION CURRENT = 4.871	0.17E-08	0.29E-05	58619.835	3.832	3.456	0.45E-08	0.10E-08
58619.844	0.444	3.864	0.27E-10	C.54E-05	58619.846	1.574		0.31E-08	0.75E-07
58619.851	3.896	3.864	0.13E-08	0.25E-05	58619.852	3.845	3.469	0.43E-08	0.98E-09
58619.860	0.444	3.915	0.27E-10	0.54E-05	58619.862	1.574		0.31E-08	0.75E-07
58619.868	3.947	3.915	0.11E-08	0.21E-05	58619.869	3.807	3.431	0.49E-08	0.11E-08
58619.877	C.431	3.775	0.27E-10	C.53E-05	58619.879	1.574		0.31E-08	0.75E-07
58619.884	3.807	BAL EMISSION CURRENT = 4.871	0.18E-08	0.32E-05	58619.885	3.744	3.367	0.61E-08	0.14E-08
58619.894	C.431	3.750	0.27E-10	C.53E-05	58619.896	1.574		0.31E-08	0.75E-07
58619.901	3.782	3.750	0.20E-08	C.34E-05	58619.902	3.756	3.380	0.58E-08	0.13E-08
58619.910	C.431	3.788	0.27E-10	0.53E-05	58619.912	1.574		0.31E-08	0.75E-07
58619.917	3.820	3.788	0.18E-08	0.30E-05	58619.918	3.782	3.405	0.54E-08	0.12E-08
58619.927	C.431	3.826	0.27E-10	0.53E-05	58619.929	1.561		0.30E-08	0.72E-07
58619.934	3.858	BAL EMISSION CURRENT = 4.871	0.15E-08	C.27E-05	58619.935	3.807	3.431	0.49E-08	0.11E-08
58619.944	0.444	3.826	0.27E-10	0.54E-05	58619.946	1.574		0.31E-08	0.75E-07

58615.951	3.909	3.677	0.13E-08	C.24F-C5	58619.952	3.820	3.443	C.47E-08	0.11E-08
58615.960	0.444	3.928	0.27E-10	C.54E-C5	58619.962	1.574	3.469	C.31E-08	0.75E-07
58615.968	3.959	3.928	0.11E-08	C.21E-C5	58619.969	3.845	3.469	0.98E-09	0.98E-09
58615.977	0.431	3.763	0.27E-10	C.53F-C5	58619.979	1.574	3.456	C.31E-08	0.75E-07
58615.984	3.794	3.763	0.19E-08	C.33E-C5	58619.985	3.832	3.456	C.45E-08	0.10E-08
58615.994	1.431	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.001	3.807	3.775	0.27E-10	C.53F-C5	58619.996	1.574	3.350	C.31E-05	0.75E-07
58620.010	3.820	3.775	0.18E-08	C.32E-C5	58620.002	1.565	3.350	0.13E-08	0.13E-08
58620.018	3.830	3.798	0.26E-10	C.52E-C5	58620.019	3.766	3.350	C.57E-08	0.13E-08
58620.027	3.840	3.836	0.17E-08	C.32E-C5	58620.029	1.552	3.402	0.29E-08	0.70E-07
58620.034	3.868	3.836	0.26E-10	C.52F-C5	58620.035	3.779	3.402	C.54E-08	0.12E-08
58620.043	0.433	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.051	3.904	3.874	0.27E-10	C.53E-C5	58620.045	1.552	3.415	0.70E-07	0.70E-07
58620.060	3.909	3.874	0.13E-08	C.24F-C5	58620.052	3.791	3.415	0.12E-08	0.12E-08
58620.067	3.909	3.877	0.27E-10	C.54E-C5	58620.062	1.561	3.415	C.52E-08	0.72E-07
58620.077	0.431	3.877	0.13E-08	C.24E-C5	58620.068	3.820	3.443	C.30E-08	0.11E-08
58620.084	3.756	3.725	0.22E-08	C.53E-C5	58620.079	1.574	3.431	C.47E-08	0.75E-07
58620.094	0.431	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.101	3.782	3.750	0.27E-10	C.53E-C5	58620.096	1.574	3.456	0.75E-07	0.75E-07
58620.110	0.431	3.814	0.20E-08	C.54E-C5	58620.102	3.832	3.456	0.10E-08	0.10E-08
58620.118	3.845	3.814	0.16E-08	C.53E-C5	58620.112	1.574	3.456	0.75E-07	0.75E-07
58620.127	0.431	3.852	0.27E-10	C.53E-C5	58620.119	3.832	3.456	0.10E-08	0.10E-08
58620.134	3.883	3.852	0.14E-08	C.25E-C5	58620.129	1.574	3.353	C.31E-08	0.75E-07
58620.144	0.444	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.151	3.934	3.902	0.27E-10	C.54E-C5	58620.146	1.561	3.353	0.56E-08	0.75E-07
58620.160	0.444	3.826	0.12E-08	C.22E-C5	58620.152	3.769	3.353	0.30E-08	0.72E-07
58620.167	3.858	3.826	0.27E-10	C.54E-C5	58620.162	1.561	3.405	0.12E-08	0.12E-08
58620.177	0.431	3.763	0.15E-08	C.27E-C5	58620.168	3.782	3.405	0.54E-08	0.72E-07
58620.184	3.794	3.763	0.27E-10	C.53E-C5	58620.179	1.561	3.405	0.30E-08	0.72E-07
58620.194	0.431	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.201	3.807	3.775	0.27E-10	C.53E-C5	58620.196	1.561	3.405	0.30E-08	0.72E-07
58620.210	0.431	3.814	0.18E-08	C.22E-C5	58620.202	3.807	3.421	0.49E-08	0.11E-08
58620.218	3.845	3.814	0.27E-10	C.53E-C5	58620.212	1.574	3.456	0.31E-08	0.75E-07
58620.227	0.431	3.864	0.16E-08	C.28E-C5	58620.219	3.832	3.456	0.45E-08	0.10E-08
58620.234	3.896	3.864	0.27E-10	C.53E-C5	58620.229	1.574	3.456	0.31E-08	0.75E-07
58620.244	0.444	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.251	3.934	3.902	0.13E-08	C.25E-C5	58620.235	3.858	3.456	0.42E-08	0.94E-09
58620.260	0.444	3.902	0.27E-10	C.54E-C5	58620.246	1.561	3.456	0.31E-08	0.75E-07
58620.268	3.820	3.788	0.12E-08	C.22E-C5	58620.252	3.782	3.405	0.54E-08	0.12E-08
58620.277	0.431	3.763	0.18E-08	C.28E-C5	58620.262	1.574	3.350	0.31E-08	0.75E-07
58620.284	3.794	3.763	0.27E-10	C.53E-C5	58620.269	3.756	3.350	0.58E-08	0.13E-08
58620.293	0.431	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.301	3.820	3.788	0.18E-08	C.25E-C5	58620.285	3.756	3.350	0.58E-08	0.13E-08
58620.310	0.444	3.788	0.27E-10	C.53E-C5	58620.295	1.561	3.418	0.30E-08	0.72E-07
58620.317	3.861	3.829	0.15E-08	C.30E-C5	58620.302	3.794	3.418	0.51E-08	0.12E-08
58620.327	0.444	3.867	0.27E-10	C.54E-C5	58620.312	1.582	3.434	0.32E-08	0.77E-07
58620.334	3.899	3.867	0.13E-08	C.24E-C5	58620.318	3.810	3.434	0.49E-08	0.11E-08
58620.344	0.456	BA1 EMISSION CURRENT = 4.871			BA2 EMISSION CURRENT = 4.940				
58620.351	3.949	3.918	0.28E-10	C.54E-C5	58620.335	3.835	3.459	0.32E-08	0.77E-07
58620.360	0.444	3.918	0.11E-08	C.21E-C5	58620.346	1.582	3.472	0.32E-08	0.77E-07
58620.368	3.807	3.775	0.27E-10	C.54E-C5	58620.352	3.848	3.472	0.43E-08	0.97E-09
58620.377	0.431	3.775	0.18E-08	C.32E-C5	58620.362	1.574	3.469	0.31E-08	0.75E-07
58620.384	3.807	3.775	0.27E-10	C.53E-C5	58620.369	3.845	3.469	0.32E-08	0.77E-07
58620.394	0.431	3.775	0.18E-08	C.32F-C5	58620.379	1.561	3.367	0.30E-08	0.92E-09
58620.404	3.807	3.775	0.18E-08	C.32F-C5	58620.385	3.744	3.367	0.61E-08	0.14E-08

5862C.594	C.431	PA1 EMISSION CURRENT = 4.811	BA2 EMISSION CURRENT = 4.940	0.75E-07
5862C.401	3.788	0.27E-10 C.53E-C5	58620.356	0.31E-08
5862C.410	3.788	0.18E-08 C.30E-C5	58620.402	0.56E-08
5862C.417	3.855	0.26E-10 C.52E-C5	58620.412	0.30E-C2
5862C.427	0.420	0.16E-08 C.20E-C5	58620.418	0.54E-08
5862C.434	3.906	0.26E-10 C.52E-C5	58620.429	0.30E-08
5862C.444	0.433	0.13E-C8 C.24E-C5	58620.435	0.50E-08
5862C.451	3.957	0.27E-10 C.53E-C5	58620.446	4.940
5862C.460	C.444	0.11E-08 C.21E-C5	58620.452	0.38E-08
5862C.468	3.794	0.27E-10 C.54E-C5	58620.462	0.48E-08
5862C.477	0.431	0.19E-08 C.33E-C5	58620.469	0.31E-08
5862C.484	3.807	0.27E-10 C.53E-C5	58620.479	0.49E-08
5862C.494	0.431	0.18E-C8 C.24E-C5	58620.485	0.30E-08
5862C.501	3.832	PA1 EMISSION CURRENT = 4.811	BA2 EMISSION CURRENT = 4.940	0.75E-07
5862C.510	C.431	0.27E-10 C.53E-C5	58620.496	0.31E-08
5862C.518	3.871	0.17E-C8 C.29E-C5	58620.502	0.51E-08
5862C.527	0.431	0.27E-10 C.53E-C5	58620.512	0.31E-08
5862C.534	3.909	0.15E-C8 C.26E-C5	58620.519	0.58E-08
5862C.543	C.444	0.27E-10 C.53E-C5	58620.529	0.75E-07
5862C.551	3.883	0.14E-C8 C.24E-C5	58620.535	0.31E-08
5862C.560	0.433	0.27E-10 C.54E-C5	58620.545	4.940
5862C.567	3.779	0.27E-10 C.53E-C5	58620.552	0.31E-08
5862C.577	C.420	0.20E-08 C.34E-C5	58620.568	0.51E-08
5862C.584	3.804	0.26E-10 C.52E-C5	58620.579	0.30E-08
5862C.594	0.420	0.19E-C8 C.32E-C5	58620.585	0.75E-07
5862C.601	3.842	PA1 EMISSION CURRENT = 4.811	BA2 EMISSION CURRENT = 4.940	0.12E-08
5862C.610	0.431	0.26E-10 C.52E-C5	58620.596	0.31E-08
5862C.618	3.883	0.16E-C8 C.29E-C5	58620.602	0.29E-08
5862C.627	C.431	0.27E-10 C.53E-C5	58620.612	0.46E-08
5862C.634	3.934	0.14E-C8 C.25E-C5	58620.619	0.72E-07
5862C.644	0.444	0.27E-10 C.53E-C5	58620.629	0.30E-08
5862C.651	3.845	0.12E-08 C.22E-C5	58620.635	0.94E-09
5862C.660	C.433	PA1 EMISSION CURRENT = 4.921	BA2 EMISSION CURRENT = 4.913	0.75E-07
5862C.667	3.779	0.27E-10 C.54E-C9	58620.646	0.31E-08
5862C.677	0.420	0.16E-C8 C.28E-C9	58620.652	0.56E-08
5862C.684	3.804	0.27E-10 C.53E-C5	58620.662	0.30E-08
5862C.694	C.420	0.20E-08 C.34E-C9	58620.668	0.73E-07
5862C.701	3.842	0.20E-08 C.34E-C9	58620.679	0.59E-08
5862C.710	0.420	0.26E-10 C.51E-C5	58620.685	0.30E-08
5862C.718	3.893	0.19E-08 C.32E-C5	58620.695	0.73E-07
5862C.727	C.420	PA1 EMISSION CURRENT = 4.921	BA2 EMISSION CURRENT = 4.913	0.12E-08
5862C.734	3.931	0.16E-C8 C.28E-C9	58620.696	0.54E-08
5862C.744	0.433	0.26E-10 C.51E-C5	58620.702	0.30E-08
5862C.751	3.817	0.16E-08 C.29E-C9	58620.712	0.50E-08
5862C.760	0.444	0.26E-10 C.51E-C5	58620.722	0.73E-07
5862C.768	3.794	0.14E-08 C.25E-C5	58620.719	0.30E-08
5862C.777	C.431	0.14E-08 C.25E-C5	58620.729	0.46E-08
5862C.784	3.826	0.26E-10 C.51E-C5	58620.735	0.10E-08
5862C.793	C.431	0.12E-08 C.22E-C5	58620.746	0.70E-07
5862C.801	3.858	PA1 EMISSION CURRENT = 4.921	BA2 EMISSION CURRENT = 4.913	0.73E-07
5862C.810	C.431	0.27E-10 C.53E-C5	58620.752	0.29E-08
5862C.817	3.909	0.18E-08 C.30E-C5	58620.762	0.44E-08
5862C.827	0.433	0.19E-08 C.33E-C5	58620.769	0.99E-09
5862C.837	3.826	0.27E-10 C.53E-C5	58620.779	0.70E-07
5862C.847	0.433	0.18E-08 C.30E-C5	58620.785	0.12E-08
5862C.857	3.826	PA1 EMISSION CURRENT = 4.921	BA2 EMISSION CURRENT = 4.913	0.75E-07
5862C.867	0.433	0.27E-10 C.53E-C5	58620.795	0.31E-08
5862C.877	3.858	0.15E-C8 C.27E-C5	58620.802	0.12E-08
5862C.887	C.431	0.27E-10 C.53E-C5	58620.812	0.75E-07
5862C.897	3.909	0.13E-08 C.24E-C5	58620.818	0.31E-08
5862C.907	0.433			0.49E-08

5862C.827	C.431	3.915	0.27E-10	C.53E-C5	58620.829	1.574	0.31E-08
5862C.834	3.947	BA1 EMISSION CURRENT = 4.521	0.11E-08	C.21E-C5	58620.835	3.832	C.45E-08
5862C.844	C.444	3.763	0.27E-10	C.54E-C5	58620.846	3.456	0.31E-08
5862C.851	3.794	0.19E-08	0.19E-08	C.33E-C5	58620.852	1.574	C.47E-08
5862C.860	C.456	3.766	0.28E-10	C.55E-C5	58620.862	3.850	0.11E-08
5862C.868	3.797	0.19E-08	0.19E-08	C.32E-C5	58620.869	1.570	0.75E-07
5862C.877	C.443	3.807	0.27E-10	C.54E-C5	58620.879	3.835	0.10E-08
5862C.884	3.835	0.17E-08	0.17E-08	C.32E-C5	58620.885	1.574	0.75E-07
5862C.894	C.443	3.804	0.17E-08	C.29E-C5	58620.895	3.772	0.12E-08
5862C.901	3.873	BA1 EMISSION CURRENT = 4.521	0.27E-10	C.54E-C5	58620.896	BA2 EMISSION CURRENT = 4.913	0.75E-07
5862C.910	C.420	3.842	0.15E-08	0.26E-C5	58620.902	1.570	0.13E-08
5862C.917	3.919	0.26E-10	0.12E-08	C.51E-C5	58620.912	3.759	0.58E-08
5862C.927	C.420	3.887	0.12E-08	C.23E-C5	58620.918	1.572	0.70E-07
5862C.934	3.944	3.912	0.26E-10	C.51E-C5	58620.929	3.390	0.13E-08
5862C.944	C.433	3.760	0.11E-08	0.22E-C5	58620.935	1.565	0.30E-08
5862C.951	3.791	BA1 EMISSION CURRENT = 4.521	0.27E-10	C.53E-C5	58620.946	3.791	0.52E-08
5862C.960	C.433	3.772	0.20E-08	C.33E-C5	58620.952	1.565	0.30E-08
5862C.968	3.804	0.27E-10	0.19E-08	0.33E-C5	58620.962	1.565	0.11E-08
5862C.977	C.420	3.798	0.19E-08	C.32E-C5	58620.969	3.804	0.50E-08
5862C.984	3.830	0.26E-10	0.17E-08	C.51E-C5	58620.979	1.565	0.73E-07
5862C.994	C.420	3.849	0.14E-08	C.30E-C5	58620.985	3.842	0.99E-09
58621.001	3.880	0.27E-10	0.26E-10	C.51E-C5	58620.996	BA2 EMISSION CURRENT = 4.913	0.70E-07
58621.010	C.431	3.890	0.27E-10	C.26E-C5	58621.002	1.552	0.99E-09
58621.018	3.921	0.12E-08	0.27E-10	C.53E-C5	58621.012	3.842	0.44E-08
58621.027	C.431	3.839	0.27E-10	0.23E-C5	58621.019	1.574	0.75E-07
58621.034	3.871	0.15E-08	0.15E-08	0.32E-C5	58621.029	3.769	0.13E-08
58621.043	C.444	3.750	0.27E-10	C.26E-C5	58621.035	3.353	0.12E-08
58621.051	3.782	0.20E-08	0.20E-08	C.54E-C5	58621.045	BA2 EMISSION CURRENT = 4.913	0.75E-07
58621.060	C.444	3.775	0.18E-08	C.34E-C5	58621.052	1.574	0.31E-08
58621.067	3.807	0.18E-08	0.27E-10	C.54E-C5	58621.062	3.769	0.56E-08
58621.077	C.431	3.814	0.27E-10	C.32E-C5	58621.068	1.574	0.75E-07
58621.084	3.845	0.16E-08	0.16E-08	0.32E-C5	58621.079	3.782	0.12E-08
58621.094	C.431	3.839	0.27E-10	C.53E-C5	58621.085	1.561	0.75E-07
58621.101	3.871	BA1 EMISSION CURRENT = 4.521	0.27E-10	0.28E-C5	58621.096	3.820	0.11E-08
58621.110	C.431	3.839	0.15E-08	C.53E-C5	58621.102	BA2 EMISSION CURRENT = 4.913	0.72E-07
58621.118	3.934	0.27E-10	0.27E-10	C.26E-C5	58621.112	1.561	0.10E-08
58621.127	C.431	3.902	0.12E-08	C.53E-C5	58621.119	3.832	0.45E-08
58621.134	3.832	0.27E-10	0.27E-10	C.23E-C5	58621.129	1.574	0.75E-07
58621.144	C.444	3.801	0.17E-08	0.53E-C5	58621.135	3.794	0.94E-09
58621.151	3.782	BA1 EMISSION CURRENT = 4.871	0.27E-10	C.23E-C5	58621.146	3.443	0.75E-07
58621.160	C.444	3.750	0.20E-08	0.54E-C5	58621.152	BA2 EMISSION CURRENT = 4.937	0.14E-08
58621.167	3.807	0.18E-08	0.27E-10	C.34E-C5	58621.162	1.574	0.31E-08
58621.177	C.431	3.775	0.18E-08	0.54E-C5	58621.168	3.756	0.75E-07
58621.184	3.858	0.27E-10	0.27E-10	C.32E-C5	58621.179	1.574	0.13E-08
58621.194	C.431	3.826	0.15E-08	C.53E-C5	58621.185	3.794	0.75E-07
58621.201	3.896	BA1 EMISSION CURRENT = 4.871	0.27E-10	0.27E-C5	58621.196	BA2 EMISSION CURRENT = 4.937	0.12E-08
58621.210	C.431	3.864	0.13E-08	0.53E-C5	58621.202	1.574	0.75E-07
58621.218	3.947	0.27E-10	0.27E-10	C.23E-C5	58621.212	3.807	0.11E-08
58621.227	C.431	3.915	0.11E-08	0.53E-C5	58621.219	1.574	0.75E-07
58621.234	3.807	0.27E-10	0.27E-10	C.21E-C5	58621.229	3.832	0.10E-08
58621.244	C.444	3.775	0.18E-08	C.53E-C5	58621.235	1.574	0.75E-07
58621.251	3.794	BA1 EMISSION CURRENT = 4.871	0.27E-10	C.32E-C5	58621.246	3.820	0.11E-08
		0.27E-10	0.27E-10	0.54E-C5	58621.252	BA2 EMISSION CURRENT = 4.937	0.75E-07
		0.19E-08	0.19E-08	C.33E-C5		1.574	0.31E-08
						3.845	0.49E-08
						3.469	0.75E-07
							0.98E-09

DENSITY PLOT TAPE OUTPUT (A6)

EDIT = 327 ORBIT = 711

52058619.301	-44.42	134.33	1.30	918.4PDD0.	0.598E-170.	0.
52058620.067	-44.42	134.42	1.30	918.4PDD0.576E-150.	1.02E-160.	0.
52058620.651	-44.77	134.46	1.31	918.4PDD0.386E-150.	3.71E-170.	0.
52058621.901	-44.75	134.50	1.31	918.4PDD0.107E-150.	3.40E-170.	0.
52058622.484	-44.72	134.54	1.31	918.4PDD0.251E-150.	4.80E-170.	0.
52058623.350	-44.69	134.58	1.32	918.3PDD0.347E-150.	5.13E-170.	0.
52058623.933	-44.67	134.62	1.32	918.3PDD0.742E-160.	0.	0.
52058624.700	-44.64	134.66	1.32	918.3PDD0.107E-150.	3.90E-170.	0.
52058625.383	-44.61	134.69	1.32	918.3PDD0.427E-160.	0.	0.
52058625.767	-44.59	134.73	1.33	918.3PDD0.106E-150.	2.68E-170.	0.
52058626.350	-44.56	134.77	1.33	918.3PDD0.	0.	0.
52058627.217	-44.54	134.81	1.33	918.3PDD0.	0.137E-170.	0.
52058627.783	-44.51	134.85	1.34	918.3PDD0.	0.179E-160.	0.
52058628.850	-44.48	134.89	1.34	918.3PDD0.264E-150.	9.78E-170.	0.
52058629.633	-44.46	134.93	1.34	918.3PDD0.	0.337E-180.	0.
52058630.300	-44.43	134.97	1.34	918.3PDD0.236E-150.	7.61E-170.	0.
52058631.066	-44.41	135.01	1.35	918.2PDD0.339E-160.	1.76E-160.	0.
52058631.750	-44.38	135.04	1.35	918.2PDD0.745E-160.	5.93E-170.	0.
52058632.433	-44.35	135.08	1.35	918.2PDD0.	0.	0.
52058632.916	-44.33	135.12	1.35	918.2PDD0.400E-150.	0.	0.
52058633.399	-44.30	135.16	1.36	918.2PDD0.	0.128E-170.	0.
52058633.982	-44.28	135.20	1.36	918.2PDD0.	0.	0.
52058634.916	-44.25	135.23	1.36	918.2PDD0.	0.363E-170.	0.
52058635.899	-44.22	135.27	1.37	918.2PDD0.247E-150.	1.17E-160.	0.
52058636.582	-44.20	135.31	1.37	918.1PDD0.221E-150.	4.77E-170.	0.
52058636.866	-44.17	135.34	1.37	918.1PDD0.463E-150.	1.48E-160.	0.
52058638.032	-44.15	135.38	1.37	918.1PDD0.224E-150.	4.79E-170.	0.
52058638.616	-44.12	135.42	1.38	918.1PDD0.354E-150.	2.61E-170.	0.
52058639.382	-44.09	135.45	1.38	918.1PDD0.529E-150.	9.55E-170.	0.
52058639.966	-44.07	135.49	1.38	918.1PDD0.359E-150.	4.66E-170.	0.
52058640.832	-44.04	135.53	1.38	918.1PDD0.572E-150.	7.17E-170.	0.
52058641.516	-44.02	135.56	1.39	918.0PDD0.337E-170.	2.49E-170.	0.
52058641.616	-43.99	135.60	1.39	918.0PDD0.385E-150.	0.	0.
52058642.965	-43.97	135.64	1.39	918.0PDD0.	0.393E-170.	0.
52058643.648	-43.94	135.68	1.39	918.0PDD0.311E-150.	0.	0.
52058644.314	-43.91	135.71	1.40	918.0PDD0.983E-160.	6.95E-170.	0.
52058644.698	-43.89	135.75	1.40	918.0PDD0.572E-150.	1.00E-160.	0.
52058645.765	-43.86	135.79	1.40	918.0PDD0.	0.915E-170.	0.
52058646.348	-43.84	135.82	1.40	917.9PDD0.	0.676E-170.	0.
52058646.948	-43.81	135.86	1.41	917.9PDD0.	0.331E-160.	0.
52058647.798	-43.78	135.90	1.41	917.9PDD0.745E-160.	5.93E-170.	0.
52058648.181	-43.76	135.93	1.41	917.9PDD0.212E-150.	1.00E-160.	0.
52058649.148	-43.73	135.97	1.42	917.9PDD0.165E-150.	1.42E-160.	0.
52058649.531	-43.71	136.01	1.42	917.9PDD0.214E-150.	9.63E-170.	0.
52058650.598	-43.68	136.04	1.42	917.9PDD0.299E-150.	1.13E-160.	0.
52058651.281	-43.65	136.08	1.42	917.8PDD0.297E-150.	9.15E-170.	0.
52058652.064	-43.63	136.12	1.43	917.8PDD0.209E-150.	1.34E-170.	0.
52058652.648	-43.60	136.16	1.43	917.8PDD0.209E-150.	0.	0.
52058652.931	-43.57	136.20	1.43	917.8PDD0.351E-160.	7.17E-170.	0.
52058653.897	-43.54	136.24	1.43	917.8PDD0.308E-150.	5.33E-170.	0.
52058654.580	-43.51	136.27	1.44	917.7PDD0.332E-160.	1.27E-170.	0.
52058654.897	-43.49	136.31	1.44	917.7PDD0.476E-150.	1.31E-170.	0.
52058656.130	-43.46	136.35	1.44	917.7PDD0.193E-150.	2.60E-170.	0.
52058656.414	-43.43	136.39	1.45	917.7PDD0.237E-150.	6.91E-170.	0.
52058657.580	-43.40	136.43	1.45	917.7PDD0.282E-150.	1.16E-170.	0.
52058658.347	-43.37	136.47	1.45	917.6PDD0.	0.107E-160.	0.
52058658.930	-43.35	136.50	1.45	917.6PDD0.864E-160.	9.58E-170.	0.
52058659.713	-43.32	136.54	1.46	917.6PDD0.279E-160.	2.48E-170.	0.
52058660.381	-43.29	136.58	1.46	917.6PDD0.	0.110E-160.	0.
52058660.965	-43.26	136.62	1.46	917.6PDD0.276E-160.	9.95E-170.	0.

5.0	20.00.565E	010.122E	010.146E-0058619.869	0.000	0.	0.0000.111E-08	-8.95625	5055.
5.0	20.00.565E	010.122E	010.146E-0058619.885	0.000	8.547	0.0000.135E-08	-8.86846	5164.
5.0	20.00.565E	010.122E	010.146E-0058619.902	0.000	17.894	0.0000.130E-08	-8.88609	5142.
5.0	20.00.565E	010.122E	010.146E-0058619.918	0.000	26.841	0.0000.120E-08	-8.92125	5098.
5.0	20.00.565E	010.122E	010.146E-0058619.935	0.000	35.788	0.0000.111E-08	-8.95625	5055.
5.0	20.00.565E	010.122E	010.146E-0058619.952	0.000	44.598	0.0000.106E-08	-8.97369	5033.
5.0	20.00.565E	010.122E	010.146E-0058619.969	0.000	53.945	0.0000.981E-09	-9.00445	4989.
5.0	20.00.565E	010.122E	010.146E-0058619.985	0.000	62.892	0.0000.102E-08	-8.99109	5011.
5.0	20.00.565E	010.122E	010.146E-0058620.002	0.000	71.839	0.0000.130E-08	-8.88609	5142.
5.0	20.00.565E	010.122E	010.146E-0058620.019	0.000	80.786	0.0000.126E-08	-8.89935	5126.
5.0	20.00.565E	010.122E	010.146E-0058620.035	0.000	89.733	0.0000.121E-08	-8.91696	5104.
5.0	20.00.565E	010.122E	010.146E-0058620.052	0.000	98.680	0.0000.116E-08	-8.93454	5082.
5.0	20.00.565E	010.122E	010.146E-0058620.068	0.000	107.627	0.0000.106E-08	-8.97369	5033.
5.0	20.00.565E	010.122E	010.146E-0058620.085	0.000	116.573	0.0000.111E-08	-8.95625	5055.
5.0	20.00.565E	010.122E	010.146E-0058620.102	0.000	125.784	0.0000.102E-08	-8.99109	5011.
5.0	20.00.565E	010.122E	010.146E-0058620.119	0.000	134.731	0.0000.102E-08	-8.99109	5011.
5.0	20.00.565E	010.122E	010.146E-0058620.135	0.000	143.677	0.0000.125E-08	-8.90369	5120.
5.0	20.00.565E	010.122E	010.146E-0058620.152	0.000	152.624	0.0000.125E-08	-8.90369	5120.
5.0	20.00.565E	010.122E	010.146E-0058620.168	0.000	161.571	0.0000.120E-08	-8.92125	5098.
5.0	20.00.565E	010.122E	010.146E-0058620.185	0.000	170.518	0.0000.120E-08	-8.92125	5098.
5.0	20.00.565E	010.122E	010.146E-0058620.202	0.000	179.728	0.0000.111E-08	-8.95625	5055.
5.0	20.00.565E	010.122E	010.146E-0058620.219	0.000	188.675	0.0000.102E-08	-8.99109	5011.
5.0	20.00.565E	010.122E	010.146E-0058620.235	0.000	197.622	0.0000.942E-09	-9.02576	4968.
5.0	20.00.565E	010.122E	010.146E-0058620.252	0.000	206.569	0.0000.120E-08	-8.92125	5098.
5.0	20.00.565E	010.122E	010.146E-0058620.269	0.000	215.516	0.0000.130E-08	-8.88609	5142.
5.0	20.00.565E	010.122E	010.146E-0058620.285	0.000	224.463	0.0000.130E-08	-8.88609	5142.
5.0	20.00.565E	010.122E	010.146E-0058620.302	0.000	233.410	0.0000.115E-08	-8.93877	5077.
5.0	20.00.565E	010.122E	010.146E-0058620.318	0.000	242.357	0.0000.110E-08	-8.96041	5049.
5.0	20.00.565E	010.122E	010.146E-0058620.335	0.000	251.304	0.0000.101E-08	-8.99514	5006.
5.0	20.00.565E	010.122E	010.146E-0058620.352	0.000	260.514	0.0000.972E-09	-9.01244	4984.
5.0	20.00.565E	010.122E	010.146E-0058620.369	0.000	0.	0.0000.981E-09	-9.00845	4989.
5.0	20.00.565E	010.122E	010.146E-0058620.385	0.000	8.947	0.0000.135E-08	-8.86846	5164.
5.0	20.00.565E	010.122E	010.146E-0058620.402	0.000	17.894	0.0000.125E-08	-8.90369	5120.
5.0	20.00.565E	010.122E	010.146E-0058620.418	0.000	26.841	0.0000.121E-08	-8.91696	5104.
5.0	20.00.565E	010.122E	010.146E-0058620.435	0.000	35.788	0.0000.112E-08	-8.95208	5060.
5.0	20.00.565E	010.122E	010.146E-0058620.452	0.000	44.598	0.0000.107E-08	-8.96957	5038.
5.0	20.00.565E	010.122E	010.146E-0058620.469	0.000	53.945	0.0000.111E-08	-8.95625	5055.
5.0	20.00.565E	010.122E	010.146E-0058620.485	0.000	62.892	0.0000.102E-08	-8.99109	5011.
5.0	20.00.565E	010.122E	010.146E-0058620.502	0.000	71.839	0.0000.115E-08	-8.93877	5077.
5.0	20.00.565E	010.122E	010.146E-0058620.519	0.000	80.786	0.0000.125E-08	-8.90369	5120.
5.0	20.00.565E	010.122E	010.146E-0058620.535	0.000	89.733	0.0000.120E-08	-8.92125	5098.
5.0	20.00.565E	010.122E	010.146E-0058620.552	0.000	98.680	0.0000.115E-08	-8.93877	5077.
5.0	20.00.565E	010.122E	010.146E-0058620.568	0.000	107.627	0.0000.121E-08	-8.91696	5104.
5.0	20.00.565E	010.122E	010.146E-0058620.585	0.000	116.573	0.0000.112E-08	-8.95208	5060.
5.0	20.00.565E	010.122E	010.146E-0058620.602	0.000	125.784	0.0000.103E-08	-8.98702	5016.
5.0	20.00.565E	010.122E	010.146E-0058620.619	0.000	134.731	0.0000.942E-09	-9.02576	4968.
5.0	20.00.565E	010.122E	010.146E-0058620.635	0.000	143.677	0.0000.125E-08	-8.90369	5120.
5.0	20.00.565E	010.122E	010.146E-0058620.652	0.000	152.624	0.0000.125E-08	-8.90369	5120.
5.0	20.00.565E	010.122E	010.146E-0058620.668	0.000	161.571	0.0000.131E-08	-8.88170	5148.
5.0	20.00.565E	010.122E	010.146E-0058620.685	0.000	170.518	0.0000.121E-08	-8.91696	5104.
5.0	20.00.565E	010.122E	010.146E-0058620.702	0.000	179.728	0.0000.112E-08	-8.95208	5060.
5.0	20.00.565E	010.122E	010.146E-0058620.719	0.000	188.675	0.0000.103E-08	-8.98702	5016.
5.0	20.00.565E	010.122E	010.146E-0058620.735	0.000	197.622	0.0000.993E-09	-9.00443	4994.
5.0	20.00.565E	010.122E	010.146E-0058620.752	0.000	206.569	0.0000.107E-08	-8.96957	5038.
5.0	20.00.565E	010.122E	010.146E-0058620.769	0.000	215.516	0.0000.135E-08	-8.86846	5164.
5.0	20.00.565E	010.122E	010.146E-0058620.785	0.000	224.463	0.0000.125E-08	-8.90369	5120.
5.0	20.00.565E	010.122E	010.146E-0058620.802	0.000	233.410	0.0000.120E-08	-8.92125	5098.
5.0	20.00.565E	010.122E	010.146E-0058620.818	0.000	242.357	0.0000.111E-08	-8.95625	5055.
5.0	20.00.565E	010.122E	010.146E-0058620.835	0.000	251.304	0.0000.102E-08	-8.99109	5011.
5.0	20.00.565E	010.122E	010.146E-0058620.852	0.000	260.514	0.0000.106E-08	-8.97369	5033.

PRESSURE PLOT TAPE OUTPUT (C5)

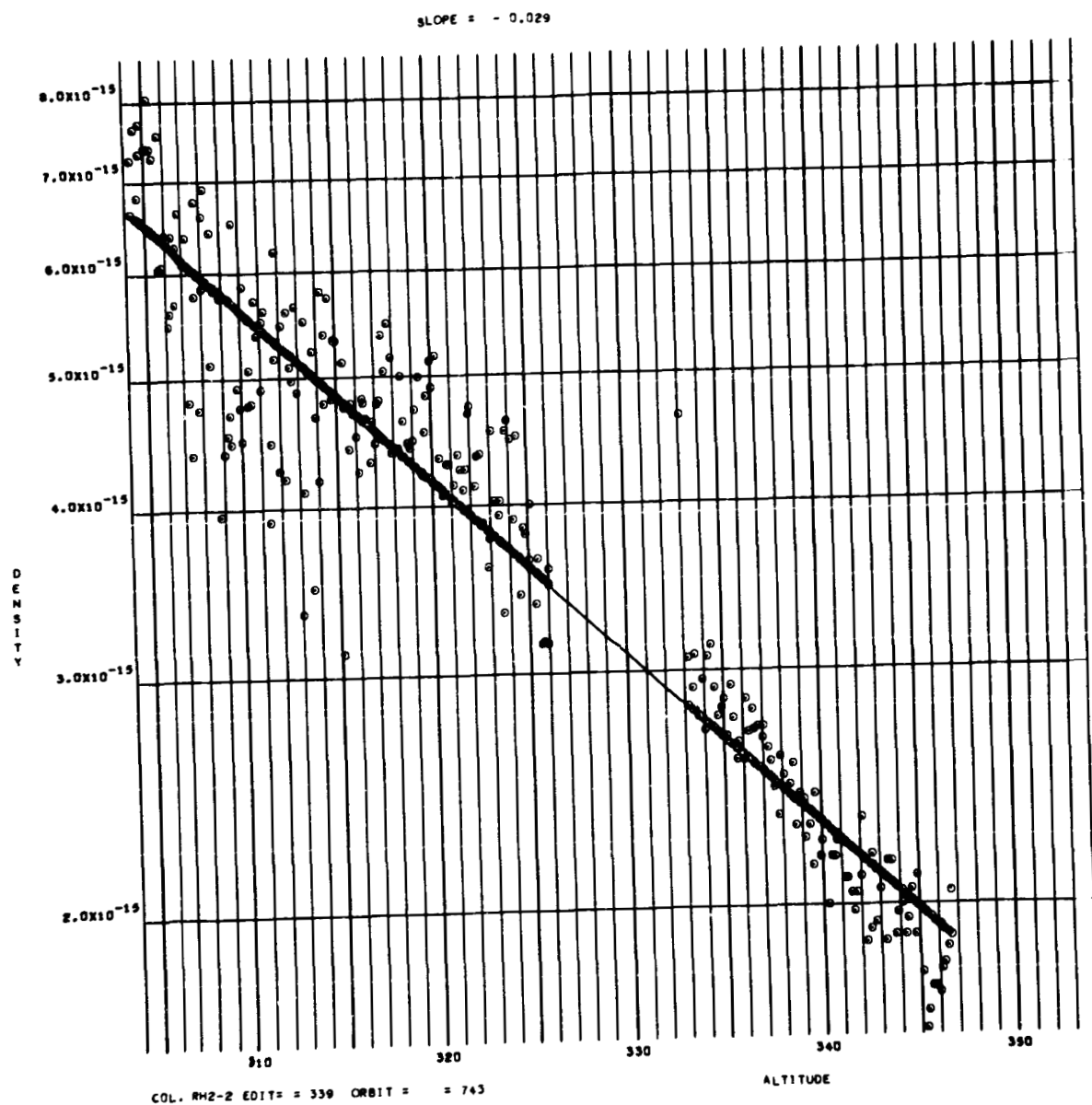
EDIT = 327 ORBIT = 711

5.0	20.00.209E-060.213E	010.101E	0958619.862	7.549	0.	7.5490.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958619.879	7.549	8.947	7.4580.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958619.896	7.549	17.894	7.1850.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958619.912	7.549	26.841	6.7380.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958619.929	7.248	35.788	6.1300.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.101E	0958619.946	7.549	44.598	5.3550.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958619.962	7.549	53.945	4.4850.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958619.979	7.549	62.892	3.5450.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958619.996	7.549	71.839	2.6000.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.012	7.344	80.786	1.7360.730E-07	-7.13665	7329.
5.0	20.00.209E-060.213E	010.101E	0958620.029	7.037	89.733	1.0370.700E-07	-7.15520	7306.
5.0	20.00.209E-060.213E	010.101E	0958620.045	7.037	98.680	0.5500.700E-07	-7.15520	7306.
5.0	20.00.209E-060.213E	010.101E	0958620.062	7.248	107.627	0.2590.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.101E	0958620.079	7.549	116.573	0.1110.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.096	7.549	125.784	0.0440.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.112	7.549	134.731	0.0180.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.129	7.549	143.677	0.0070.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.146	7.549	152.624	0.0030.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.162	7.248	161.571	0.0020.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.101E	0958620.179	7.248	170.518	0.0010.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.101E	0958620.196	7.248	179.728	0.0010.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.101E	0958620.212	7.549	188.675	0.0010.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.229	7.549	197.622	0.0020.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.246	7.549	206.569	0.0030.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.262	7.549	215.516	0.0070.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.101E	0958620.279	7.248	224.463	0.0160.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.101E	0958620.295	7.248	233.410	0.0400.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.101E	0958620.312	7.760	242.357	0.1000.771E-07	-7.11271	7359.
5.0	20.00.209E-060.213E	010.979E	0858620.329	7.549	0.	7.5490.771E-07	-7.11271	7359.
5.0	20.00.209E-060.213E	010.979E	0858620.346	7.549	9.210	7.4520.771E-07	-7.11271	7359.
5.0	20.00.209E-060.213E	010.979E	0858620.362	7.345	18.157	7.1740.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.379	7.052	27.104	6.7230.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.979E	0858620.396	7.345	36.051	6.1100.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.412	7.145	44.598	5.3550.730E-07	-7.13665	7329.
5.0	20.00.209E-060.213E	010.979E	0858620.429	7.145	53.945	4.4850.730E-07	-7.13665	7329.
5.0	20.00.209E-060.213E	010.979E	0858620.446	7.145	63.155	3.5170.730E-07	-7.13665	7329.
5.0	20.00.209E-060.213E	010.979E	0858620.462	7.345	72.102	2.5730.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.479	7.052	81.049	1.7130.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.979E	0858620.496	7.345	89.996	1.0200.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.512	7.345	98.943	0.5300.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.529	7.345	107.890	0.2510.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.545	7.345	116.837	0.1090.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.562	7.145	125.784	0.0440.730E-07	-7.13665	7329.
5.0	20.00.209E-060.213E	010.979E	0858620.579	7.145	134.731	0.0180.730E-07	-7.13665	7329.
5.0	20.00.209E-060.213E	010.979E	0858620.596	6.845	143.941	0.0070.700E-07	-7.15520	7306.
5.0	20.00.209E-060.213E	010.979E	0858620.612	7.052	152.888	0.0030.721E-07	-7.14231	7322.
5.0	20.00.209E-060.213E	010.979E	0858620.629	7.345	161.835	0.0020.750E-07	-7.12465	7344.
5.0	20.00.209E-060.213E	010.979E	0858620.646	7.385	170.781	0.0010.755E-07	-7.12226	7347.
5.0	20.00.209E-060.213E	010.979E	0858620.662	7.184	179.728	0.0010.734E-07	-7.13426	7332.
5.0	20.00.209E-060.213E	010.979E	0858620.679	7.184	188.675	0.0010.734E-07	-7.13426	7332.
5.0	20.00.209E-060.213E	010.979E	0858620.696	7.184	197.885	0.0020.734E-07	-7.13426	7332.
5.0	20.00.209E-060.213E	010.979E	0858620.712	7.184	206.832	0.0070.734E-07	-7.13426	7332.
5.0	20.00.209E-060.213E	010.979E	0858620.729	6.894	215.779	0.0070.703E-07	-7.15281	7309.
5.0	20.00.209E-060.213E	010.979E	0858620.746	6.834	224.726	0.0170.703E-07	-7.15281	7309.
5.0	20.00.209E-060.213E	010.979E	0858620.762	7.091	233.673	0.0410.725E-07	-7.13993	7325.
5.0	20.00.209E-060.213E	010.979E	0858620.779	7.385	242.620	0.1070.755E-07	-7.12226	7347.
5.0	20.00.209E-060.213E	010.979E	0858620.795	7.385	251.567	0.2410.755E-07	-7.12226	7347.
5.0	20.00.209E-060.213E	010.979E	0858620.812	7.385	260.514	0.5160.755E-07	-7.12226	7347.
5.0	20.00.209E-060.213E	010.979E	0858620.829	7.385	269.461	0.9840.755E-07	-7.12226	7347.
5.0	20.00.209E-060.213E	010.979E	0858620.846	7.385	278.671	1.6890.755E-07	-7.12226	7347.

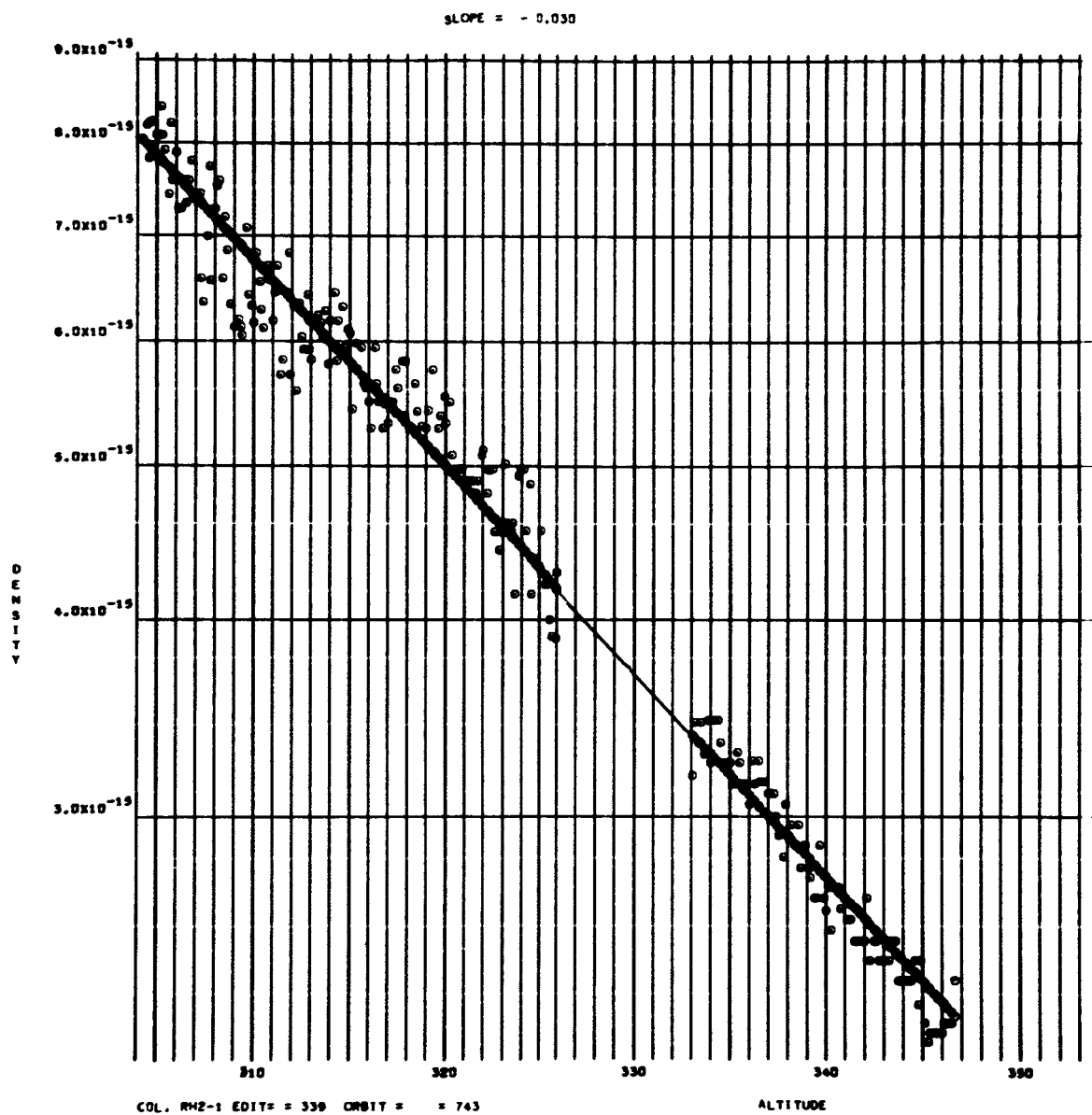
5.0	20.00.209E-060.213E	010.257E	1158619.301	7.549	0.	7.5490.293E-09	-9.53268	4334.
5.0	20.00.209E-060.213E	010.257E	1158619.317	8.753	8.547	7.4580.340E-09	-9.46842	4414.
5.0	20.00.209E-060.213E	010.257E	1158619.334	8.124	17.694	7.1850.316E-09	-9.50083	4374.
5.0	20.00.209E-060.213E	010.257E	1158619.351	7.025	27.104	6.7230.273E-09	-9.56394	4295.
5.0	20.00.209E-060.213E	010.257E	1158619.368	6.372	36.051	6.1100.248E-09	-9.60634	4242.
5.0	20.00.209E-060.213E	010.257E	1158619.384	5.564	44.598	5.3550.216E-09	-9.66523	4168.
5.0	20.00.209E-060.213E	010.257E	1158619.401	8.196	53.545	4.4850.318E-09	-9.49699	4379.
5.0	20.00.209E-060.213E	010.257E	1158619.417	8.431	62.892	3.5450.328E-09	-9.48470	4394.
5.0	20.00.209E-060.213E	010.257E	1158619.434	7.830	71.839	2.6000.304E-09	-9.51683	4354.
5.0	20.00.209E-060.213E	010.257E	1158619.451	7.025	81.049	1.7130.273E-09	-9.56394	4295.
5.0	20.00.209E-060.213E	010.257E	1158619.468	6.110	89.596	1.0200.237E-09	-9.62457	4219.
5.0	20.00.209E-060.213E	010.257E	1158619.484	5.347	98.943	0.5380.208E-09	-9.68246	4147.
5.0	20.00.209E-060.213E	010.257E	1158619.501	8.431	107.890	0.2530.328E-09	-9.48470	4394.
5.0	20.00.209E-060.213E	010.257E	1158619.518	8.124	116.837	0.1080.316E-09	-9.50083	4374.
5.0	20.00.209E-060.213E	010.257E	1158619.534	7.549	125.784	0.0440.293E-09	-9.53268	4334.
5.0	20.00.209E-060.213E	010.257E	1158619.551	6.780	134.731	0.0180.263E-09	-9.57934	4276.
5.0	20.00.209E-060.213E	010.257E	1158619.567	5.949	143.677	0.0070.231E-09	-9.63614	4205.
5.0	20.00.209E-060.213E	010.257E	1158619.584	5.752	152.624	0.0030.223E-09	-9.65077	4187.
5.0	20.00.209E-060.213E	010.257E	1158619.601	8.508	161.635	0.0020.331E-09	-9.48077	4399.
5.0	20.00.209E-060.213E	010.257E	1158619.618	8.124	170.781	0.0010.316E-09	-9.50083	4374.
5.0	20.00.209E-060.213E	010.257E	1158619.634	7.549	179.728	0.0010.293E-09	-9.53268	4334.
5.0	20.00.209E-060.213E	010.257E	1158619.651	6.547	188.675	0.0010.254E-09	-9.59458	4257.
5.0	20.00.209E-060.213E	010.257E	1158619.667	5.906	197.622	0.0020.229E-09	-9.63931	4201.
5.0	20.00.209E-060.213E	010.257E	1158619.684	6.780	206.569	0.0030.263E-09	-9.57934	4276.
5.0	20.00.209E-060.213E	010.257E	1158619.701	8.431	215.779	0.0070.328E-09	-9.48470	4394.
5.0	20.00.209E-060.213E	010.257E	1158619.718	7.830	224.726	0.0170.304E-09	-9.51683	4354.
5.0	20.00.209E-060.213E	010.257E	1158619.734	7.281	233.673	0.0410.283E-09	-9.54839	4315.
5.0	20.00.209E-060.213E	010.257E	1158619.751	6.547	242.620	0.1030.254E-09	-9.59458	4257.
5.0	20.00.209E-060.213E	010.257E	1158619.768	5.711	251.567	0.2410.222E-09	-9.65387	4183.
5.0	20.00.209E-060.213E	010.257E	1158619.784	7.830	260.514	0.5160.304E-09	-9.51683	4354.
5.0	20.00.209E-060.213E	010.257E	1158619.801	8.431	269.461	0.9840.328E-09	-9.48470	4394.
5.0	20.00.209E-060.213E	010.257E	1158619.817	7.830	278.408	1.6650.304E-09	-9.51683	4354.
5.0	20.00.209E-060.213E	010.257E	1158619.834	7.549	287.355	2.5170.293E-09	-9.53268	4334.
5.0	20.00.209E-060.213E	010.257E	1158619.851	6.323	296.565	3.4870.246E-09	-9.60966	4238.
5.0	20.00.209E-060.213E	010.257E	1158619.868	5.525	305.512	4.4300.215E-09	-9.66826	4165.
5.0	20.00.209E-060.213E	010.257E	1158619.884	8.124	314.459	5.3050.316E-09	-9.50083	4374.
5.0	20.00.209E-060.213E	010.257E	1158619.901	8.753	323.406	6.0640.340E-09	-9.46842	4414.
5.0	20.00.209E-060.213E	010.257E	1158619.917	7.830	332.353	6.6900.304E-09	-9.51683	4354.
5.0	20.00.209E-060.213E	010.257E	1158619.934	7.025	341.300	7.1520.273E-09	-9.56394	4295.
5.0	20.00.209E-060.213E	010.257E	1158619.951	6.110	350.510	7.4460.237E-09	-9.62457	4219.
5.0	20.00.209E-060.213E	010.257E	1158619.968	5.347	359.457	7.5490.208E-09	-9.68246	4147.
5.0	20.00.209E-060.213E	010.257E	1158619.984	8.431	368.404	7.4680.328E-09	-9.48470	4394.
5.0	20.00.209E-060.213E	010.257E	1158620.001	8.124	377.351	7.2070.316E-09	-9.50083	4374.
5.0	20.00.209E-060.213E	010.257E	1158620.018	7.614	386.298	6.7700.296E-09	-9.52899	4339.
5.0	20.00.209E-060.213E	010.257E	1158620.034	6.835	395.245	6.1710.266E-09	-9.57587	4280.
5.0	20.00.209E-060.213E	010.257E	1158620.051	6.156	404.192	5.4280.239E-09	-9.62132	4223.
5.0	20.00.209E-060.213E	010.316E	1158620.067	7.549	C.	7.5490.237E-09	-9.62457	4219.
5.0	20.00.209E-060.213E	010.316E	1158620.084	11.668	8.947	7.4580.367E-09	-9.43549	4456.
5.0	20.00.209E-060.213E	010.316E	1158620.101	10.816	18.157	7.1740.340E-09	-9.46842	4414.
5.0	20.00.209E-060.213E	010.316E	1158620.118	8.997	27.104	6.7230.283E-09	-9.54839	4315.
5.0	20.00.209E-060.213E	010.316E	1158620.134	8.089	36.051	6.1100.254E-09	-9.59458	4257.
5.0	20.00.209E-060.213E	010.316E	1158620.151	7.057	44.998	5.3550.222E-09	-9.65387	4183.
5.0	20.00.209E-060.213E	010.316E	1158620.167	8.680	53.945	4.4850.273E-09	-9.56394	4295.
5.0	20.00.209E-060.213E	010.316E	1158620.184	10.418	62.892	3.5450.328E-09	-9.48470	4394.
5.0	20.00.209E-060.213E	010.316E	1158620.201	10.038	72.102	2.5730.316E-09	-9.50083	4374.
5.0	20.00.209E-060.213E	010.316E	1158620.218	8.997	81.049	1.7130.283E-09	-9.54839	4315.
5.0	20.00.209E-060.213E	010.316E	1158620.234	7.813	89.596	1.0200.246E-09	-9.60966	4238.
5.0	20.00.209E-060.213E	010.316E	1158620.251	7.057	98.943	0.5380.222E-09	-9.65387	4183.
5.0	20.00.209E-060.213E	010.316E	1158620.268	9.675	107.890	0.2530.304E-09	-9.51683	4354.
5.0	20.00.209E-060.213E	010.316E	1158620.284	10.416	116.837	0.1080.328E-09	-9.48470	4394.

**SAMPLE PLOTS
FROM
SELECTED PASSES**

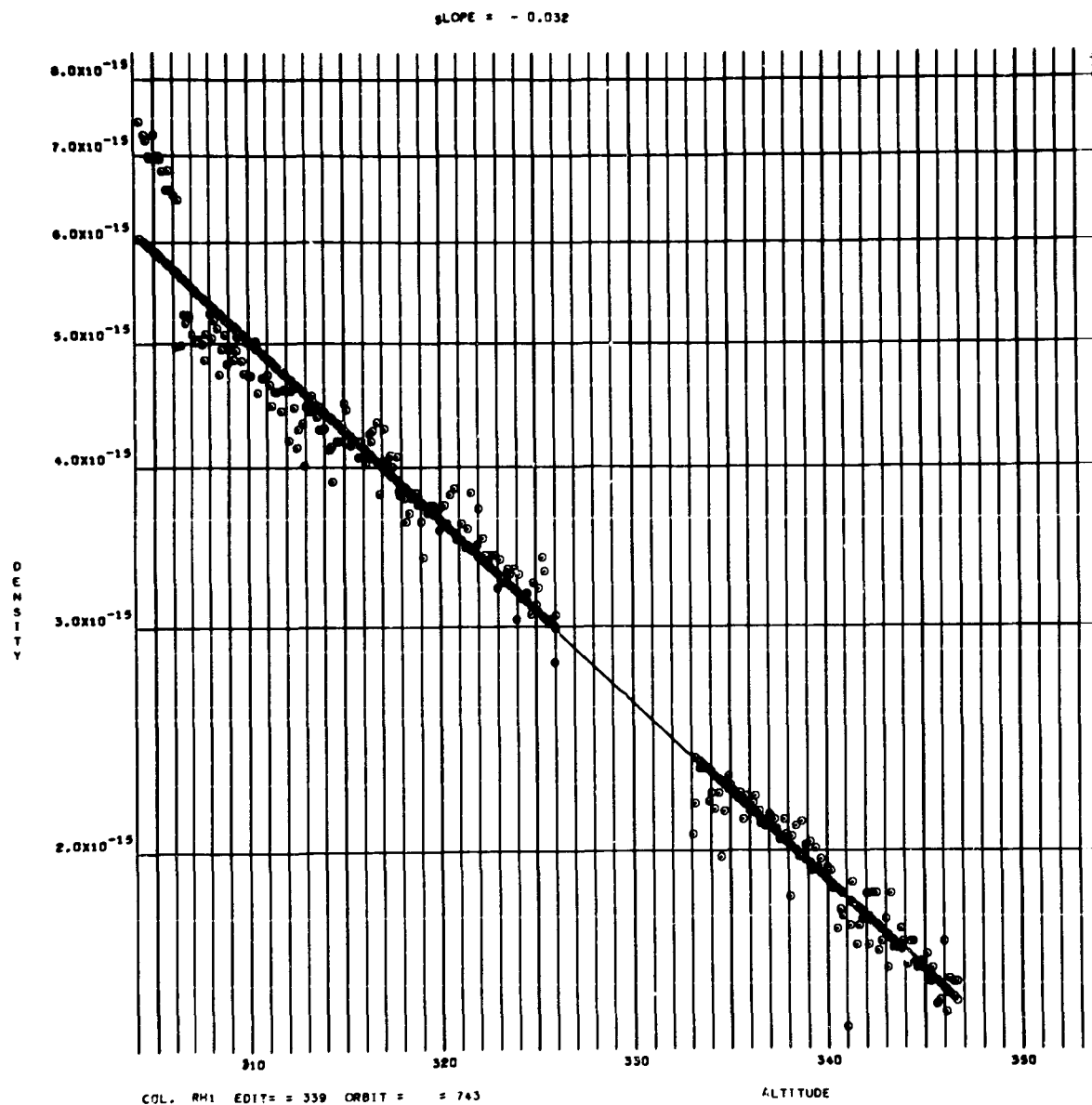
DENSITY PLOT



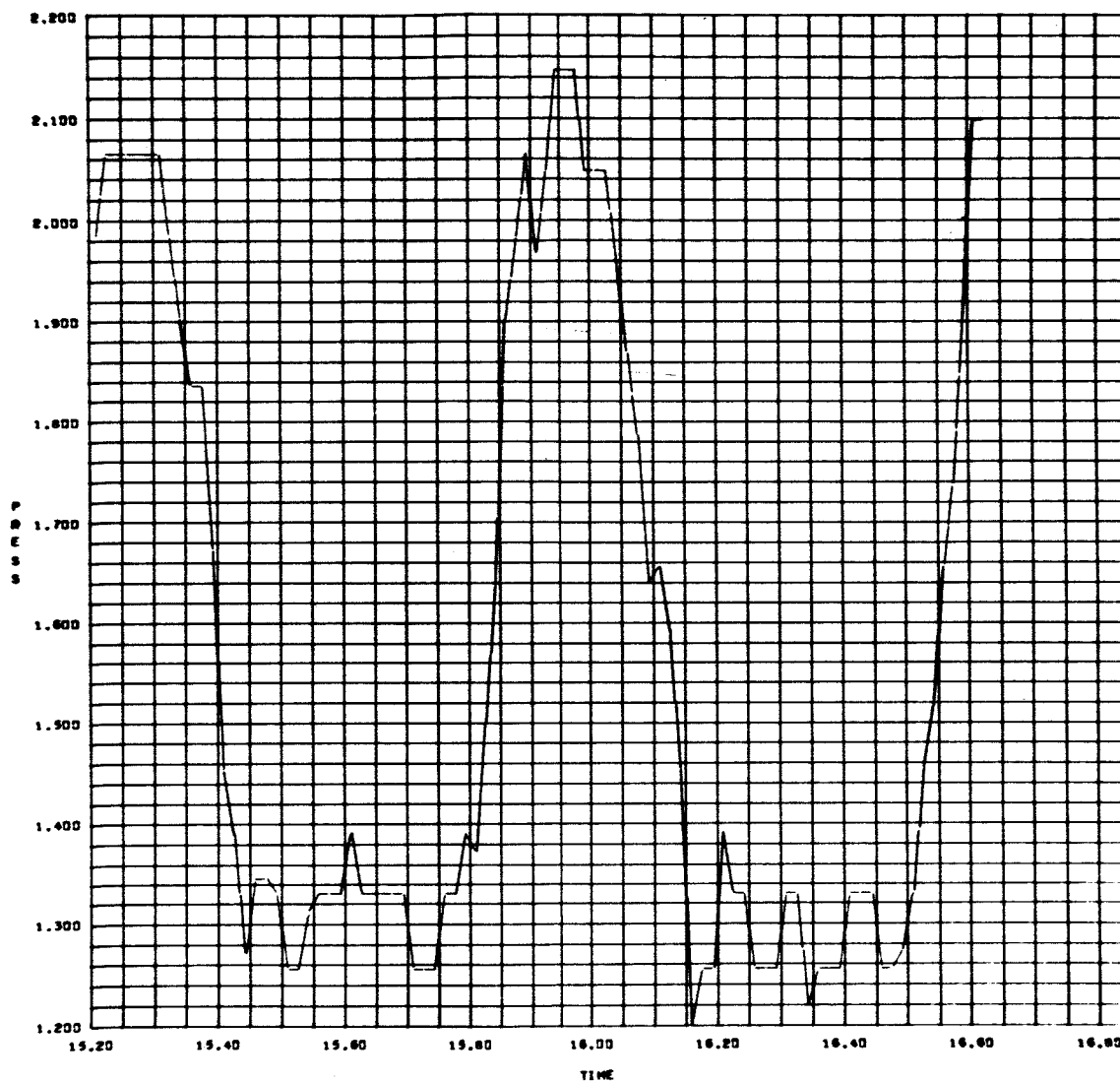
DENSITY PLOT



DENSITY PLOT

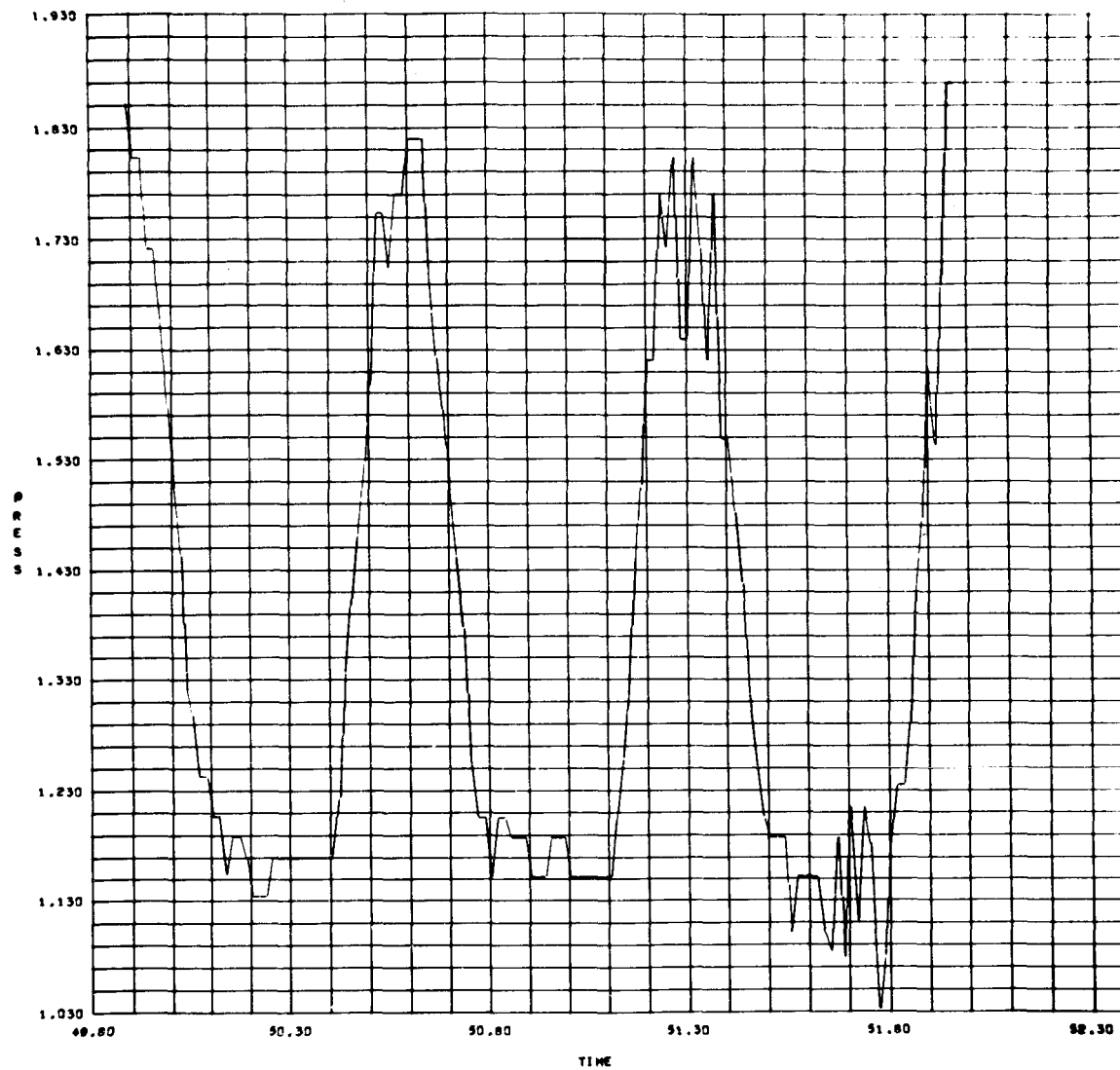


RAW PRESSURE PLOT



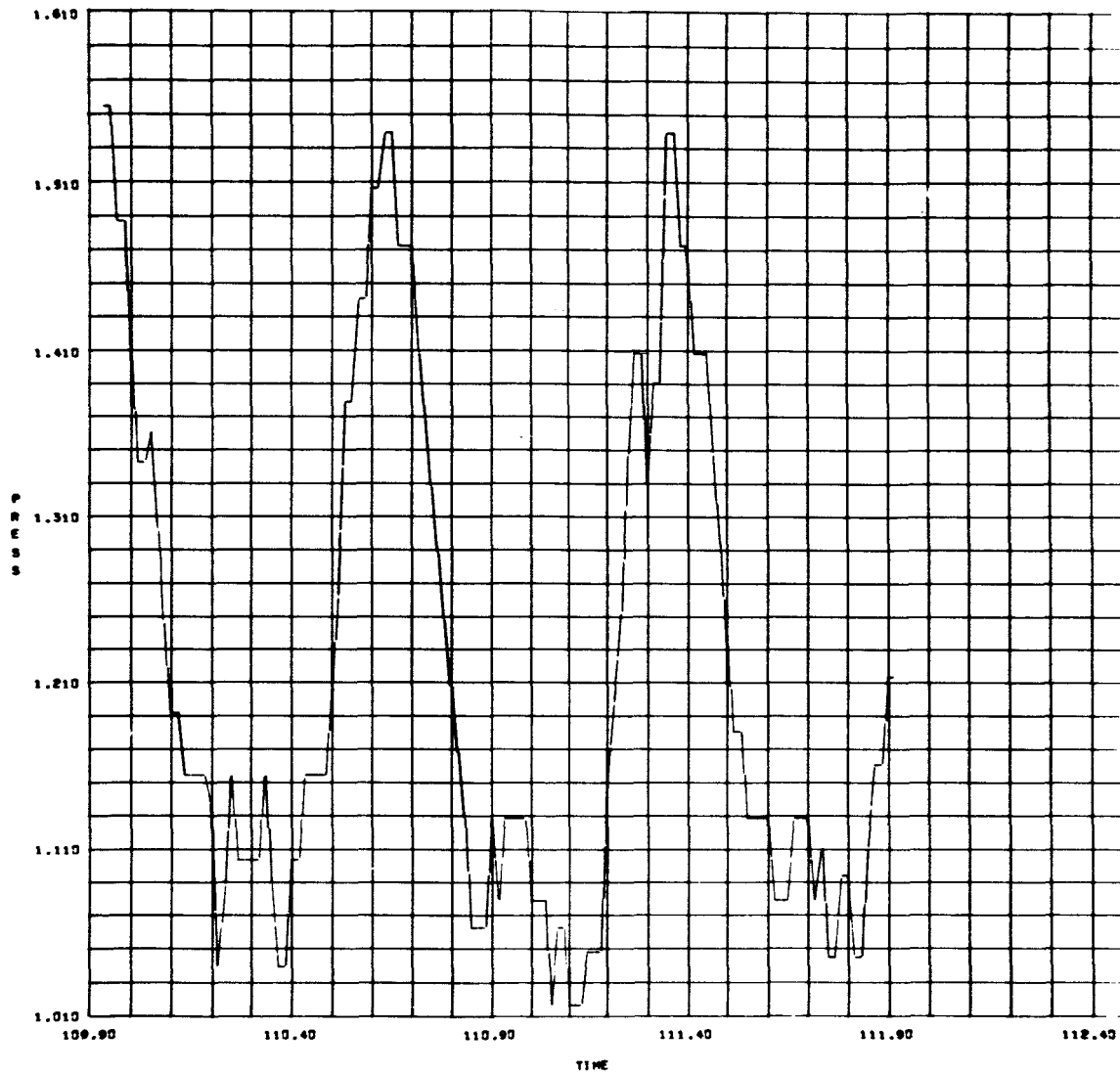
QUL. 8A2 ORBIT - 877 PRESSURE MIN - .610E-7 84015

RAW PRESSURE PLOT



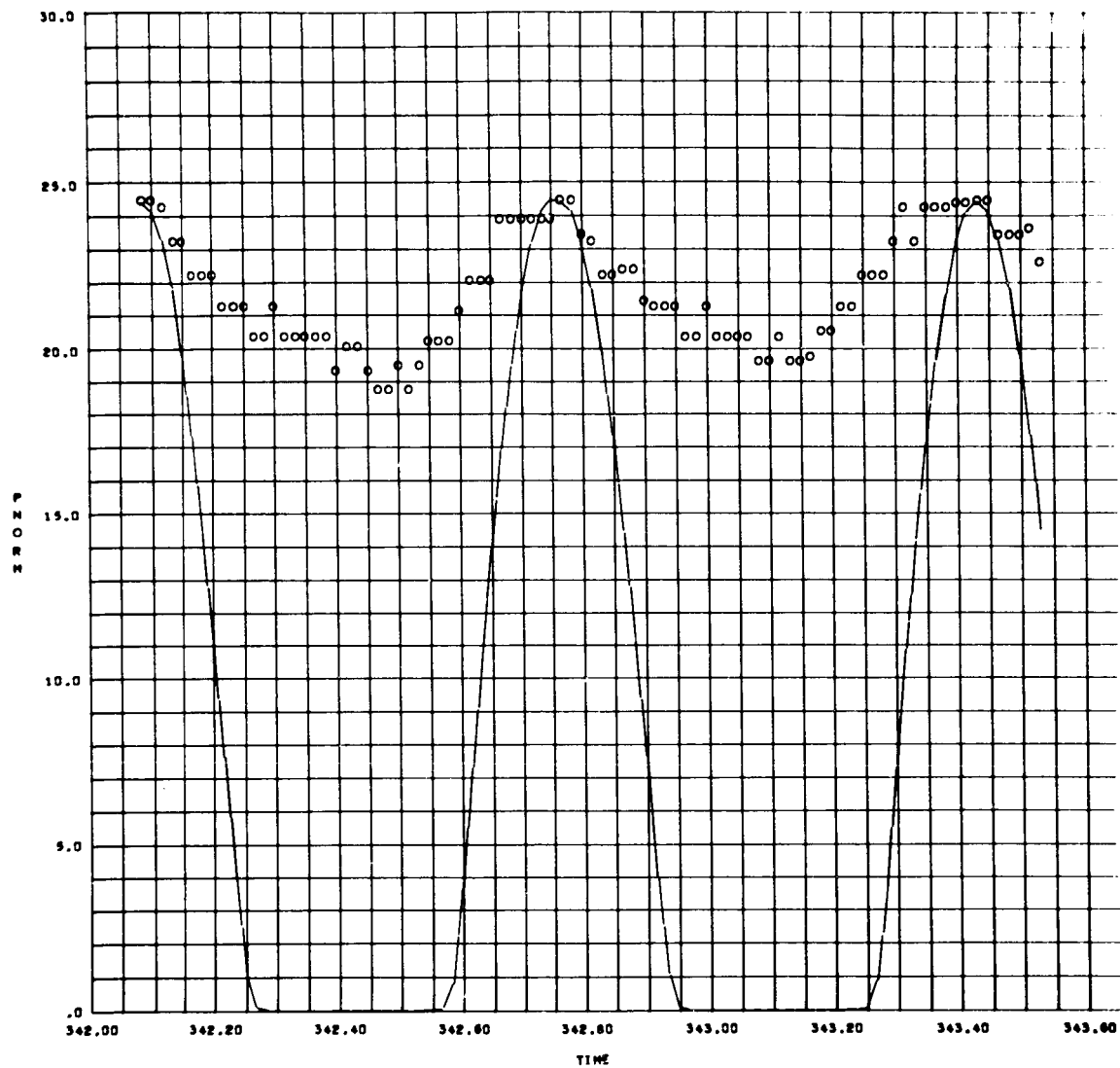
QVI. BA2 ORBIT - 877 PRESSURE MIN - .610E-7 64015

RAW PRESSURE PLOT



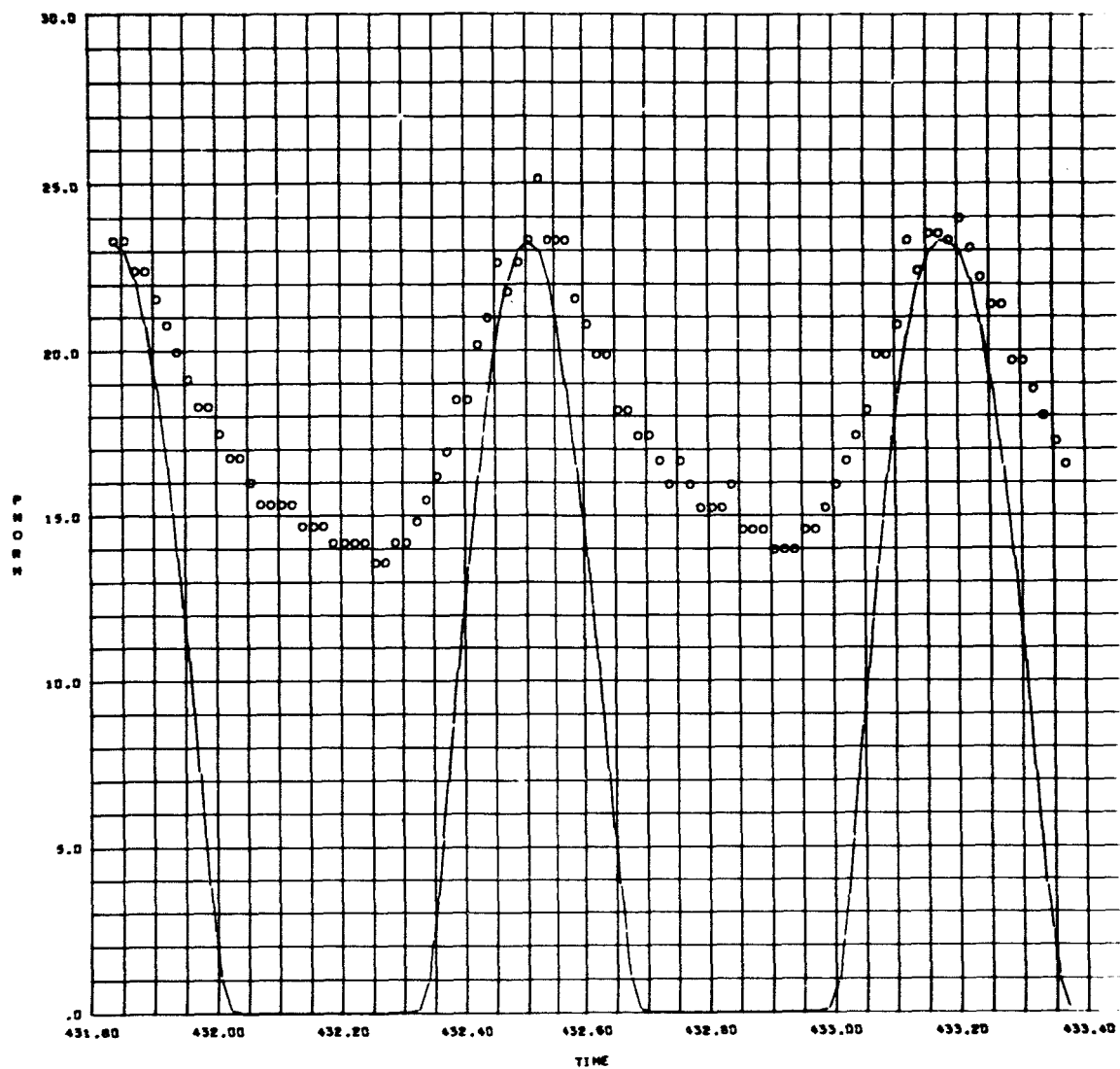
QJ1. BA2 ORBIT - 877 PRESSURE MIN - .610E-7 64015

PNORM-VPOFS PLOT



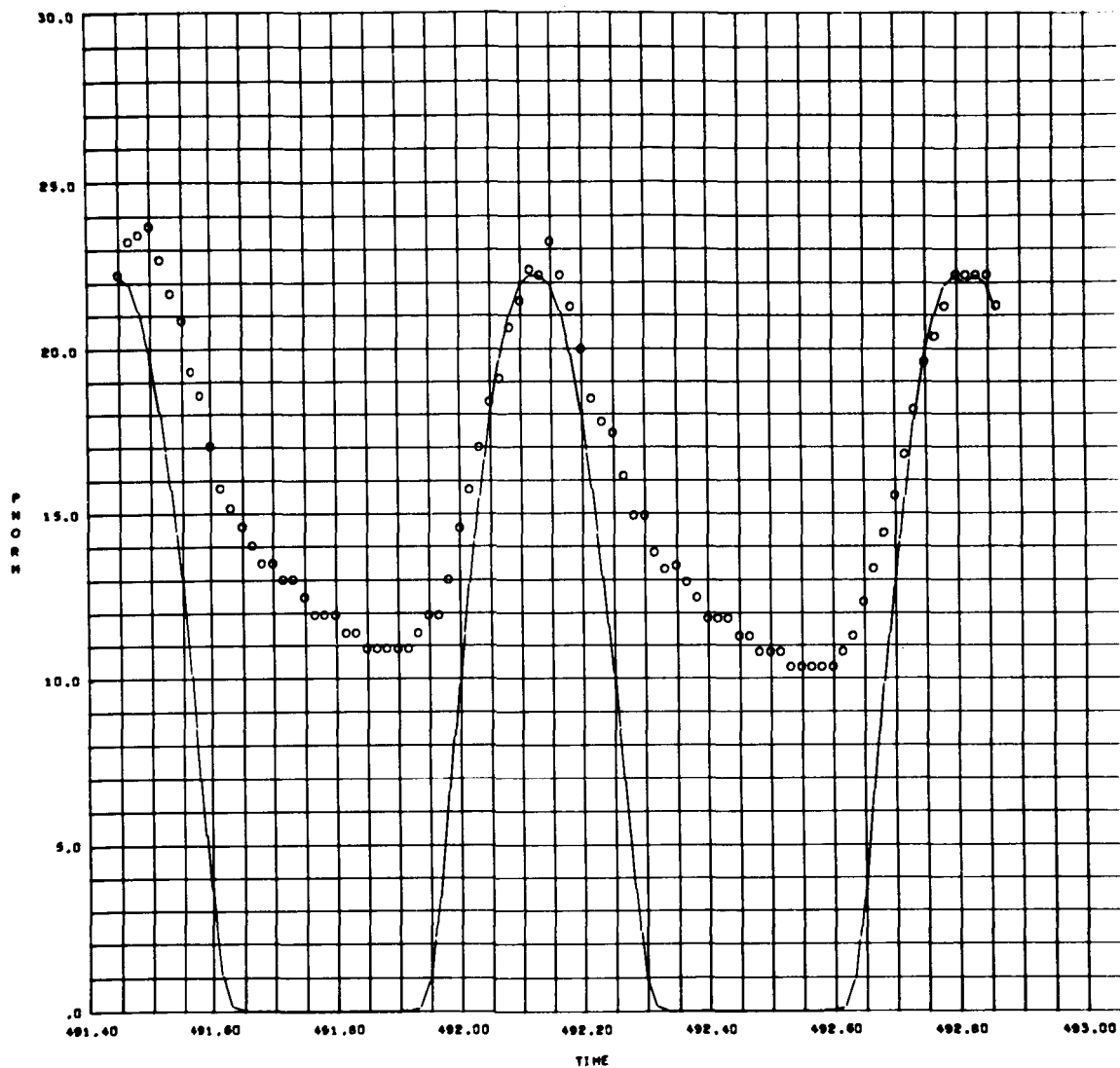
OUT. BA2 ORBIT -1300 VPOFS -LINE PNORM-CIRCLE 00001

PNORM-VPOFS PLOT



QJ1. BA2 ORBIT -1300 VPOFS -LINE PNORM-CIRCLE 00001

PNORM-VPOFS PLOT



QUI. BA2 ORBIT -1300 VPOFS -LINE PNORM-CIRCLE 00001

FORTRAN II LISTING (PDP)

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*      CHARLES J HANLEY      ROOM 22      BUILDING 11
*      PAUSE
*      XEQ
*      CARDS COLUMN
*      LIST 8
*      FORMAP
*      LABEL
C CJH
C      PRESSURE GAUGES DC OUTPUT VOLTAGES CONVERTED TO
C      CORRECTED ION CURRENT
      DIMENSION A(8),B(255),BV(18),BI(18),BV2(18),BI2(18),VC(8),RI(8),
1VC2(8),RI2(8),ELN(18),RIC(8),R2C(8),BV1(18),VC1(8),R1C(8),C(21),
2D(21),RSCX(4),RSX(4),RS1(4),RS2(4),RSC1(4),RSC2(4),P(21),T(2
31),RA1(90,4),BA2(90,4),RFD1(90,5),RFD2(90,5),E(209),F(142)
1      , XTIME(30),XALT(30),XLAT(30),XLONG(30),XLST(30),XRBA1(3
10),XPRA2(30),XRRH1(30),      XRRH2(30)
      COMMON BI,BV1,BV2,VC1,VC2,RI,RI2,XHF,XMF,XLF,X2HF,X2MF,X2LF,XHL,
1XML,XLL,X2HL,X2ML,X2LL,NEDI,NORB
1      ,XTIME,XALT,XLAT,XLONG,XLST,XRBA1,XRBA2,XRRH1,XRRH2
      NRZA = 0
8888  READ 970,NEDI,NORB
      IF(NEDI)9981,960,9981
9981  IF(NRZA)964,8889,964
8889  CALL MATCH(NEDI,NED)
      IF(NED-1)8891,964,8891
8891  IF(NRZA)964,8890,964
964   PRINT 986
      PAUSE 7777
      CALL MATCH(NEDI,NED)
      IF(NED-1)8890,8888,8890
8890  READ TAPE 15,A
      READ TAPE 5,E
      CALL DEN
      WRITE OUTPUT TAPE 6,9999,NEDI,NORB
      WRITE OUTPUT TAPE 16,9999,NEDI,NORB
      WRITE OUTPUT TAPE 25,9999,NEDI,NORB
      WRITE OUTPUT TAPE 26,9999,NEDI,NORB
9999  FORMAT(90X6HEDIT =I4,10X7HORBIT =I4)
      NRFC=F(209)
      DO 1100 JA=1,NRFC
      READ TAPE 5,F
      XTIME(JA)=F(3)
      XALT(JA)=F(12)
      XLAT(JA)=F(11)
      XLONG(JA)=F(10)
      XLST(JA)=F(13)

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XRBA1(JA)=F(61)
XRBA2(JA)=F(64)
XRRH1(JA)=F(73)
XRRH2(JA)=F(76)
1100 CONTINUE
N0X = 0
NNXZ = NRFC +1
5021 IF(NNXZ-N0X)5022,5022,5020
5020 N0X = N0X +1
BACKSPACE 5
GO TO 5021
5022 IF(A(8)-60000004.)2,3,2
C PRINT ERROR MESSAGE - WRONG TAPE
2 PRINT 200
GO TO 8888
3 A(4)=A(4)+60.
WRITE OUTPUT TAPE 3,600,A(1),NFDI,NORB,A(2),A(3),A(4),A(5),A(6),A(
18)
IF(SENSE SWITCH 2)3038,3036
3036 SENSOR=1.0
CALL PAGE(SENSOR)
3038 READ TAPE 15,R
R(2)=R(2)/1000.
JHRSMN=R(2)/3600.
HRSEC=3600*JHRSMN
RSEC=R(2)-HRSEC
MSECMN=RSEC/60.
XRB =MSECMN*60
RSEC1M=RSEC-XRB
BACKSPACE 15
WRITE OUTPUT TAPE 3,12121,JHRSMN,MSECMN,RSEC1M
C READ INPUT CURRENT TABLE FORMAT 202
READ 202,RI
961 DO 4 I=1,18
FLN(I)=LOGF(RI(I))
4 CONTINUE
C READ REDHEAD CALIBRATION VOLTAGES AND CURRENTS FOR REDHEAD 1 AND 2
READ 300,VC1,VC2
READ 303,RI,RI2
READ 305,XHL,XML,XLL,X2HL,X2ML,X2LL
READ 203,T0,TI,W0,WI,HID
READ 305,XHF,XMF,XLF,X2HF,X2MF,X2LF
C READ BAYARD ALPERT 1 CALIBRATION VOLTAGES BY FORMAT 204
READ 204,RV1
C READ BAYARD ALPERT 2 CALIBRATION VOLTAGES BY FORMAT 204
READ 204,RV2

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```

      AFTA1=19.5
      AFTA2=23.9
R     HJD=472424000000
      IPL0T=1
      TIME1=0.0
      TIME2=0.0
      TIME3=0.0
      TIME4=0.0
      ICNT=1
      JCNT=1
      KCNT=1
      JPL0T=1
      KPL0T=1
      WRITE OUTPUT TAPE 3,12222,BV1
      WRITE OUTPUT TAPE 3,13333,BV2
      WRITE OUTPUT TAPE 3,14444
      WRITE OUTPUT TAPE 3,219
      WRITE OUTPUT TAPE 3,15555,XHF,XMF,XLF,X2HF,X2MF,X2LF
      WRITE OUTPUT TAPE 3,20969,T0,T1,W0,WI
      WRITE OUTPUT TAPE 3,99570,AFTA1,AFTA2
      READ TAPE 5,F
      READ TAPE 5,F
      IF (F(133)-0.0)242,240,242
240  WRITE OUTPUT TAPE 3,949
242  BACKSPACE 5
      BACKSPACE 5
      IF (SENSE SWITCH 2)4044,4404
4404 WRITE OUTPUT TAPE 3,699
      GO TO 6111
4044 WRITE OUTPUT TAPE 3,700
      IF (SENSE SWITCH 1)711,722
722  WRITE OUTPUT TAPE 3,900
      GO TO 6111
711  WRITE OUTPUT TAPE 3,800
6111 X=1.
      DO 30 M=1,8
      R1C(M)=LOGF(RI(M))
30  CONTINUE
      DO 95 M=1,8
      R2C(M)=LOGF(RI2(M))
95  CONTINUE
      DC0N=SQRTF((2.0*83150000.*T1)/W1)
      VPI=DC0N
      VPO=SQRTF((2.0*83150000.*T0)/W0)*1.0E-05
      C0N=.05/48.
      XCNT=0.

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```

XSPIN=0.
IX=1
JX=1
II=1
MM=1
READ TAPE 5,E
IDAY=F(203)
IMON=F(202)
READ TAPE 5,F
XCNT=XCNT+1.
9992 READ TAPE 15,B
R(2)=R(2)/1000.
IF(R(2)-F(132))9992,2999,2999
2999 IF(R(2)-(F(132)+21.0))2299,2299,1199
1199 READ TAPE 5,F
XCNT=XCNT+1.
GO TO 2999
2299 TSPIN=R(2)+.667
BACKSPACE 15
100 READ TAPE 15,B
DO 52 K=1,10
L=25*(K-1)
DO 8282 J=1,25
I=J+L
R(J)=R(I)
8282 CONTINUE
IF(R(1)-99999929.)5252,106,5252
5252 J=3
R(2)=R(2)/1000.
IF(R(2)-TSPIN)3415,5143,5143
5143 CSPIN=R(2)
IF((CSPIN-XR2)-.7)141,140,140
141 IF((CSPIN-XR2)-.1)3415,70713,70713
140 IF(JX-1)70713,112,70713
3415 DO 2345 I=1,18
RV(I)=BV1(I)
2345 CONTINUE
I=1
T(3)=R(2)+CON*(3.)
T(4)=R(2)+CON*19.
T(5)=R(2)+CON*35.
20 IF(J-6)7,8,7
7 IF(R(J)-RV(I))6,11,12
12 I=I+1
IF(I-19)7,14,14
14 I=1

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```

      C(J)=00.00
      P(J)=00.00
      J=J+1
      IF(J-12)29,25,29
6     IF(I-1)9,88,9
88    C(J)=00.00
      P(J)=00.00
      J=J+1
      I=1
      IF(J-12)29,25,29
9     CLN=FLN(I-1)+((B(J)-RV(I-1))/(RV(I)-RV(I-1)))*(ELN(I)-FLN(I-1))
      GO TO 15
11    CLN=FLN(I)
15    XIEN=FXPF(CLN)
      C(J)=XIEN
      J=J+1
      I=1
      IF(J-12)29,25,29
C     START OF BAYARD ALPERT 2 COMPUTATION
8     DO 20 I=1,18
      RV(I)=RV2(I)+.075
20    CONTINUE
      T(9)=R(2)+CON*5.
      T(10)=B(2)+CON*21.
      T(11)=B(2)+CON*37.
      J=9
      I=1
      IF(J-12)7,25,7
C     START OF REDHEAD COMPUTATIONS
25    DVC=(XHL-XHF+XML-XMF+XLL-XLF)/3.0
      T(15)=B(2)+CON*10.
      T(16)=B(2)+CON*26.
      T(17)=B(2)+CON*42.
      DO 5432 M=1,8
      VC(M)=VC1(M)
5432  CONTINUE
      DO 5324 M=1,6
      RIC(M)=PIC(M)
5324  CONTINUE
      J=15
      M=1
35    IF(J-18)41,42,41
41    IF(J-21)51,77,51
51    D(J)=R(J)+DVC
      IF(D(J)-VC(M))61,71,72
72    M=M+1

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      IF(M-9)51,75,75
75  M=1
      C(J)=00.00
      D(J)=00.00
      P(J)=00.00
      J=J+1
      GO TO 35
71  CRN=RIC(M)
      D(J)=R(J)
      GO TO 80
61  IF(M-1)6262,99,6262
99  C(J)=00.00
      D(J)=00.00
      J=J+1
      M=1
      GO TO 35
6262 CRN=RIC(M-1)+((D(J)-VC(M-1))/(VC(M)-VC(M-1)))*(RIC(M)-RIC(M-1))
80  XION=FXPF(CRN)
      C(J)=XION
      J=J+1
      M=1
      GO TO 35
C    START OF REDHEAD 2 COMPUTATIONS
42  DO 91 M=1,8
      VC(M)=VC2(M)
91  CONTINUE
      DO 222 M=1,8
      RIC(M)=R2C(M)
222  CONTINUE
      T(18)=R(2)+CON*11.
      T(19)=R(2)+CON*27.
      T(20)=R(2)+CON*43.
      DVC=(X2HL-X2HF+X2ML-X2MF+X2LL-X2LF)/3.0
      J=18
      M=1
      GO TO 41
C    START OF REDHEAD COMPUTATION FOR PRESSURE
77  DO 1234 J=15,17
      IF(C(J)-1.0E-09)789,987,987
789  SRSX=10.
      SRSXA=0.
      GO TO 4047
987  IF(C(J)-1.0E-08)2332,2332,1117
2332 SRSX=7.22
      SRSXA=.60E-10
      GO TO 4047

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1117 IF(C(J)-1.01E-08)2332,2227,7
2227 IF(C(J)-1.0E-07)3337,3337,4447
3337 SRSX=9.3
      SRSXA=.42F-09
      GO TO 4047
4447 IF(C(J)-1.01E-07)3337,5557,5557
5557 IF(C(J)-1.0E-06)6667,6667,8887
6667 SRSX=13.9
      SRSXA=.45F-08
      GO TO 4047
8887 IF(C(J)-1.01E-06)6667,9997,9997
9997 IF(C(J)-2.8E-06)2027,2027,3037
2027 SRSX=16.9
      SRSXA=.34F-07
      GO TO 4047
3037 IF(C(J)-2.81E-06)2027,2727,2727
2727 IF(C(J)-1.0E-05)2828,2828,3838
2828 SRSX=10.8
      SRSXA=-.59F-07
      GO TO 4047
3838 SRSX=10.
      SRSXA=0.
4047 P(J)=(C(J)/SRSX)+SRSXA
      RFD1(II,1)=T(J)
      RFD1(II,2)=R(J)
      RFD1(II,3)=D(J)
      RFD1(II,4)=C(J)
      RFD1(II,5)=P(J)
      II=II+1
1234 CONTINUE
      DO 4321 J=18,20
      IF(C(J)-1.0E-09)7111,7222,7222
7111 SRSX=10.
      SRSXA=0.
      GO TO 7808
7222 IF(C(J)-1.0E-08)7333,7333,7444
7333 SRSX=4.72
      SRSXA=.61F-10
      GO TO 7808
7444 IF(C(J)-1.01E-08)7333,7555,7555
7555 IF(C(J)-1.0E-07)7666,7666,7888
7666 SRSX=6.22
      SRSXA=.23F-09
      GO TO 7808
7888 IF(C(J)-1.01E-07)7666,7101,7101
7101 IF(C(J)-1.0E-06)7202,7202,7303

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7202 SRSX=8.66
      SRSXA=.24E-08
      GO TO 7808
7303 IF(C(J)-1.01E-06)7202,7404,7404
7404 IF(C(J)-2.8E-06)7505,7505,7606
7505 SRSX=11.8
      SRSXA=.23E-07
      GO TO 7808
7606 IF(C(J)-2.81E-06)7505,7005,7005
7005 IF(C(J)-1.0E-05)7025,7025,7035
7025 SRSX=11.8
      SRSXA=.23E-07
      GO TO 7808
7035 SRSX=10.
      SRSXA=0.
7808 P(J)=(C(J)/SRSX)+SRSXA
      RFD2(MM,1)=T(J)
      RFD2(MM,2)=R(J)
      RFD2(MM,3)=D(J)
      RFD2(MM,4)=C(J)
      RFD2(MM,5)=P(J)
      MM=MM+1
4321 CONTINUE
C      START OF BAYARD ALPERT 1 PRESSURE COMPUTATION
      JK=21
444 IF(R(JK)-15.0)212,232,212
232 FM1=R(JK+2)
323 JK=JK+25
      IF(JK-271)121,131,121
131 GO TO 433
121 IF(R(JK)-0.)323,322,323
322 FM2=R(JK+2)
      GO TO 433
212 IF(R(JK)-0.)411,404,411
404 FM2=R(JK+2)
661 JK=JK+25
      IF(JK-271)626,433,626
626 IF(R(JK)-15.0)661,636,661
636 FM1=R(JK+2)
      GO TO 433
411 JK=JK+25
      IF(JK-271)444,555,444
555 IF(X-1.)433,422,433
422 FM1=-0.
      FM2=-0.
      X=X+1.

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433 SFN1=(1.0/97.5)*FM1
   SFN2=(1.0/119.5)*FM2
   X=X+1.
   DO 5445 J=3,5
   P(J)=C(J)/SFN1
   RA1(IX,1)=T(J)
   RA1(IX,2)=R(J)
   RA1(IX,3)=C(J)
   RA1(IX,4)=P(J)
   IX=IX+1
5445 CONTINUE
   DO 4554 J=9,11
   P(J)=C(J)/SFN2
   RA2(JX,1)=T(J)
   RA2(JX,2)=R(J)
   RA2(JX,3)=C(J)
   RA2(JX,4)=P(J)
   JX=JX+1
4554 CONTINUE
   XR2=R(2)
   IF(SENSE SWITCH 2)70712,70713
70712 IF(SENSE SWITCH 1)654,456
654 WRITE OUTPUT TAPE 3,400,B(2),B(3),C(3),B(9),C(9),B(15),D(15),C(15)
   1,B(18),D(18),C(18)
   WRITE OUTPUT TAPE 3,500,B(4),C(4),B(10),C(10),B(16),D(16),C(16),
   1,B(19),D(19),C(19)
   WRITE OUTPUT TAPE 3,500,B(5),C(5),B(11),C(11),B(17),D(17),C(17),
   1,B(20),D(20),C(20)
   GO TO 52
456 WRITE OUTPUT TAPE 3,1000,T(3),B(3),C(3),P(3),T(9),B(9),C(9),P(9)
   WRITE OUTPUT TAPE 3,1009,T(15),B(15),D(15),C(15),P(15),T(18),B(18)
   1,D(18),C(18),P(18)
   WRITE OUTPUT TAPE 3,1000,T(4),B(4),C(4),P(4),T(10),B(10),C(10),P(1
   10)
   WRITE OUTPUT TAPE 3,1009,T(16),B(16),D(16),C(16),P(16),T(19),B(19)
   1,D(19),C(19),P(19)
   WRITE OUTPUT TAPE 3,1000,T(5),B(5),C(5),P(5),T(11),B(11),C(11),P(1
   11)
   WRITE OUTPUT TAPE 3,1009,T(17),B(17),D(17),C(17),P(17),T(20),B(20)
   1,D(20),C(20),P(20)
   IX=1
   JX=3
   II=1
   MM=1
   GO TO 52
70713 IF(R(2) -TSPIN) 52,128,128

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128 IF(JX-2)112,112,113
113 PMIN1=BA1(1,4)
    PMAX1=BA1(1,4)
    IX=IX-1
    GO 7771 IXX=1,IX
    IF(PMIN1-BA1(IXX,4))7772,7773,7773
7773 PMIN1=BA1(IXX,4)
    TMIN1=BA1(IXX,1)
    BMIN1=BA1(IXX,2)
    CMIN1=BA1(IXX,3)
    LMIN1=IXX
7772 IF(PMAX1-BA1(IXX,4))7774,7774,7771
7774 PMAX1=BA1(IXX,4)
    TMAX1=BA1(IXX,1)
    RMAX1=BA1(IXX,2)
    CMAX1=BA1(IXX,3)
    LMAX1=IXX
7771 CONTINUE
    IF(LMIN1-IX)449,450,450
449 LMIN1=LMIN1+1
    PMIN1=BA1(LMIN1,4)
    TMIN1=BA1(LMIN1,1)
    BMIN1=BA1(LMIN1,2)
    CMIN1=BA1(LMIN1,3)
450 IF(LMAX1-1)452,452,451
451 LMAX1=LMAX1-1
    PMAX1=BA1(LMAX1,4)
    TMAX1=BA1(LMAX1,1)
    RMAX1=BA1(LMAX1,2)
    CMAX1=BA1(LMAX1,3)
452 DFLP1=PMAX1-PMIN1
    XC@N=.667
    TRX1=F(60)+XSPIN*XC@N
64483 IF(ABSF(TMAX1-TBX1)-.335)645,19065,19065
19065 IF(TMAX1-TRX1)1300,1301,1302
1300 TRX1=TRX1-.667
    GO TO 64483
1301 GO TO 645
1302 TRX1=TRX1+.667
    GO TO 64483
645 TRN1=F(87)+XSPIN*XC@N
63092 IF(ABSF(TMIN1-TBN1)-.335)36332,71363,71363
71363 IF(TMIN1-TBN1)3100,3101,3102
3100 TRN1=TRN1-.667
    GO TO 63092
3101 GO TO 36332

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3102 TRN1=TRN1+.667
GO TO 63092
36332 SXRA1=F(61)/VP0
SNRA1=F(88)/VP0
S=SXRA1
CALL F0S(S,FS)
FSX=FS
S=SNRA1
CALL F0S(S,FS)
FSN=FS
IF(SXRA1-0.)10480,15011,15011
15011 IF(SXRA1-1.)81647,81647,91647
91647 IF(SNRA1-1.)69179,14194,14194
14194 DB101=((PMAX1*1333.)/(177245.39*VPI*F(61)))
DB102=((DELP1*1333.)/(177245.39*VPI*2.0*(F(61)-F(108))))
GO TO 36207
69179 DB101=((PMAX1*1333.)/(177245.39*VPI*F(61)))
DB102=((DELP1*W0*1333.)/(83150000.*(SQRTF(T0*T1))*(FSX-FSN)))
GO TO 36207
81647 DB101=0.
DB102=((DELP1*W0*1333.)/(83150000.*(SQRTF(T0*T1))*(FSX-FSN)))
GO TO 36207
10480 DB101=0.
DB102=0.
36207 PMIN2=RA2(1,4)
PMAX2=RA2(1,4)
JX=JX-1
DO 5551 JJX=1,JX
IF(PMIN2-RA2(JJX,4))5552,6661,6661
6661 PMIN2=RA2(JJX,4)
TMIN2=RA2(JJX,1)
RMIN2=RA2(JJX,2)
CMIN2=RA2(JJX,3)
LMIN2=JJX
5552 IF(PMAX2-RA2(JJX,4))6662,6662,5551
6662 PMAX2=RA2(JJX,4)
TMAX2=RA2(JJX,1)
RVAX2=RA2(JJX,2)
CMAX2=RA2(JJX,3)
LMAX2=JJX
JX=JJX
5551 CONTINUE
IF(LMIN2-JX)453,454,454
453 LMIN2=LMIN2+1
PMIN2=RA2(LMIN2,4)
TMIN2=RA2(LMIN2,1)

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      RMIN2=RA2(LMIN2,2)
      CMIN2=RA2(LMIN2,3)
454 IF(LMAX2-1)465,465,455
455 LMAX2=LMAX2-1
      PMAX2=RA2(LMAX2,4)
      TMAX2=RA2(LMAX2,1)
      RMAX2=RA2(LMAX2,2)
      CMAX2=RA2(LMAX2,3)
465 DELP2=PMAX2-RMIN2
      TR2=F(63)+XSPIN*XCEN
40004 IF(ABSF(TMAX2-TR2)-.335)44404,44444,44444
44444 IF(TMAX2-TR2)4100,4101,4102
4100 TR2=TR2-.667
      GO TO 40004
4101 GO TO 44404
4102 TR2=TR2+.667
      GO TO 40004
44404 DR2=((1333.*DELP2)/(177245.39*F(64)*DCEN))
      RDR2=DR2*1.83
      IF(IPL0T-4)21,21,22
22 IF((CSPIN-XB2)-29.)23,24,24
23 IF(CSPIN-(TIME1+60.))416,416,26
26 IF(TIME1-60.)416,416,13
13 GO TO(3737,416),ICNT
24 TIME1=CSPIN
      IPL0T = 1
      GO TO 416
3737 ICNT = ICNT + 1
      IPL0T = 1
21 IF(SENSE SWITCH 3)416,214
214 GO TO(412,413,413,415),IPL0T
412 PXX2=PMAX2
      XABB=F(64)-F(109)
      TXX2=TMAX2
      S=F(64)/VP0
      CALL F0S(S,FS)
      XAMM=(VP0*FS)/PXX2
      DO 418 JJX=LMAX2,JX
      THETA=((RA2(JJX,1)-TXX2)/.0167)*9.
      THRAD=THETA*.017453292
      S=(F(109)+XABB*COSF(THRAD))/VP0
      CALL F0S(S,FS)
      VP0FS=VP0*FS
      PNNN=XAMM*RA2(JJX,4)
      XLP=.43429448*L0GF(RA2(JJX,4))
      XV=(XLP+13.)*1250.

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      WRITE OUTPUT TAPE 16,8001,A      ,A(3),F(109),XABB,XAMM,BA2(JJX,1),
1PNNN,THETA,VP@FS,BA2(JJX,4),XLP,XV
418 CONTINUE
      IPL@T=IPL@T+1
      TX@LD=TX@X2
      PX@LD=PX@X2
      GO TO 416
413 KXX=LMAX2-1
      DO 318 JJX=1,KXX
      THETA=((BA2(JJX,1)-TX@LD)/.0167)*9.
      THRAD=THETA*.017453292
      S=(F(109)+XABB*COSF(THRAD))/VP@
      CALL F@S(S,FS)
      VP@FS=VP@*FS
      PNNN=XAMM*BA2(JJX,4)
      XLP=.43429448*L@GF(BA2(JJX,4))
      XV=(XLP+13.)*1250.
      WRITE OUTPUT TAPE 16,8001,A(2),A(3),F(109),XABB,XAMM,BA2(JJX,1),
1PNNN,THETA,VP@FS,BA2(JJX,4),XLP,XV
318 CONTINUE
      GO TO 412
415 IPL@T=5
416 PNR1=REFD1(1,5)
      PXR1=REFD1(1,5)
      II=II-1
      DO 5556 KII=1,II
      IF(PNR1-REFD1(KII,5))5057,5558,5558
5558 PNR1=REFD1(KII,5)
      TNR1=REFD1(KII,1)
      RNR1=REFD1(KII,2)
      DNR1=REFD1(KII,3)
      CNR1=REFD1(KII,4)
      LNR1=KII
5057 IF(PXR1-REFD1(KII,5))5559,5559,5556
5559 PXR1=REFD1(KII,5)
      TXR1=REFD1(KII,1)
      BXR1=REFD1(KII,2)
      DXR1=REFD1(KII,3)
      CXR1=REFD1(KII,4)
      LMR1=KII
      LX=KII
5556 CONTINUE
      IF(LNR1-II)457,458,458
457 LNR1=LNR1+1
      PNR1=REFD1(LNR1,5)
      TNR1=REFD1(LNR1,1)

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      BNR1=RED1(LNR1,2)
      DNR1=RED1(LNR1,3)
      CNR1=RED1(LNR1,4)
458  IF(LMR1-1)460,460,459
459  LMR1=LMR1-1
      PXR1=RED1(LMR1,5)
      TXR1=RED1(LMR1,1)
      RXR1=RED1(LMR1,2)
      DXR1=RED1(LMR1,3)
      CXR1=RED1(LMR1,4)
460  DERP1=PXR1-PNR1
      TR1=F(72)+XSPIN*XC0N
50005 IF(ABS(TXR1-TR1)-.335)55505,55555,55555
55555 IF(TXR1-TR1)4000,4001,4002
4000  TR1=TR1-.667
      GO TO 50005
4001  GO TO 55505
4002  TR1=TR1+.667
      GO TO 50005
55505 DR1=((1333.*DERP1)/(177245.39*F(73)*DC0N))
      RDR1=DR1*1.83
      IF(JPL0T-4)31,31,32
32  IF((CSPIN-XR2)-29.0)33,34,34
33  IF(CSPIN-(TIME2+60.))516,516,36
36  IF(TIME2-60.)516,516,39
39  GO TO(725,516),JCNT
34  TIME2 = CSPIN
      JPL0T = 1
      GO TO 516
725  JCNT = JCNT + 1
      JPL0T = 1
31  IF(SENSE SWITCH 3)516,215
215  GO TO(512,513,513,515),JPL0T
512  PXXR1=PXR1
      TXXR1=TXR1
      XRRR=F(73)-F(112)
      S=F(73)/VP0
      CALL F0S(S,FS)
      XMMM=(VP0*FS)/PXXR1
      DO 4180 KII=LMR1,II
      THETA=((RED1(KII,1)-TXXR1)/.0167)*9.
      THRAD=THETA*.017453292
      S=(F(112)+XRRR*CSF(THRAD))/VP0
      CALL F0S(S,FS)
      VP0FSX=VP0*FS
      PNNN=XMMM*RED1(KII,5)

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      XLP=.43429448*LOGF(RFD1(KII,1))
      XV=(XLP+13.)*1250.0
      WRITE OUTPUT TAPE 25,8001,A(2),A(3),F(112),XBBB,XMMM,RFD1(KII,1),
      1PNNN,THETA,VP@FSX,RFD1(KII,5),XLP,XV
4180 CONTINUE
      JPL@T=JPL@T+1
      TX@P1=TXXR1
      PX@P1=PXXR1
      GO TO 516
513 LXX=LNR1-1
      DO 3180 KII=1,LXX
      THETA=((RFD1(KII,1)-TX@P1)/.0167)*9.
      THPAD=THETA*.017453292
      S=(F(112)+XBBB*COSE(THPAD))/VP@
      CALL F@S(S,FS)
      VP@FC=VP@*FS
      PNNN=XMMM*RFD1(KII,5)
      XLP=.43429448*LOGF(RFD1(KII,5))
      XV=(XLP+13.)*1250.0
      WRITE OUTPUT TAPE 25,8001,A(2),A(3),F(112),XBBB,XMMM,RFD1(KII,1),
      1PNNN,THETA,VP@FS ,RFD1(KII,5),XLP,XV
3180 CONTINUE
      GO TO 512
515 JPL@T=5
516 PNR2=RFD2(1,5)
      PXR2=RFD2(1,5)
      MM=MM-1
      DO 4115 KM=1,MM
      IF(PNR2-RFD2(KM,5))3113,3114,3114
3114 PNR2=RFD2(KM,5)
      TNR2=RFD2(KM,1)
      RNR2=RFD2(KM,2)
      DNR2=RFD2(KM,3)
      CNR2=RFD2(KM,4)
      LNR2=KM
3113 IF(PXR2-RFD2(KM,5))4114,4114,4115
4114 PXR2=RFD2(KM,5)
      TXR2=RFD2(KM,1)
      RXR2=RFD2(KM,2)
      DXR2=RFD2(KM,3)
      CXR2=RFD2(KM,4)
      LMR2=KM
      MX=KM
4115 CONTINUE
      IF(LNR2-MM)461,462,462
461 LNR2=LNR2+1

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PNR2=RFD2(LNR2,5)
TNR2=RFD2(LNR2,1)
RNR2=RFD2(LNR2,2)
DNR2=RFD2(LNR2,3)
CNR2=RFD2(LNR2,4)
462 IF(LMR2-1)464,464,463
463 LMR2=LMP2-1
PXR2=RFD2(LMR2,5)
TXR2=RFD2(LMR2,1)
RXR2=RFD2(LMR2,2)
DXR2=RFD2(LMR2,3)
CXR2=RFD2(LMR2,4)
464 DFRP2=PXR2-PNR2
IF(KPL@T-4)81,81,82
82 IF((CSPIN-XR2)-29.0)83,84,84
83 IF(CSPIN-(TIME3+60.))616,616,86
86 IF(TIME3-60.)616,616,85
85 GO TO(726,616),KCNT
84 TIME3 = CSPIN
KPL@T = 1
GO TO 616
726 KCNT = KCNT + 1
KPL@T = 1
81 IF(SENSE SWITCH 3)616,216
216 GO TO(612,613,613,615),KPL@T
612 PXXR2=PXR2
TXXR2=TXR2
XCBB=F(76)-F(113)
S=F(76)/VP@
CALL F@S(S,FS)
XCMM=(VP@*FS)/PXXR2
DO 4118 KM=LMR2,MM
THETA=((RFD2(KM,1)-TXXR2)/.0167)*9.
THRAD=THETA*.017453292
S=(F(113)+XCBB*C@SF(THRAD))/VP@
CALL F@S(S,FS)
VP@FSX=VP@*FS
PNNN=XCMM*RFD2(KM,5)
XLP=.43429448*L@GF(RFD2(KM,5))
XV=(XLP+13.)*1250.
WRITE OUTPUT TAPE 26,8001,A(2),A(3),F(113),XCBB,XCMM,RFD2(KM,1),
1PNNN,THETA,VP@FSX,RFD2(KM,5),XLP,XV
4118 CONTINUE
KPL@T=KPL@T+1
TX@P2=TXXR2
PX@P2=PXXR2

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      GO TO 616
613  MMX=LMR2-1
      DO 4121 KM=1,MMX
      THETA=((RED2(KM,1)-TXOR2)/.0167)*9.
      THRAD=THETA*.017453292
      S=(F(113)+XCBB*COSF(THRAD))/VP0
      CALL FOS(S,FS)
      VP0FSX=VP0*FS
      PNNN=XCMM*RED2(KM,5)
      XLP=.43429448*LOGF(RED2(KM,5))
      XV=(XLP+13.)*1250.
      WRITE OUTPUT TAPE 26,8001,A(2),A(3),F(113),XCBB,XCMM,RED2(KM,1),
1PNNN,THETA,VP0FSX,RED2(KM,5),XLP,XV
4121 CONTINUE
      GO TO 612
615  KPL0T=5
616  TRN2=F(102)+XSPIN*XC0N
74851 IF(ARSF(TRN2-TRN2)-.335)10368,85187,85187
85187 IF(TRN2-TRN2)3000,3001,3002
3000 TRN2=TRN2-.667
      GO TO 74851
3001 GO TO 10368
3002 TRN2=TRN2+.667
      GO TO 74851
10368 TRX2=F(75)+XSPIN*XC0N
14202 IF(ARSF(TRX2-TRX2)-.335)78371,37117,37117
37117 IF(TRX2-TRX2)2001,2002,2003
2001 TRX2=TRX2-.667
      GO TO 14202
2002 GO TO 78371
2003 TRX2=TRX2+.667
      GO TO 14202
78371 SXRED2=F(76)/VP0
      SNRED2=F(103)/VP0
      S= SXRED2
      CALL FOS(S,FS)
      FSX2=FS
      S=SNRED2
      CALL FOS(S,FS)
      FSN2=FS
      IF(SXRED2-0.)91291,22368,22368
22368 IF(SXRED2-1.)46573,46573,25595
25595 IF(SNRED2-1.)85393,30995,30995
30995 DR201=((PXR2*1333.)/(177245.39*VPI*F(76)))
      DR202=((DFRP2*1333.)/(177245.39*VPI*2.0*(F(76)-F(113))))
      GO TO 89198

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85393 DR201=((PXR2*1333.)/(177245.9*VPI*F(76)))
      DR202=((DERP2*W0*1333.)/(83150000.*(SQRTF(T0*TI)))*(FSX2-FSN2)))
      GO TO 89198
46573 DR201=0.
      DR202=((DERP2*W0*1333.)/(83150000.*(SQRTF(T0*TI)))*(FSX2-FSN2)))
      GO TO 89198
91291 DR201=0.
      DR202=0.
89198 RR201=DR201*1.83
      RR202=DR202*1.83
      CALL INTER(TSPIN,NREC,YALT,YLAT,YLONG,YLST)
      WRITE OUTPUT TAPE 3,3500,TMAX2,BMAX2,CMAX2,PMAX2
      WRITE OUTPUT TAPE 3,3510,YALT,YLAT,YLONG,YLST,DELP2,TB2,F(64),
1DR2,RDR2
      WRITE OUTPUT TAPE 3,3501,TMIN2,BMIN2,CMIN2,PMIN2
      WRITE OUTPUT TAPE 3,3610,TXR1,BXR1,DXR1,CXR1,PXR1
      WRITE OUTPUT TAPE 3,2531,YALT,YLAT,YLONG,YLST,DERP1,TR1,F(73),
1DR1,RDR1
      WRITE OUTPUT TAPE 3,3611,TNR1,BNR1,DNR1,CNR1,PNR1
      WRITE OUTPUT TAPE 3,34095,TRX2,PXR2,TRX2,F(76),SXRED2,DR201,RR201
      WRITE OUTPUT TAPE 3,19174,YALT,YLAT,YLONG,YLST,DERP2,F(113),
1DR202,RR202
      WRITE OUTPUT TAPE 3,39615,TNR2,PNR2,TRN2,F(103),SNRED2
      WRITE OUTPUT TAPE 6,8000,IMON,IDAY,TXR1,YLAT,YLONG,YLST,YALT,
1HID,RDB2,RDR1,RR201,RR202
112 IX=1
      JX=1
      II=1
      MM=1
      IF(B(2)-(F(132)+21.0))2108,218,218
2108 IF(TSPIN-(F(132)+21.0))281,218,218
281 TSPIN=CSPIN+.667
      XSPIN=XSPIN+1.0
      GO TO 52
218 IF(XCNT-F(209))954,955,955
955 WRITE OUTPUT TAPE 3,951
      GO TO 953
954 READ TAPE 5,F
      XCNT=XCNT+1.
      IF(B(2)-(F(132)+21.0))33303,218,218
33303 IF(TSPIN-(F(132)+21.0))33333,218,218
33333 TSPIN=B(2)+.667
      XSPIN=0.
52 CONTINUE
      GO TO 100
106 WRITE OUTPUT TAPE 3,950

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953 REWIND 15
    FND FILE 3
    IF (SENSE SWITCH 4) 335,334
334 CALL PRFSS
335 FND FILE 3
    FND FILE 6
    FND FILE 16
    FND FILE 25
    FND FILE 26
    NR7A = NR7A + 1
    GO TO PRRR
960 IF (SENSE SWITCH 4) 980,981
980 NRRA = NR7A
    GO TO 982
981 NRRA = 2*NR7A
982 PRINT 983,NRRA,NR7A
    PPRINT 959

200 FORMAT(50X1H117H WRONG TAPE ON B5)
202 FORMAT(9F8.2/9F8.2)
203 FORMAT(4F8.2,A3)
204 FORMAT(9F6.3/9F6.3)
300 FORMAT(9F8.6/7F8.6)
303 FORMAT(9F8.2/7F8.2)
305 FORMAT(6F6.3)
400 FORMAT(6XF7.2,2XF6.3,3XE9.2,4XF6.3,4XE9.2,3XF6.3,4XF6.3,3XE9.2,3XF
16.3,4XF6.3,3XF9.2)
500 FORMAT(15XF6.3,3XF9.2,4XF6.3,4XE9.2,3XF6.3,4XF6.3,3XE9.2,3XF6.3,4X
1F6.3,3XF9.2)
600 FORMAT(1H149X15HSATELLITE NO. =F8.0,20X6HEDIT =I4,5X7HORBIT =I4,11
158X7HMONTH =F8.0,11X60X5HDAY =F8.0,11X59X6HYEAR =F8.0,11X52X13HSTATIO
2N NO. =F8.0,11X48X17HANALOG TAPE NO. =F8.0,11X45X2CHPRFSSURE GAUGES
3ID =F15.0,11X)
625 FORMAT(30X15HSATELLITE NO. =F12.4,11X38X7HMONTH =F12.4,11X40X5HDAY =
1F12.4,11X39X6HYEAR =F12.4,11X32X13HSTATION NO. =F12.4,11X28X17HANALOG
2G TAPE NO. =F12.4,11X30X15HS-6 ASPCT ID =F15.4)
699 FORMAT(1H126X72HPRESSURE GAUGES DC OUTPUT VOLTAGES CONVERTED TO PR
1ESSURE AND DENSITY 11X)
700 FORMAT(1H126X72HPRESSURE GAUGES DC OUTPUT VOLTAGES CONVERTED TO IO
1N CURRENT AND PRESSURE 11X)
800 FORMAT (6X109HTIME BA 1 CURRENT BA 2 CURRENT
1 RFD 1 ADJ CURRENT RED 2 ADJ CURRENT 11X)
900 FORMAT(6X107HTIME GAUGE VOLTS ADJ VOLTS CURRENT PRESSURE
1 TIME GAUGE VOLTS ADJ VOLTS CURRENT PRESSURE 11X)
950 FORMAT(35X27HALL DATA HAS BEEN PROCESSED)
959 FORMAT(1H111HEND OF JOB 11X)
970 FORMAT(14X14,10X14)

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983  FORMAT(20X13HFILES @N A3 = ,//20X22HFILES @N A6,B6,C5,C6 =I4)
1000 FORMAT(3XF9.3,4XF7.3,15XE9.2,3XE9.2,3XF9.3,3XF7.3,12XE9.2,4XE9.2)
1009 FORMAT(3XF9.3,4XF7.3,4XF6.3,5XE9.2,3XF9.2,3XF9.3,3XF7.3,2XF6.3,4XE
19.2,4XF9.2)
2500 FORMAT (4X65HTIME(MAX)      GAUGE(VOLTS)      ADJ VOLTS      CURRENT
1 PRESSURE(MAX)///)
2520 FORMAT(4X66HTIME(MIN)      GAUGE(VOLTS)      ADJ VOLTS      CURRENT      P
1 PRESSURE(MIN)////)
3610 FORMAT(6X10HTMAX(SEC)=F9.3,3X8HV(VOLT)=F7.3,3X6HADJ V=F7.3,3X7HC(A
1MP)=F9.2,3X9HP(TORRS)=F9.2///)
3611 FORMAT(6X10HTMIN(SEC)=F9.3,3X8HV(VOLT)=F7.3,3X6HADJ V=F7.3,3X7HC(A
1MP)=F9.2,3X9HP(TORRS)=F9.2////)
33321 FORMAT(60XI3)
9090 FORMAT(90XI2)
9994 FORMAT(70XF9.2)
9993 FORMAT(50XF9.2)
9992 FORMAT(30XE9.2)
9991 FORMAT(4(10XF9.3))
12222 FORMAT(1H029X6H1BA1 9F6.3,/30X6H2BA1 9F6.3)
13333 FORMAT(1H029X6H1BA2 9F6.3,/30X6H2BA2 9F6.3)
12121 FORMAT(1H0 //37X14HTIME - HRS =I2,5X5HMIN =I2,5X5HSEC =F6.3)
14444 FORMAT(1H037X31HBAYARD ALPERT 2 DC SHIFT = .075)
15555 FORMAT(1H037X12HFLIGHT CAL 6F6.3)
20969 FORMAT(1H037X4HT0 =F8.3 ,2X5HT1 = F7.3,2X5HM0 = F7.3,2X5HMI = F7.3
1)
99570 FORMAT(1H037X13HT0RR/AMP 1 = F7.3,6X13HT0RR/AMP 2 = F7.3)
3510 FORMAT(3X3HBA2,4X4HALT=F6.1,3X4HLAT=F6.1,3X5HL0NG=F6.1,3X4HLST=F6.
12,3X4HDP =E9.2,2X6HTXRAM=F9.3,2X4HRX =F7.3,2X9HDENSITY =E9.3/117XE
29.3)
2531 FORMAT(3X3HRH1,4X4HALT=F6.1,3X4HLAT=F6.1,3X5HL0NG=F6.1,3X4HLST=F6.
12,3X4HDP =E9.2,2X6HTXRAM=F9.3,2X4HRX =F7.3,2X9HDENSITY =E9.3/117X
2F9.3)
19174 FORMAT(3X3HRH2,4X4HALT=F6.1,3X4HLAT=F6.1,3X5HL0NG=F6.1,3X4HLST=F6.
12,3X9HDELTA P =F9.2,3X13HAVE.RAM VEL.=F7.3,3X9HDENSITY =E9.3/117X
2F9.3)
53402 FORMAT(3X3HBA1,4X4HALT=F6.1,3X4HLAT=F6.1,3X5HL0NG=F6.1,3X4HLST=F6.
12,3X9HDELTA P =E9.2,3X13HAVE.RAM VEL.=F7.3,3X9HDENSITY =E9.2//)
34095 FORMAT(6X10HTMAX(SEC)=F9.3,3X9HP(TORRS)=E9.2,3X11HTXRAM(SEC)=F9.3,
13X13HMAX.RAM VEL.=F5.3,2X3HSX=F11.3,2X9HDENSITY =E9.3/117XE9.3)
39615 FORMAT(6X10HTMIN(SEC)=F9.3,3X9HP(TORRS)=E9.2,3X11HTNRAM(SEC)=F9.3,
14X13HMIN.RAM VEL.=F7.3,2X4HSN =F11.3/////))
3500 FORMAT(6X10HTMAX(SEC)=F9.3,3X8HV(VOLT)=F7.3,3X7HC(AMP)=E9.2,3X9HP(
1TORRS)=F9.2//)
3501 FORMAT(6X10HTMIN(SEC)=F9.3,3X8HV(VOLT)=F7.3,3X7HC(AMP)=E9.2,3X9HP(
1TORRS)=F9.2/////))
27982 FORMAT(6X10HTMAX(SEC)=F9.3,3X9HP(TORRS)=E9.2,3X11HTXRAM(SEC)=F9.3,

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12X13HMAX.RAM VEL.=F5.3,2X3H=F11.3,2X9HDENSITY =F9.2//)
93965 FORMAT(6X10HTMIN(SFC)=F9.3,2X9HP(TORRS)=E9.2,3X11HTNRAM(SFC)=F9.3,
14X13HMIN.RAM VEL.=F7.3,2X4HSN =F11.3/////))
8000 FORMAT(2I2,F9.3,F7.2,F8.2,F6.2,F6.1,A3,4E9.3)
8001 FORMAT(F4.1,F5.1,E9.3,E9.3,E9.3,F9.3,F9.3,F9.3,F9.3,E9.3,F9.5,F9.0
1)
77276 FORMAT(10X3HS =F9.3,5X4HFS =F9.3,5X4HVP0=E9.3,5X4HRX =F9.3)
951 FORMAT(35X18HEND OF ASPECT DATA)
210 FORMAT(38X30HRH1 - 2.75 RH2 - 3.22 )
949 FORMAT(1HC37X25H CALCULATED ASPECT DATA )
986 FORMAT(1H1////////25X36HMOUNT NEW TAPE ON B5---- PUSH START //////////)
END
* CARDS COLUMN
* LABEL
C MATCH
SUBROUTINE MATCH(NEDI,N)
DIMENSION R(255),F(200),F(142),A(12)
REWIND 5
READ TAPE 15,A
READ TAPE 5,F
IF(99999996.0-E(202))1,1,2
2 IF(A(2)-F(202))7,3,7
3 IF(A(3)-F(203))7,4,7
4 IF(A(5)-F(205))7,5,7
5 IF(5.0-ABS(F(A(11))-F(200)))7,6,6
6 IF(A(10)-F(199))7,12,7
12 BACKSPACE 5
N =0
BACKSPACE 15
GO TO 9
1 PRINT 10,NEDI
GO TO 11
7 READ TAPE 5,F
IF(99999996.0-F(1))8,8,7
10 FORMAT(10X31HASPECT NOT AVAILABLE FOR EDIW = 14)
202 FORMAT(F8.2/F8.2)
204 FORMAT(F6.3/F6.3/F6.3/F6.3)
300 FORMAT(F8.6/F8.6)
206 FORMAT(F6.3)
301 FORMAT(F8.6)
11 READ 202,RI,BIF
READ 300,RE,BF
READ 202,RG,RH
READ 206,BAC
READ 301,BAE
READ 206,BAD

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      READ 204,RA,BB,BC,BD
      N = 1
9     RETURN
      END
*     CARDS COLUMN
      SUBROUTINE GTMC (A,B,C,D)
      TFSTMF(A) = SIGNF(MIN1F(ABSF(A),1.0),A)
      IF(RAD)11,10,11
10    RAD=57.2957795
      THK=11.494
      PHK=-69.68
      SK=SINF(THK/RAD)
      CK=COSF(THK/RAD)
11    F=A/RAD
1    DFL=R-PHK
      IF (R - 180.0) 3,3,6
6     DFL =DFL-180.0
3     CT = SINF(E)
      COST = TESTMF(CK*CT+SK*COSF(E)*COSF(DFL/RAD))
      C= ASIND(COST)
      SINT=SQRT(1.0-COST**2)
      ARG = TFSTMF((CT-CK*COST)/(SK*SINT))
      D=ACOSD(ARG)
4     IF (DFL) 7,8,8
7     D=D-180.0
      GO TO 99
8     IF (DFL - 180.0) 9,9,7
9     D = 180.0 - D
99    RETURN
      END
*     CARDS COLUMN
*     LABEL
C INTER
      SUBROUTINE INTER(TS ,NREC,YALT,YLAT,YLONG,YLST)
      DIMENSION A(8),B(255),RV(18),BI(18),BV2(18),BI2(18),VC(8),RI(8),
      1VC2(8),RI2(8),ELN(18),RIC(8),R2C(8),BV1(18),VC1(8),R1C(8),C(21),
      2D(21),RSCX(4 ),RSX(4 ),RS1(4 ),RS2(4 ),RSC1(4 ),RSC2(4 ),P(21),T(2
      31),RA1(90,4),RA2(90,4),RFD1(90,5),RFD2(90,5),F(209),F(142)
1     , XTIME(30),XALT(30),XLAT(30),XLONG(30),XLST(30),XRBA1(3
      10),XPRA2(30),XRRH1(30), XRRH2(30)
      COMMON BI,BV1,BV2,VC1,VC2,RI,RI2,XHF,XMF,XLF,X2HF,X2MF,X2LF,XHL,
      1XML,XLL,X2HL,X2ML,X2LL,NEDI,NORB
1     , XTIME,XALT,XLAT,XLONG,XLST,XRBA1,XRBA2,XRRH1,XRRH2
      TSS=TS-.334
      JA=1
1300 IF(TSS-XTIME(JA)) 12 ,1302,1303

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12      IF(JA-1)1304,1304,1301
1303    IF(JA-NREC)11 ,1301,10
11      JA = JA + 1
        GO TO 1300
10      JA = JA-1
        GO TO 1301
1302    IF(JA-1) 1304,1304,1305
1304    YALT=XALT(JA)
        YLAT=XLAT(JA)
        YLONG =XLONG(JA)
        YLST=XLST(JA)
        GO TO 1
1305    IF(JA-NREC)1301,1301,1306
1306    YALT=XALT(NREC)
        YLAT=XLAT(NREC)
        YLONG=XLONG(NREC)
        YLST=XLST(NREC)
        GO TO 1
1301    CASP=(TSS-XTIME(JA-1))/(XTIME(JA)-XTIME(JA-1))
        YALT = CASP*(XALT(JA)-XALT(JA-1)) + XALT(JA-1)
        YLAT = CASP*(XLAT(JA)-XLAT(JA-1)) + XLAT(JA-1)
        YLONG = CASP*(XLONG(JA)-XLONG(JA-1)) + XLONG(JA-1)
        YLST = CASP*(XLST(JA)-XLST(JA-1)) + XLST(JA-1)
1      RETURN
      END
*      CARDS COLUMN
*      LIST 8
*      SUBROUTINE PAGE
      SUBROUTINE PAGE (SENSOR)
      DIMENSION FL0K(209),CL0K(141)
C      PAGE 1 FORMAT
      PSTOP=0.
      CENSOR=SENSOR
      READ TAPE 5,FL0K
      STOP=FL0K(209)
      SATN0=FL0K(201)
      XM0=FL0K(202)
      DAY=FL0K(203)
      YR=FL0K(204)
      STAN0=FL0K(205)
      ANATN=FL0K(206)
      READ TAPE 5,CL0K
      PSTOP=PSTOP+1.
      DAYGTM=CL0K(2)
      JHRSMN=CL0K(3)/3600.
      HRSEC=3600*JHRSMN

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RSFC=CLOK(3)-HRSEC
MSECMN=RSFC/60.
R=MSECMN*60
RSEC1M=RSFC-R
PLONGN=CLOK(10)
PLATMN=CLOK(11)
ALTMN=CLOK(12)
PLOCMN=CLOK(13)
100 IF(PSTOP-STOP)11,300,300
11 READ TAPE 5,CLOK
PSTOP=PSTOP+1.
PLONGM=CLOK(10)
PLATMX=CLOK(11)
ALTMX=CLOK(12)
PLOCMX=CLOK(13)
DAYGTX=CLOK(2)
JHRSMX=CLOK(3)/3600.
HRSEC=3600*JHRSMX
RSFC=CLOK(3)-HRSEC
MSECMX=RSFC/60.
R=MSECMX*60
RSEC1X=RSFC-R
GO TO 100
300 CALL PAGE 1 (SATNO,STANO, XM0,DAY,YR,ALTMN,ALTMX,PLATMN,P
CLATMX,PLOCMN,PLOCMX,JHRSAN,MSECMN,RSEC1M,JHRSMX,MSECMX,RSEC1X,DAYG
CTM,DAYGTX,CFNSOR,PLONGN,PLONGM)
N = 0
NSTOP = PSTOP
NSTOP = NSTOP + 1
2 IF(NSTOP-N)3,3,1
1 BACKSPACE 5
N = N + 1
GO TO 2
3 RETURN
END
* CARDS COLUMN
* LIST 8
* SUBROUTINE PAGE 1
SUBROUTINE PAGE 1 (SATNO,STANO, XM0,DAY,YR,ALTMN,ALTMX,PL
CATMN,PLATMX,PLOCMN,PLOCMX,JHRSAN,MSECMN,RSEC1M,JHRSMX,MSECMX,RSEC1
CX,DAYGTM,DAYGTX,CFNSOR,PLONGN,PLONGM)
I=CFNSOR
JA=STANO
CALL GTMC(PLATMN,PLONGN,GAMMA,ALPHA)
CALL GTMC(PLATMX,PLONGM,RHO,BETA)
1001 FORMAT (1H0,39X,25HGEOMAGNETIC LAT (DEG.) F7.2,4H TO F7.2 )

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1000  FORMAT (1H0,39X,25HGEOMAGNET C LONG(DEG.)  F7.2,4H TO F7.2  )
      WRITE OUTPUT TAPE 3,100,SAT,L
      GO TO (211,212,213,214,215,216,217,218),I
211  WRITE OUTPUT TAPE 3,201
      GO TO 209
212  WRITE OUTPUT TAPE 3,202
      GO TO 209
213  WRITE OUTPUT TAPE 3,203
      GO TO 209
214  WRITE OUTPUT TAPE 3,204
      GO TO 209
215  WRITE OUTPUT TAPE 3,205
      GO TO 209
216  WRITE OUTPUT TAPE 3,206
      GO TO 209
217  WRITE OUTPUT TAPE 3,207
      GO TO 209
218  WRITE OUTPUT TAPE 3,208
209  GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18),JA
      1 WRITE OUTPUT TAPE 3,21,XM0,DAY,YR
        GO TO 41
      2 WRITE OUTPUT TAPE 3,22
        GO TO 41
      3 WRITE OUTPUT TAPE 3,23,XM0,DAY,YR
        GO TO 41
      4 WRITE OUTPUT TAPE 3,22
        GO TO 41
      5 WRITE OUTPUT TAPE 3,25,XM0,DAY,YR
        GO TO 41
      6 WRITE OUTPUT TAPE 3,26,XM0,DAY,YR
        GO TO 41
      7 WRITE OUTPUT TAPE 3,27,XM0,DAY,YR
        GO TO 41
      8 WRITE OUTPUT TAPE 3,28,XM0,DAY,YR
        GO TO 41
      9 WRITE OUTPUT TAPE 3,22
        GO TO 41
     10 WRITE OUTPUT TAPE 3,22
        GO TO 41
     11 WRITE OUTPUT TAPE 3,22
        GO TO 41
     12 WRITE OUTPUT TAPE 3,32,XM0,DAY,YR
        GO TO 41
     13 WRITE OUTPUT TAPE 3,33,XM0,DAY,YR
        GO TO 41
     14 WRITE OUTPUT TAPE 3,34,XM0,DAY,YR

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GO TO 41
15 WRITE OUTPUT TAPE 3,35,XM0,DAY,YR
GO TO 41
16 WRITE OUTPUT TAPE 3,36,XM0,DAY,YR
GO TO 41
17 WRITE OUTPUT TAPE 3,37,XM0,DAY,YR
GO TO 41
18 WRITE OUTPUT TAPE 3,38,XM0,DAY,YR
41 WRITE OUTPUT TAPE 3,400,ALTMIN,ALTMAX
WRITE OUTPUT TAPE 3,500,PLATMN,PLATMX
WRITE OUTPUT TAPE 3,1001,GAMMA,RHO
WRITE OUTPUT TAPE 3,501,PLONGN,PLONGM
WRITE OUTPUT TAPE 3,1000,ALPHA,BETA
WRITE OUTPUT TAPE 3,600,PL0CMN,PL0CMX
WRITE OUTPUT TAPE 3,700
WRITE OUTPUT TAPE 3,800,DAYGTM,JHRSMN,MSECMN,RSEC1M
WRITE OUTPUT TAPE 3,900,DAYGTX,JHRSMX,MSECMX,RSEC1X
100 FORMAT (1H0 52X,13HSATELLITE SF2.0)
201 FORMAT (1H0,39X,33H DATA ANALYSIS )
202 FORMAT (1H0,39X,33H ETP NO.2 DATA ANALYSIS )
203 FORMAT (1H0,39X,33H B.A. NO.1 DATA ANALYSIS )
204 FORMAT (1H0,39X,33H B.A. NO.2 DATA ANALYSIS )
205 FORMAT (1H0,39X,33H M.S. NO.1 DATA ANALYSIS )
206 FORMAT (1H0,39X,33H M.S. NO.2 DATA ANALYSIS )
207 FORMAT (1H0,39X,33H R.H. NO.1 DATA ANALYSIS )
208 FORMAT (1H0,39X,33H R.H. NO.2 DATA ANALYSIS )
21 FORMAT (1H0,39X,26HSTATION - BLOSSOM POINT ,5HDATE 3F3.0 )
22 FORMAT (1H0,39X,26HSTATION NUMBER IS INCORRECT )
23 FORMAT (1H0,39X,26HSTATION - FORT MYERS ,5HDATE 3F3.0 )
25 FORMAT (1H0,39X,26HSTATION - QUITO ,5HDATE 3F3.0 )
26 FORMAT (1H0,39X,26HSTATION - LIMA ,5HDATE 3F3.0 )
27 FORMAT (1H0,39X,26HSTATION - ANTOFAGASTA ,5HDATE 3F3.0 )
28 FORMAT (1H0,39X,26HSTATION - SANTIAGO ,5HDATE 3F3.0 )
32 FORMAT (1H0,39X,26HSTATION - ST. JOHNS ,5HDATE 3F3.0 )
33 FORMAT (1H0,39X,26HSTATION - FAIRBANKS ,5HDATE 3F3.0 )
34 FORMAT (1H0,39X,26HSTATION - E. GRAND FORKS ,5HDATE 3F3.0 )
35 FORMAT (1H0,39X,26HSTATION - WINKFIELD ,5HDATE 3F3.0 )
36 FORMAT (1H0,39X,26HSTATION - JOHANNESBURG ,5HDATE 3F3.0 )
37 FORMAT (1H0,39X,26HSTATION - GOLDSTONE LAKE ,5HDATE 3F3.0 )
38 FORMAT (1H0,39X,26HSTATION - WOMMERA ,5HDATE 3F3.0 )
400 FORMAT (1H0,39X,25HALTITUDE RANGE (KM) F7.2,4H TO F7.2 )
500 FORMAT (1H0,39X,25HLATITUDE RANGE (DEG.) F7.2,4H TO F7.2 )
501 FORMAT (1H0,39X,25HLONGITUDE RANGE (DEG.) F7.2,4H TO F7.2 )
600 FORMAT (1H0,39X,25HLOCAL TIME (HRS) F7.2,4H TO F7.2 )
700 FORMAT (1H0,54X,10HTIME (GMT) )
800 FORMAT (1H0,39X,5HFROM F4.0,6HDAYS 12,6H HRS 12,6H MIN F6.3,4H

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```

      CSEC      )
900 FORMAT (1H0,39X,5HT0  F4.0,5H DAYS  12,6H HRS  12,6H MIN  F6.3,4H
      CSEC      )
      RETURN
      END
* CARDS COLUMN
SUBROUTINE F05 (S,FS)
C PROGRAM TO EVALUTE THE THERMAL TRANSPIRATION FUNCTION
  DIMENSION R(2),TN(2)
  R(1)=S
  R(2)=0.
  D SS=R
  D S2=SS*SS
  IF(R(1)-3.8) 8,8,6
  D 6 DFS=3.5449077*SS
  GO TO 70
  R TN(2)=0.
  D ONF=1.
  D TWO=2.
  D T=TWO*S2
  IF(ABS(R(1))-2.5)10,10,40
  D 10 A=ONF
  D SUM=ONF
  DO 20 N=1,49
  TN(1)=N
  D C1=(ONF-TWO*TN)/(ONF+TWO*TN)
  D C2=S2/TN
  D A=C1*(C2*A)
  D FRD=SUM+A
  D IF (FRD-SUM) 20,30,20
  D 20 SUM=FRD
  D 30 DFS=EXPF(-S2)+T*SUM+1.7724538500*SS
  GO TO 70
  D 40 A=-ONF
  D SUM=0.0
  NEND=S2
  DO 50 N=1,NEND
  TN(1)=N
  D A=((ONF-TWO*TN)/T)*A
  D 50 SUM=SUM+A
  D DFS=SUM*EXPF(-S2)
  IF(R(1)) 70,70,60
  D 60 DFS=DFS+3.5449077*SS
  70 FS=DFS
  RETURN
  END

```

```

*      CARDS COLUMN
SUBROUTINE PRESS
C      PRESSURE GAUGES DC OUTPUT VOLTAGES CONVERTED TO
C      CORRECTED ION CURRENT
      DIMENSION A(8),B(255),BV(18),BI(18),BV2(18),BI2(18),VC(8),RI(8),
1VC2(8),RI2(8),ELN(18),RIC(8),R2C(8),BV1(18),VC1(8),R1C(8),C(21),
2D(21),RSCX(4),RSX(4),RS1(4),RS2(4),RSC1(4),RSC2(4),P(21),T(2
31),BA1(90,4),BA2(90,4),RED1(90,5),RED2(90,5),E(209),F(142)
1      , XTIME(30),XALT(30),XLAT(30),XLONG(30),XLST(30),XRBA1(3
10),XPRA2(30),XRRH1(30), XRRH2(30)
      COMMON BI,BV1,BV2,VC1,VC2,RI,RI2,XHF,XMF,XLF,X2HF,X2MF,X2LF,XHL,
1XML,XLL,X2HL,X2ML,X2LL,NEDI,NORB
1      , XTIME,XALT,XLAT,XLONG,XLST,XRBA1,XRBA2,XRRH1,XRRH2
8888 READ TAPE 15,A
      IF(A(8)-600000004.)2,3,2
C      PRINT ERROR MESSAGE - WRONG TAPE
2 PRINT 200
      GO TO 8888
3 A(4)=A(4)+60.
      LW1=A(1)
      LW2=A(2)
      LW3=A(3)
      LW4=A(4)
      LW5=A(5)
      LW6=A(6)
      NRA2=0
      NPFD1=0
      NPFD2=0
      WRITE OUTPUT TAPE 3,600,LW1,NEDI,NORB,LW2,LW3,LW4,LW5,LW6,A(3)
      READ TAPE 15,B
      R(2)=R(2)/1000.
      JHRSMN=R(2)/3600.
      HRSEC=3600*JHRSMN
      RSEC=R(2)-HRSEC
      MSECNM=RSEC/60.
      XRRR=MSECNM*60
      RSEC1M=RSEC-XRRR
      BACKSPACE 15
      WRITE OUTPUT TAPE 3,12121,JHRSMN,MSECNM,RSEC1M
      WRITE OUTPUT TAPE 3,12222,BV1
      WRITE OUTPUT TAPE 3,13333,BV2
      WRITE OUTPUT TAPE 3,14444
      WRITE OUTPUT TAPE 3,15555,XHF,XMF,XLF,X2HF,X2MF,X2LF
      WRITE OUTPUT TAPE 3,700
      IF(SENSE SWITCH 1)711,722
722 WRITE OUTPUT TAPE 3,900

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```

      GO TO 6111
711  WRITE OUTPUT TAPE 3,800
6111 X=1.
      DO 4 I=1,18
      FLN(I)=LOGF(BI(I))
      4  CONTINUE
      DO 30 M=1,8
      R1C(M)=LOGF(RI(M))
      30  CONTINUE
      DO 95 M=1,8
      P2C(M)=LOGF(RI2(M))
      95  CONTINUE
      CON=.05/48.
100  READ TAPE 15,B
      DO 52 K=1,10
      L=25*(K-1)
      DO 8282 J=1,25
      I=J+L
      R(J)=R(I)
8282  CONTINUE
      IF(R(1)-99999999.15252,106,5252
5252  J=2
      DO 2345 I=1,18
      RV(I)=RV1(I)
2345  CONTINUE
      I=1
      R(2)=R(2)/1000.
      T(3)=B(2)+CON*(3.)
      T(4)=R(2)+CON*19.
      T(5)=R(2)+CON*35.
29  IF(J-6)7,8,7
      7  IF(R(J)-RV(I))6,11,12
12  I=I+1
      IF(I-19)7,14,14
14  I=1
      C(J)=00.00
      P(J)=00.00
      J=J+1
      I=1
      IF(J-12)29,25,29
      6  IF(I-1)9,88,9
88  C(J)=00.00
      P(J)=00.00
      J=J+1
      I=1
      IF(J-12)29,25,29

```



```

9 CLN=FLN(I-1)+((B(J)-BV(I-1) (BV(I)-BV(I-1)))*(ELN(I)-ELN(I-1))
GO TO 15
11 CLN=FLN(I)
15 XION=FXPF(CLN)
N=J
C(N)=XION
J=J+1
I=1
IF(J-12)29,25,29
C START OF BAYARD ALPERT 2 COMPUTATION
8 DO 20 I=1,18
RV(I)=RV2(I)+.075
20 CONTINUE
T(9)=B(2)+CON*5.
T(10)=B(2)+CON*21.
T(11)=B(2)+CON*37.
J=9
I=1
IF(J-12)7,25,7
C START OF REDHEAD COMPUTATIONS
25 DVC=(XHL-XHF+XML-XMF+XLL-XLF)/3.0
T(15)=B(2)+CON*10.
T(16)=B(2)+CON*26.
T(17)=B(2)+CON*42.
DO 5432 M=1,8
VC(M)=VC1(M)
5432 CONTINUE
DO 5324 M=1,8
RIC(M)=RIC(M)
5324 CONTINUE
J=15
M=1
35 IF(J-18)41,42,41
41 IF(J-21)51,77,51
51 D(J)=B(J)+DVC
IF(D(J)-VC(M))61,71,72
72 M=M+1
IF(M-9)51,75,75
75 M=1
C(J)=00.00
D(J)=00.00
P(J)=00.00
J=J+1
GO TO 35
71 CRN=RIC(M)
D(J)=R(J)

```

```

      GO TO 80
61 IF(M-1)6262,99,6262
99 C(J)=00.00
   D(J)=00.00
   J=J+1
   M=1
      GO TO 35
6262 CRN=RIC(M-1)+((D(J)-VC(M-1))/(VC(M)-VC(M-1)))*(RIC(M)-RIC(M-1))
80 XION=FXPF(CRN)
   C(J)=XION
   J=J+1
   M=1
      GO TO 35
C   START OF REDHEAD 2 COMPUTATIONS
42 DO 91 M=1,8
   VC(M)=VC2(M)
91 CONTINUE
   DO 222 M=1,8
   RIC(M)=R2C(M)
222 CONTINUE
   T(18)=B(2)+CON*11.
   T(19)=B(2)+CON*27.
   T(20)=B(2)+CON*43.
   DVC=(X2HL-X2HF+X2ML-X2MF+X2LL-X2LF)/3.0
   J=18
   M=1
      GO TO 41
C   START OF REDHEAD COMPUTATION FOR PRESSURE
77 DO 1234 J=15,17
   IF(C(J)-1.0E-09)789,987,987
789 SRSX=10.
   SPSXA=0.
      GO TO 4047
987 IF(C(J)-1.0E-08)2332,2332,1117
2332 SPSX=7.22
   SRSXA=.60E-10
      GO TO 4047
1117 IF(C(J)-1.01E-08)2332,2227,2227
2227 IF(C(J)-1.0E-07)3337,3337,4447
3337 SRSX=9.3
   SRSXA=.42E-09
      GO TO 4047
4447 IF(C(J)-1.01E-07)3337,5557,5557
5557 IF(C(J)-1.0E-06)6667,6667,8887
6667 SRSX=13.9
   SRSXA=.45E-08

```

GO TO 4047
 8887 IF(C(J)-1.01E-06)6667,9997,9997
 9997 IF(C(J)-2.8E-06)2027,2027,3037
 2027 SRSX=16.9
 SRSXA=.34E-07
 GO TO 4047
 3037 IF(C(J)-2.81E-06)2027,2727,2727
 2727 IF(C(J)-1.0E-05)2828,2828,3838
 2828 SRSX=10.8
 SRSXA=-.59E-07
 GO TO 4047
 3838 SRSX=10.
 SRSXA=0.
 4047 P(J)=(C(J)/SRSX)+SRSXA
 1234 CONTINUE
 DO 4321 J=18,20
 IF(C(J)-1.0E-09)7111,7222,7222
 7111 SRSX=10.
 SRSXA=0.
 GO TO 7808
 7222 IF(C(J)-1.0E-08)7333,7333,7444
 7333 SRSX=4.72
 SRSXA=.61E-10
 GO TO 7808
 7444 IF(C(J)-1.01E-08)7333,7555,7555
 7555 IF(C(J)-1.0E-07)7666,7666,7888
 7666 SRSX=6.22
 SRSXA=.23E-09
 GO TO 7808
 7888 IF(C(J)-1.01E-07)7666,7101,7101
 7101 IF(C(J)-1.0E-06)7202,7202,7303
 7202 SRSX=8.66
 SRSXA=.24E-08
 GO TO 7808
 7303 IF(C(J)-1.01E-06)7202,7404,7404
 7404 IF(C(J)-2.8E-06)7505,7505,7606
 7505 SRSX=11.8
 SRSXA=.23E-07
 GO TO 7808
 7606 IF(C(J)-2.81E-06)7505,7005,7005
 7005 IF(C(J)-1.0E-05)7025,7025,7035
 7025 SRSX=11.8
 SRSXA=.23E-07
 GO TO 7808
 7035 SRSX=10.
 SRSXA=0.

```

7808 P(J)=(C(J)/SRSX)+SRSXA
4321 CONTINUE
C      START OF BAYARD ALPERT 1 PRESSURE COMPUTATION
      J=21
444 IF(R(J)-15.0)212,232,212
232 FM1=R(J+2)
323 J=J+25
      IF(J-271)121,131,121
131 GO TO 433
121 IF(R(J)-2.1)323,322,323
322 FM2=R(J+2)
      GO TO 433
212 IF(R(J)-2.1)411,404,411
404 FM2=R(J+2)
661 J=J+25
      IF(J-271)626,433,626
626 IF(R(J)-15.0)661,636,661
636 FM1=R(J+2)
      GO TO 433
411 J=J+25
      IF(J-271)444,555,444
555 IF(X-1.1)433,422,433
422 FM1=-0.
      FM2=-0.
      X=X+1.
433 SEN1=(1.0/97.5)*FM1
      SEN2=(1.0/119.5)*FM2
      X=X+1.
      DO 5445 J=3,5
      P(J)=C(J)/SEN1
5445 CONTINUE
      DO 4554 J=9,11
      P(J)=C(J)/SEN2
4554 CONTINUE
      IF(SENSE SWITCH 1)654,456
654 WRITE OUTPUT TAPE 3,400,B(2),B(3),C(3),B(9),C(9),B(15),D(15),C(15)
      1,B(18),D(18),C(18)
      WRITE OUTPUT TAPE 3,500,B(4),C(4),B(10),C(10),B(16),D(16),C(16),
      1B(19),D(19),C(19)
      WRITE OUTPUT TAPE 3,500,B(5),C(5),B(11),C(11),B(17),D(17),C(17),
      1B(20),D(20),C(20)
      GO TO 52
456 WRITE OUTPUT TAPE 3,9191,FM1,FM2
      WRITE OUTPUT TAPE 3,1000,T(3),B(3),C(3),P(3),T(9),B(9),C(9),P(9)
      WRITE OUTPUT TAPE 3,1009,T(15),B(15),D(15),C(15),P(15),T(18),B(18)
      1,D(18),C(18),P(18)

```

```

WRITE OUTPUT TAPE 3,1000,T(  ,B(4),C(4),P(4),T(10),B(10),C(10),P(1
10)
WRITE OUTPUT TAPE 3,1009,T(16),B(16),D(16),C(16),P(16),T(19),B(19)
1,D(19),C(19),P(19)
WRITE OUTPUT TAPE 3,1000,T(5),B(5),C(5),P(5),T(11),B(11),C(11),P(1
11)
WRITE OUTPUT TAPE 3,1009,T(17),B(17),D(17),C(17),P(17),T(20),B(20)
1,D(20),C(20),P(20)
52 CONTINUE
GO TO 100
106 WRITE OUTPUT TAPE 3,950
REWIND 15
200 FORMAT(50X1H117H WRONG TAPE ON B5)
202 FORMAT(9F8.2/9E8.2)
204 FORMAT(9F6.3/9F6.3)
300 FORMAT(9F8.6/7F8.6)
303 FORMAT(9F8.2/7E8.2)
305 FORMAT(6F6.3)
400 FORMAT(6XF7.2,2XF6.3,3XE9.2,4XF6.3,4XE9.2,3XF6.3,4XF6.3,3XE9.2,3XF
16.3,4XF6.3,3XE9.2)
500 FORMAT(15XF6.3,3XE9.2,4XF6.3,4XE9.2,3XF6.3,4XF6.3,3XE9.2,3XF6.3,4X
1F6.3,3XF9.2)
600 FORMAT(1H154X15HSATFLITE NO. = 15,18X6HEDIT =14,5X7H0RBIT =14,
1//63X7HMONTH = 15,//65X5HDAY =
1 15,//64X6HYEAR = 15,//57X13HSTATION NO. =15,//53X17HANALOG TAPE
2NO. =15,//50X20HPRESSURE GAUGES ID =F13.0//3//)
700 FORMAT(1H126X72HPRESSURE GAUGES DC OUTPUT VOLTAGES CONVERTED TO 10
IN CURRENT AND PRESSURE////)
800 FORMAT (6X109HTIME BA 1 CURRENT BA 2 CURRENT
1 RED 1 ADJ CURRENT RED 2 ADJ CURRENT////)
900 FORMAT(6X107HTIME GAUGE VOLTS ADJ VOLTS CURRENT PRESSURE
1 TIME GAUGE VOLTS ADJ VOLTS CURRENT PRESSURE////)
950 FORMAT(35X27HALL DATA HAS BEEN PROCESSED)
1000 FORMAT(3XF9.3,4XF7.3,15XE9.2,3XF9.2,3XF9.3,3XF7.3,12XE9.2,4XE9.2)
1009 FORMAT(3XF9.3,4XF7.3,4XF6.3,5XE9.2,3XE9.2,3XF9.3,3XF7.3,2XF6.3,4XE
10.2,4XF9.2)
23221 FORMAT(50X12)
12222 FORMAT(1H036X6H1BA1 9F6.3,/37X6H2BA1 9F6.3)
13333 FORMAT(1H036X6H1BA2 9F6.3,/37X6H2BA2 9F6.3)
12121 FORMAT(1H0///44X14HTIME - HRS =12,5X5HMIN =12 ,5X5HSFC =F6.3)
14444 FORMAT(1H044X31HBAYARD ALPERT 2 DC SHIFT = .075)
15555 FORMAT(1H044X12HFLIGHT CAL 6F6.3)
9191 FORMAT(30X22HBA1 EMISSION CURRENT =F9.3,10X22HBA2 EMISSION CURRENT
1 =F9.3)
RETURN
END

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```

*      SUBROUTINE DEN
*      CARDS COLUMN
*      EAP
      LRL      DEN,X
      ENTRY   DEN
DEN      CAL      @R6
      STA      *+1
      SDN
      CAL      @A6
      STA      *+1
      SDN
      CAL      @C5
      STA      *+1
      SDN
      CAL      @C6
      STA      *+1
      SDN
      TRA      1,4
      @R6      @CT      000000002206
      @A6      @CT      000000001206
      @C5      @CT      000000003205
      @C6      @CT      000000003206
      END
*
*      END TAPE

```

BA 1 AND BA 2 VOLTAGE TO CURRENT
CONVERSION TABLE*

BA 1 V_i Volts	I_c Current	BA 2 V_i Volts
.188	1.0×10^{-11}	-0.212
.285	2.0×10^{-11}	-0.123
.495	3.0×10^{-11}	0.049
.611	5.0×10^{-11}	0.212
.721	7.0×10^{-11}	0.305
.859	1.0×10^{-10}	0.418
1.065	2.0×10^{-10}	0.638
1.172	3.0×10^{-10}	0.790
1.345	1.0×10^{-7}	0.985
1.503	3.0×10^{-9}	1.164
1.808	1.0×10^{-8}	1.488
2.195	3.0×10^{-8}	1.868
2.565	1.0×10^{-7}	2.170
2.955	3.0×10^{-7}	2.538
3.330	1.0×10^{-6}	2.883
3.755	1.0×10^{-5}	3.307
4.211	3.0×10^{-5}	3.720
4.686	3.0×10^{-5}	4.235

*Table is the same for RH gauges except that the gauge voltage values are different and the I_c is only given for seven (7) values.

GAUGE SENSITIVITY
TABLE OF VALUES A AND B FOR REDHEAD
GAUGES ONE AND TWO

Gauge Current Range	RH 1 B	RH 1 A	RH 2 B	RH 2 A
$10^{-9} - 10^{-8}$ amps	7.22	0.60×10^{-10}	4.72	0.61×10^{-10}
$10^{-8} - 10^{-7}$	9.3	0.42×10^{-9}	6.22	0.23×10^{-10}
$10^{-7} - 10^{-6}$	13.9	0.45×10^{-8}	8.66	0.24×10^{-8}
$1 \times 10^{-6} -$ 2.8×10^{-6}	16.9	0.34×10^{-7}	11.8	0.23×10^{-7}
$2.8 \times 10^{-6} -$ 10^{-5}	10.8	0.59×10^{-7}	11.8	0.23×10^{-7}